

Volume 2 - Appendices

EAST BAY MUNICIPAL UTILITY DISTRICT WEST OF HILLS NORTHERN PIPELINES PROJECT

Draft Environmental Impact Report

Prepared for
East Bay Municipal Utility District

May 2013



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May 2013



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APPENDIX A

Public Involvement

Public Review under CEQA

Public involvement is an essential feature of the California Environmental Quality Act (CEQA) process. The CEQA environmental review process has greatly expanded the opportunities for interested citizens to participate in project planning and government decision-making. CEQA encourages public involvement as early as possible in the project planning phase. The Environmental Impact Report (EIR) is a well-established tool to evaluate and define a broad variety of projects, including the proposed West of Hills Northern Pipelines Project. EBMUD's outreach efforts for the Project, described below, exceed CEQA requirements.

Public Involvement for the Project

EBMUD has provided and will continue to provide opportunities for the public to participate in the CEQA process through meetings, public notices on and public review of the Draft EIR, an additional public meeting, and preparation of the Final EIR. A summary of the public involvement process to date is provided below.

EBMUD held a total of three community meetings in the cities of Berkeley, El Cerrito and San Pablo to involve the public in the West of Hills Northern Pipelines Project, prior to initiating preparation of the EIR. Community meeting dates and locations were:

November 9, 2011 Willard Middle School, 2425 Stuart Street, Berkeley, CA.

November 16, 2011 El Cerrito High School, 540 Ashbury Avenue, El Cerrito, CA.

November 30, 2011 Maple Hall, 1 Alvarado Square, San Pablo, CA.

At the meeting in the City of Berkeley, the project team presented an overview of the project background, objectives, pipeline alignment and construction process. Members of the community had questions regarding the pipeline alignment and construction schedule. They also expressed concerns regarding pipeline leakage, impacts to home access and traffic control during construction. EBMUD took note of the concerns for consideration in the EIR.

At the meeting in the City of El Cerrito, the project team again presented an overview of the project background, objectives, pipeline alignment and construction process. Members of the community had questions regarding the pipeline alignment, safety issues, construction schedule and street paving. One resident expressed particular concern regarding the traffic impacts resulting from construction activities along Richmond Street. EBMUD took note of the concerns for consideration in the EIR.

No members of the public attended the meeting in the City of San Pablo.

EIR Process

Once the Draft EIR is completed, and in conjunction with circulating the Notice of Availability and Draft EIR to agencies, community residents and interested parties, the Draft EIR will be posted on EBMUD's website, to provide opportunities for public review.

EBMUD has attempted in good faith to involve the public in reviewing and commenting on the proposed Project. At each stage of the environmental review process, EBMUD has invited (and continues to invite) the public to provide input. EBMUD welcomes and encourages comments concerning the Project and respects the input that members of the community have to offer.

APPENDIX B

Notice of Preparation

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Notice of Completion & Environmental Document Transmittal

Mail to: State Clearinghouse, P.O. Box 3044, Sacramento, CA 95812-3044 (916) 445-0613

For Hand Delivery/Street Address: 1400 Tenth Street, Sacramento, CA 95814

SCH #2012022068

Project Title: West of Hills Northern Pipelines Project

Lead Agency: East Bay Municipal Utility District

Mailing Address: 375 Eleventh Street, MS 701

City: Oakland

Zip: 94607

Contact Person: Timothy McGowan

Phone: (510) 287-1981

County: Alameda

Project Location: County: Alameda and Contra Costa

City/Nearest Community: Berkeley, ElCerrito, Richmond, San Pablo

Cross Streets: _____

Zip Code: _____

Longitude/Latitude (degrees, minutes and seconds): _____° _____' _____" N / _____° _____' _____" W Total Acres: _____

Assessor's Parcel No.: _____

Section: _____ Twp.: _____ Range: _____ Base: _____

Within 2 Miles: State Hwy #: 123

Waterways: San Francisco Bay

Airports: No

Railways: BART, SP

Schools: Yes

Document Type:

CEQA: NOP Draft EIR
 Early Cons Supplement/Subsequent EIR
 Neg Dec (Prior SCH No.) _____
 Mit Neg Dec Other: _____

NEPA: NOI Other: Joint Document
 EA Final Document
 Draft EIS Other: _____
 FONSI

Local Action Type:

General Plan Update Specific Plan
 General Plan Amendment Master Plan
 General Plan Element Planned Unit Development
 Community Plan Site Plan

