

EAST BAY MUNICIPAL UTILITY DISTRICT
ENGINEERING & OPERATIONS OFFICE
Oakland, California

SUPPORTING CALCULATIONS

for

DINGEE RESERVOIR

April 14, 1975

Submitted in Fulfillment of the Requirements of
Senate Bill No. 896, State of California

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PROJECT: INUNDATION MAPS
SUBJECT: DINGEE RESERVOIR
METHOD OF ANALYSIS

Drawn by: SPD, 3-10-75
Check by: P.M.J. 4/4/75

METHOD USED IN DERIVING THE AREA OF INUNDATION
IS COMPRISED OF THE FOLLOWING STEPS:

1. FOR THE RESERVOIR ANALYZED, THE BREACH SECTION(S)
WAS LOCATED ON A TOPOGRAPHIC MAP, ON THE BASIS
OF SOILS AND FOUNDATION CONSIDERATIONS.
2. MAXIMUM BREACH SECTION OUTFLOW WAS DETERMINED
USING THE RELATION:

$$Q_{\max} = f(C_T) d^{2.5}$$

WHERE Q_{\max} = MAXIMUM DISCHARGE, CFS

C_T = BREACH SHAPE COEFFICIENT

$$f(C_T) = Q_{\max} / d^{2.5} \text{ FROM PLATE NO. 2}$$

d = DEPTH OF WATER AT ONE HALF RESERVOIR
CAPACITY.

(REF.: CORPS OF ENGINEERS, "FLOW THROUGH A
BREACHED DAM" MILITARY HYDROLOGY BULLETIN
NO. 9, JUNE 1957 & O.E.S. LETTER OF OCT. 11, 1974)

3. THE COURSE(S) THAT BREACH FLOW WILL FOLLOW
WAS DELINEATED FROM THE STUDY OF CONTOUR
MAPS, TOPOGRAPHIC FEATURES, AND FIELD VISITS
TO THE AREA INVOLVED



PROJECT INUNDATION MAPS
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Comp by SPD DATE 3-10-75
CHK'd by P.M.J. DATE 4/4/75

4. TIME REQUIRED TO DRAIN THE RESERVOIR

UNDER BREACH FLOW CONDITIONS WAS COMPUTED IN ORDER TO DETERMINE POSSIBLE APPLICABILITY OF FLOOD ROUTING ANALYSIS, FOR A SHORT DURATION BREACH FLOW HYDROGRAPH OR FOR INUNDATION AREAS WITH ILL DEFINED MULTIPLE FLOW DIRECTIONS AND PONDING, ROUTING ANALYSIS CANNOT BE USED EFFECTIVELY.

5. INUNDATION IN AREAS WITH ILL DEFINED - MULTIPLE FLOW DIRECTIONS AND PONDING WAS ANALYZED BY USE OF FLOOD PRONE AREA MAPS AND OTHER AVAILABLE INFORMATION SUCH AS CAPACITY OF ROADWAYS TO CARRY THE BREACH FLOW.

6. TIME REQUIRED TO REACH FLOOD LEVEL AT SELECTED LANDMARKS IS COMPUTED ON THE BASIS OF THE DISTANCE OF THE LANDMARK FROM THE RESERVOIR AND THE VELOCITY OF FLOOD WAVE. TRAVEL TIMES OF MORE THAN FIFTEEN MINUTES ARE SHOWN ON THE MAP.

INUNDATION MAPS
DINGEE RESERVOIR
RESERVOIR DETAILS

SPD.

3-10-75

P.m.g.

4/4/75

DINGEE RESERVOIR

TYPE: OPEN CUT, LINED AND WITH ROOF

YEAR IN OPERATION: 1894/1939

OVERFLOW ELEV.: 772.0

1/2 CAPACITY ELEV.: 766.2 (CAPACITY CURVE)

INFLOW ELEV.: 755.9

CAPACITY: 4.182 MG = 559,100 CFT = 12.84 ACRE- FEET

DINGEE RESERVOIR IS ONE OF THE OLDER STRUCTURES BUILT BY A PREDECESSOR WATER COMPANY. THE ROOF OF THIS CONCRETE LINED RESERVOIR WAS REPLACED IN 1939.