Rezone Prezone Use Permit
 Annexation Redevelopment
 Coastal Permit Other:
 Land Division (Subdivision, etc.)
STATE CLEARING HOUSE

RECEIVED

FEB 27 2012

Development Type:

Residential: Units _____ Acres _____
 Office: Sq.ft. _____ Acres _____ Employees _____
 Commercial: Sq.ft. _____ Acres _____ Employees _____
 Industrial: Sq.ft. _____ Acres _____ Employees _____
 Educational: _____
 Recreational: _____
 Water Facilities: Type Pipelines MGD n/a

Transportation: Type _____
 Mining: Mineral _____
 Power: Type MW _____
 Waste Treatment: Type MGD _____
 Hazardous Waste: Type _____
 Other: _____

Project Issues Discussed in Document:

| | | | |
|--|--|---|--|
| <input checked="" type="checkbox"/> Aesthetic/Visual | <input type="checkbox"/> Fiscal | <input checked="" type="checkbox"/> Recreation/Parks | <input checked="" type="checkbox"/> Vegetation |
| <input type="checkbox"/> Agricultural Land | <input checked="" type="checkbox"/> Flood Plain/Flooding | <input type="checkbox"/> Schools/Universities | <input checked="" type="checkbox"/> Water Quality |
| <input checked="" type="checkbox"/> Air Quality | <input type="checkbox"/> Forest Land/Fire Hazard | <input type="checkbox"/> Septic Systems | <input checked="" type="checkbox"/> Water Supply/Groundwater |
| <input checked="" type="checkbox"/> Archeological/Historical | <input checked="" type="checkbox"/> Geologic/Seismic | <input type="checkbox"/> Sewer Capacity | <input checked="" type="checkbox"/> Wetland/Riparian |
| <input checked="" type="checkbox"/> Biological Resources | <input type="checkbox"/> Minerals | <input checked="" type="checkbox"/> Soil Erosion/Compaction/Grading | <input checked="" type="checkbox"/> Growth Inducement |
| <input type="checkbox"/> Coastal Zone | <input type="checkbox"/> Noise | <input type="checkbox"/> Solid Waste | <input checked="" type="checkbox"/> Land Use |
| <input checked="" type="checkbox"/> Drainage/Absorption | <input checked="" type="checkbox"/> Population/Housing Balance | <input type="checkbox"/> Toxic/Hazardous | <input checked="" type="checkbox"/> Cumulative Effects |
| <input type="checkbox"/> Economic/Jobs | <input checked="" type="checkbox"/> Public Services/Facilities | <input type="checkbox"/> Traffic/Circulation | <input type="checkbox"/> Other: _____ |

Present Land Use/Zoning/General Plan Designation:

Primarily developed within existing streets; also Open Space/Parks/Recreation, and Multi-Family Res/Med. Density Residential.

Project Description: (please use a separate page if necessary)

The project involves the construction and operation of four transmission pipeline segments in western Alameda and Contra Costa Counties - a proposed 1.5 mile long, 48-inch diameter pipeline in the City of Berkeley; a proposed 36-inch diameter, 2.5 mile long pipeline in the City of El Cerrito; a proposed 36-inch diameter, 2.5 mile long pipeline in the Cities of El Cerrito and Richmond; and a proposed 36-inch diameter, 1.9 mile long pipeline in the Cities of Richmond and San Pablo. The proposed pipeline routes are located within existing city streets and on non-street properties owned by EBMUD and City of San Pablo.

Note: The State Clearinghouse will assign identification numbers for all new projects. If a SCH number already exists for a project (e.g. Notice of Preparation or previous draft document) please fill in.

Reviewing Agencies Checklist

Lead Agencies may recommend State Clearinghouse distribution by marking agencies below with an "X". If you have already sent your document to the agency please denote that with an "S".