MATERIALS ENGINEERING SECTION, ON THE BASIS OF GEOLOGIC AND SOILS STABILITY CONSIDERATIONS, INDICATES THAT ONLY THE WEST SIDE OF THE RESERVOIR EMBANKMENT IS VULNERABLE TO POTENTIAL FAILURE.

A ROAD "ESTATES DRIVE" RUNS ALONG THE WEST SIDE OF THE RESERVOIR, ABOUT 15 FEET BELOW THE TOP OF THE EMBANKMENT AND 50 FEET TO THE WEST, A NATURAL DEPRESSION IN THE DIRECTION OF INDICATED BREACH RUNS FROM ESTATES DRIVE TO



INUNDATION MAPS
DINGEE RESERVOIR

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HARBORD DRIVE, ABOUT 300 FEET AWAY, HARBORD DRIVE RUNS DOWNHILL IN A NORTHWESTERLY DIRECTION FOR ABOUT 500 FEET. AT THIS POINT A NARROW, DEEP (ABOUT 60 FEET) VALLEY ON THE WEST SIDE RUNS TOWARDS MORAGA AVENUE, APPROXIMATELY 1200 FEET AWAY. MORAGA AVENUE ALSO RUNS DOWNHILL IN A WESTERLY DIRECTION FOR ABOUT 2000 FEET. AT THIS LOCATION, ON THE NORTH, ANOTHER VALLEY IS SITUATED, WHICH DRAINS INTO FOUR DETENTION BASINS HAVING A TOTAL DROP OF 60 FEET IN ELEVATION. THESE BASINS ARE REGULATED BY MOUNTAIN VIEW CEMETERY THROUGH CONTROLLED DISCHARGE OUTLET LINES TO GLEN ECHO CREEK. PARTIALLY CULVERTED GLEN ECHO CREEK DRAINS INTO LAKE MERRITT. LAKE MERRITT, WITH SURFACE AREA ABOUT 135 ACRES, IS A POND WITH AN OUTLET TO THE BAY.

CAPACITIES OF VARIOUS SECTIONS WITHIN THE INUNDATION AREA TO CARRY BREACH FLOW ARE COMPUTED ON SHEET 4.

ILL-DEFINED MULTI-DIRECTIONAL FLOW AND PONDING MAKE ANY FLOOD ROUTING ANALYSIS INEFFECTIVE.



PROJECT: INUNDATION MAPS

DESIGNED BY: SPD

DATE: 3-10-75

PROJECT: DINGEE RESERVOIR

CHECKED BY: PMJ

DATE: 4/4/75

BREACH FLOW

ASSUMING A TRIANGULAR BREACH OF FULL DEPTH
AND TOP WIDTH EQUAL TO FULL DEPTH, AREA OF
BREACH FLOW AT $\frac{1}{2}$ RESERVOIR CAPACITY IS: $\frac{1}{2} \times 10.3 \times 10.3 = 53 \text{ SQ. FT.}$

AREA OF RESERVOIR SECTION = $\frac{160+200}{2} \times 10.3 = 1854 \text{ SQ. FT.}$
AT $\frac{1}{2}$ RESERVOIR CAPACITY

AS THE AREA OF BREACH IS LESS THAN ONE SIXTH
AREA OF RESERVOIR $53 \text{ SQ. FT.} < \frac{1}{6}(1854) = 309 \text{ SQ. FT.}$

THE BREACH IS CONSIDERED TO BE SMALL.

$$\text{MAX. OUTFLOW} = f(C_t) d^{2.5}$$

REF: MILITARY HYDROLOGY BULLETIN NO. 9

"FLOW THROUGH A BREACHED DAM"

CORPS OF ENGINEERS, JUNE 1957

$$C_t = \frac{bt}{2d} = \frac{10.3}{2(10.3)} = 0.5$$

FROM PLATE NO. 2

$$\text{FOR } C_t = 0.5, f(C_t) = \frac{Q_{\text{MAX}}}{d^{2.5}} = 1.2$$

$$Q_{\text{MAX}} = 1.2 d^{2.5} = 1.2 \times 10.3^{2.5} = 408.58 \text{ CFS} \quad \boxed{\text{SAY } 410 \text{ CFS}}$$

$$\begin{aligned} \text{TIME TO DRAIN} &= \frac{\text{VOL.}}{\frac{1}{2} Q_{\text{MAX}}} = \frac{559,100 \text{ CF}}{\frac{1}{2}(400)} = 2727.3 \text{ SEC} \\ &= 45.46 \text{ MIN.} \quad \boxed{\text{SAY } 46 \text{ MIN.}} \end{aligned}$$

INUNDATION MAPS
DINGEE RESERVOIR
SECTION - ELEV. - VELOCITY - DISCHARGE

S.P.D.
PMF

3-10-75
4/4/75

RESERVOIR=DINGEE
SECTION =HARBOR DR NEAR MCANDREW DR
BED EL =670

NO. OF TRIAL DEPTHS =2

SLOPE=.111

MANNINGS N=.04

671,50,52,672,100,54

ELEV FT	VEL. FPS	FLOW CFS
671	12.090006	604.50032
672	18.718935	1871.8935

SECTION =MORAGA AVE AT PIEDMONT CITY LIMITS

BED EL =498

NO. OF TRIAL DEPTHS =2

SLOPE=.056

MANNINGS N=.04

499,110,112,500,220,114

ELEV FT	VEL. FPS	FLOW CFS
499	8.7096518	958.06169
500	13.666606	3006.6534

SECTION =MORAGA AVE NEAR PALA AVE

BED EL =385

NO. OF TRIAL DEPTHS =2

SLOPE=.02

MANNINGS N=.04

386,105,107,387,210,109

ELEV FT	VEL. FPS	FLOW CFS
386	5.2020624	546.21655
387	8.1582699	1713.2367



INUNDATION MAPS
DINGEE RESERVOIR
BREACH FLOW PATH

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BREACH FLOW WILL TRAVERSE THE TOPOGRAPHIC
PATH DESCRIBED IN DETAIL (SHEET 1 AND 2) EARLIER AS
FOLLOWS:

BREACH SECTION IN RESERVOIR, ACROSS ESTATES DRIVE →
HARBOR DRIVE → MORAGA AVENUE → DETENTION
BASINS IN MOUNTAIN VIEW CEMETERY.

BREACH FLOW WILL REACH LAKE MERRITT VIA PARTIALLY
CULVERTED GLEN ECHO CREEK AT A MODERATE RATE OF FLOW
CONTROLLED BY DETENTION BASINS IN MOUNTAIN
VIEW CEMETERY. LAKE MERRITT OUTLETS TO THE
INNER HARBOR BORDERING ALAMEDA.



INUNDATION MAPS
DINGEE RESERVOIR
TRAVEL TIME CALCULATIONS

SPD
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3-10-75
4/4/75

THE FOLLOWING COMPUTATIONS REPRESENT THE
FLOOD WAVE TRAVEL TIME TO VARIOUS POINTS ALONG THE
BREACH FLOW PATH.

$$\text{TIME} = \frac{\text{DISTANCE}}{\text{AVG. VELOCITY}}$$

LOCATION	DISTANCE (FT)	VELOCITY (FPS)	AVG. VEL. (FPS)	TRAVEL TIME Δ (MIN) Σ
DINGEE RESERVOIR		7.5		
	350		9.0	.65
HARBORD DRIVE NEAR MCANDREW DR.		10.5 ^{1 3/4}		.65
	1700		8.35	3.39
MORAGA AVE AT PIEDMONT CITY LIMITS		6.2 ^{1 1/2 3/4}		4.04
	2000		5.5	6.06
MORAGA AVE NEAR PALA AVE. - END OF INUNDATION AREA		4.8 ^{3 1/4 1 1/2}		10.1