- | | | | |
|--|--|-----------------|--|
| <input type="checkbox"/> S Air Resources Board | <input type="checkbox"/> S Office of Historic Preservation | | |
| <input type="checkbox"/> Boating & Waterways, Department of | <input type="checkbox"/> Office of Public School Construction | | |
| <input type="checkbox"/> California Emergency Management Agency | <input type="checkbox"/> Parks & Recreation, Department of | | |
| <input type="checkbox"/> California Highway Patrol | <input type="checkbox"/> Pesticide Regulation, Department of | | |
| <input type="checkbox"/> S Caltrans District # <u>4</u> | <input checked="" type="checkbox"/> X Public Utilities Commission | | |
| <input type="checkbox"/> Caltrans Division of Aeronautics | <input type="checkbox"/> S Regional WQCB # <u>2</u> | | |
| <input type="checkbox"/> Caltrans Planning | <input type="checkbox"/> Resources Agency | | |
| <input type="checkbox"/> Central Valley Flood Protection Board | <input type="checkbox"/> Resources Recycling and Recovery, Department of | | |
| <input type="checkbox"/> Coachella Valley Mtns. Conservancy | <input type="checkbox"/> S.F. Bay Conservation & Development Comm. | | |
| <input type="checkbox"/> Coastal Commission | <input type="checkbox"/> San Gabriel & Lower L.A. Rivers & Mtns. Conservancy | | |
| <input type="checkbox"/> Colorado River Board | <input type="checkbox"/> San Joaquin River Conservancy | | |
| <input type="checkbox"/> Conservation, Department of | <input type="checkbox"/> Santa Monica Mtns. Conservancy | | |
| <input type="checkbox"/> Corrections, Department of | <input type="checkbox"/> State Lands Commission | | |
| <input type="checkbox"/> Delta Protection Commission | <input type="checkbox"/> SWRCB: Clean Water Grants | | |
| <input type="checkbox"/> Education, Department of | <input type="checkbox"/> SWRCB: Water Quality | | |
| <input type="checkbox"/> Energy Commission | <input type="checkbox"/> SWRCB: Water Rights | | |
| <input type="checkbox"/> S Fish & Game Region # <u>3</u> | <input type="checkbox"/> Tahoe Regional Planning Agency | | |
| <input type="checkbox"/> Food & Agriculture, Department of | <input type="checkbox"/> Toxic Substances Control, Department of | | |
| <input type="checkbox"/> Forestry and Fire Protection, Department of | <input type="checkbox"/> Water Resources, Department of | | |
| <input type="checkbox"/> General Services, Department of | | | |
| <input type="checkbox"/> Health Services, Department of | | | |
| <input type="checkbox"/> Housing & Community Development | | | |
| <input type="checkbox"/> S Native American Heritage Commission | | | |
| <hr style="border-top: 1px dashed black;"/> | | | |
| Local Public Review Period (to be filled in by lead agency) | | | |
| Starting Date | <u>February 27, 2012</u> | Ending Date | <u>March 29, 2012</u> |
| <hr style="border-top: 1px dashed black;"/> | | | |
| Lead Agency (Complete if applicable): | | | |
| Consulting Firm: | <u>ESA</u> | Applicant: | <u>East Bay Municipal Utility District</u> |
| Address: | <u>350 Frank H. Ogawa Plaza</u> | Address: | <u>375 Eleventh Street, MS 701</u> |
| City/State/Zip: | <u>Oakland, CA 94612</u> | City/State/Zip: | <u>Oakland, CA 94607</u> |
| Contact: | <u>Josh Ferris</u> | Phone: | <u>(510) 287-1981</u> |
| Phone: | <u>(510) 366-9019</u> | | |
| <hr style="border-top: 1px dashed black;"/> | | | |
| Signature of Lead Agency Representative: | <u></u> | | Date: <u>02/24/2012</u> |

Authority cited: Section 21083, Public Resources Code. Reference: Section 21161, Public Resources Code.

**NOTICE OF PREPARATION
ENVIRONMENTAL IMPACT REPORT
WEST OF HILLS NORTHERN PIPELINES PROJECT
EAST BAY MUNICIPAL UTILITY DISTRICT**
February 27, 2012

To Responsible Agencies and Interested Parties:

The East Bay Municipal Utility District (EBMUD), acting as lead agency under the California Environmental Quality Act (CEQA), is preparing a project-level environmental impact report (EIR) for the West of Hills Northern Pipelines Project. This Notice of Preparation (NOP) EBMUD requests your input regarding the scope and content of the environmental information that should be considered or included in the EIR and that is germane to your agency's statutory responsibilities in connection with the project. CEQA requires that your response be submitted to EBMUD at the earliest possible date, but not later than March 29, 2012. Responses to or questions regarding this NOP should be directed to:

Timothy McGowan, Associate Civil Engineer, Project Manager
East Bay Municipal Utility District
375 Eleventh Street, MS 701
Oakland, CA 94607
(510) 287-1981, tmcgowan@ebmud.com

Project Purpose: The West of Hills Northern Pipelines Project is needed to ensure continued reliable water service to customers located west of the Oakland-Berkeley Hills and north of the Claremont Tunnel terminus in Berkeley. The customers served include parts of north Oakland, Berkeley, Albany, El Cerrito, Richmond, San Pablo, Pinole, Hercules and the unincorporated communities of West Contra Costa including Crockett. The purpose of the West of Hills Northern Pipelines Project is to correct existing deficiencies in water transmission and storage operations, meet future water demands, improve system reliability and water quality challenges, and facilitate repair and replacement of aging infrastructure.

Project Location and Description: The project involves the construction and operation of four transmission pipeline segments in Alameda and Contra Costa Counties (see **Figure 1**). The proposed pipeline routes are located within existing city streets and on non-street properties owned by EBMUD and the City of San Pablo. The exact placement of the pipelines within selected roadways is not presently known for all segments.

- ***Wildcat Pipeline (Berkeley)***. This proposed pipeline, 48 inches in diameter and approximately 1.5 miles long, would be located in the City of Berkeley, Alameda County (see **Figure 2**). An alternative alignment for a segment of this pipeline, located in Benvenue Avenue, is under consideration and will be evaluated in the EIR.
- ***Wildcat Pipeline (El Cerrito)***. This proposed pipeline, 36 inches in diameter and approximately 2.5 miles long, would be located in the City of El Cerrito, Contra Costa County (see **Figure 3**).
- ***Central Pressure Zone Pipeline (El Cerrito/Richmond)***. This proposed pipeline, 36 inches in diameter and approximately 2.5 miles long, would be located in San Pablo Avenue in the Cities of El Cerrito and Richmond, Contra Costa County (see **Figure 3**).

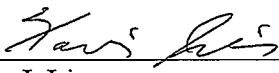
- **Central Pressure Zone Pipeline (Richmond/San Pablo).** This proposed pipeline, 36 inches in diameter and approximately 1.9 miles long, would be located primarily in 23rd Street in the Cities of Richmond and San Pablo, Contra Costa County (see **Figure 4**). At San Pablo Creek, the pipeline would be constructed within an existing EBMUD utility corridor consisting of two EBMUD-owned properties (assessor parcels 411-282-002 and 412-300-001, totaling 0.28 acres) located between Brookside Drive and Road 20 in San Pablo. An alternative alignment at San Pablo Creek (near San Pablo Avenue) is under consideration and will be evaluated in the EIR. This alternative alignment would be developed partly within a parcel owned by the City of San Pablo (assessor parcel 411-282-001).

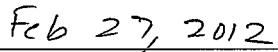
For the most part, construction of the pipelines would be by conventional open trench construction methods. Where the Central Pressure Zone Pipeline (Richmond/San Pablo) crosses San Pablo Creek, EBMUD proposes to construct a pipe bridge and trenchless (“bore and jack”) construction is proposed where the Central Pressure Zone Pipeline (Richmond/San Pablo) crosses Wildcat Creek. At Wildcat Creek, a vacant parcel (assessor parcel 411-281-015) owned by the City of San Pablo and intended for park development may be used to locate the entry pit for the bore and jack crossing of the Creek.

Construction would typically occur between 8 a.m. and 7 p.m. Longer construction hours (up to 24 hours per day) may be required where the proposed pipelines connect with existing pipelines to minimize customer water service disruption. Lane and roadway closures would be required during construction hours, with access restored during non-working hours. Construction of both Wildcat Pipeline segments would occur first and over a 9 to 14 month period from approximately January 2015 to June 2016. Construction of both Central Pressure Zone Pipeline segments would occur over a 10 to 16 month beginning in 2021.

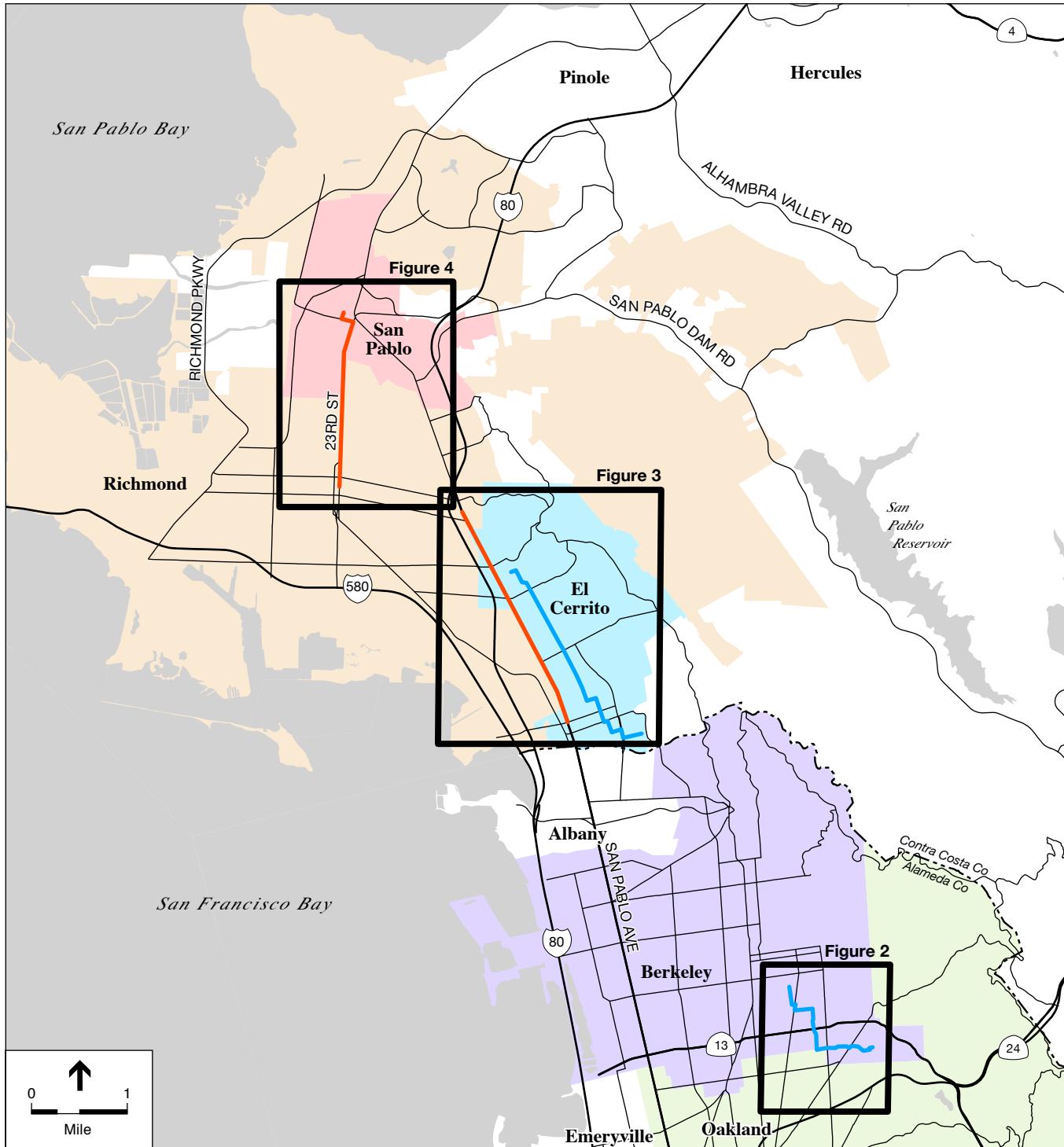
Probable Environmental Effects. Based on an Initial Study completed for the project, the environmental factors that could potentially be affected by this project (i.e. involving at least one impact that is a “Potentially Significant Impact”) include aesthetics, air quality, biological resources, cultural resources, geology/soils, greenhouse gas emissions, hazards/hazardous materials, hydrology/water quality, noise, recreation, transportation/traffic, and utilities/service systems. To review the Initial Study prepared for the project, please go to EBMUD’s project website at: <http://www.ebmud.com/about-ebmud/news/project-updates/west-hills-northern-pipelines-project>.

CEQA Process. The Draft EIR is targeted for circulation in late 2012, with action by EBMUD’s Board of Directors anticipated in the Spring of 2013. Notice will be given of public meetings. At the end of the review and comment process, EBMUD’s Board of Directors will determine whether to certify the EIR and approve the West of Hills Northern Pipelines Project. Additional information about the West of Hills Northern Pipelines Project can be obtained from the EBMUD website


Xavier J. Irias
Director, Engineering and Construction
East Bay Municipal Utility District


Date

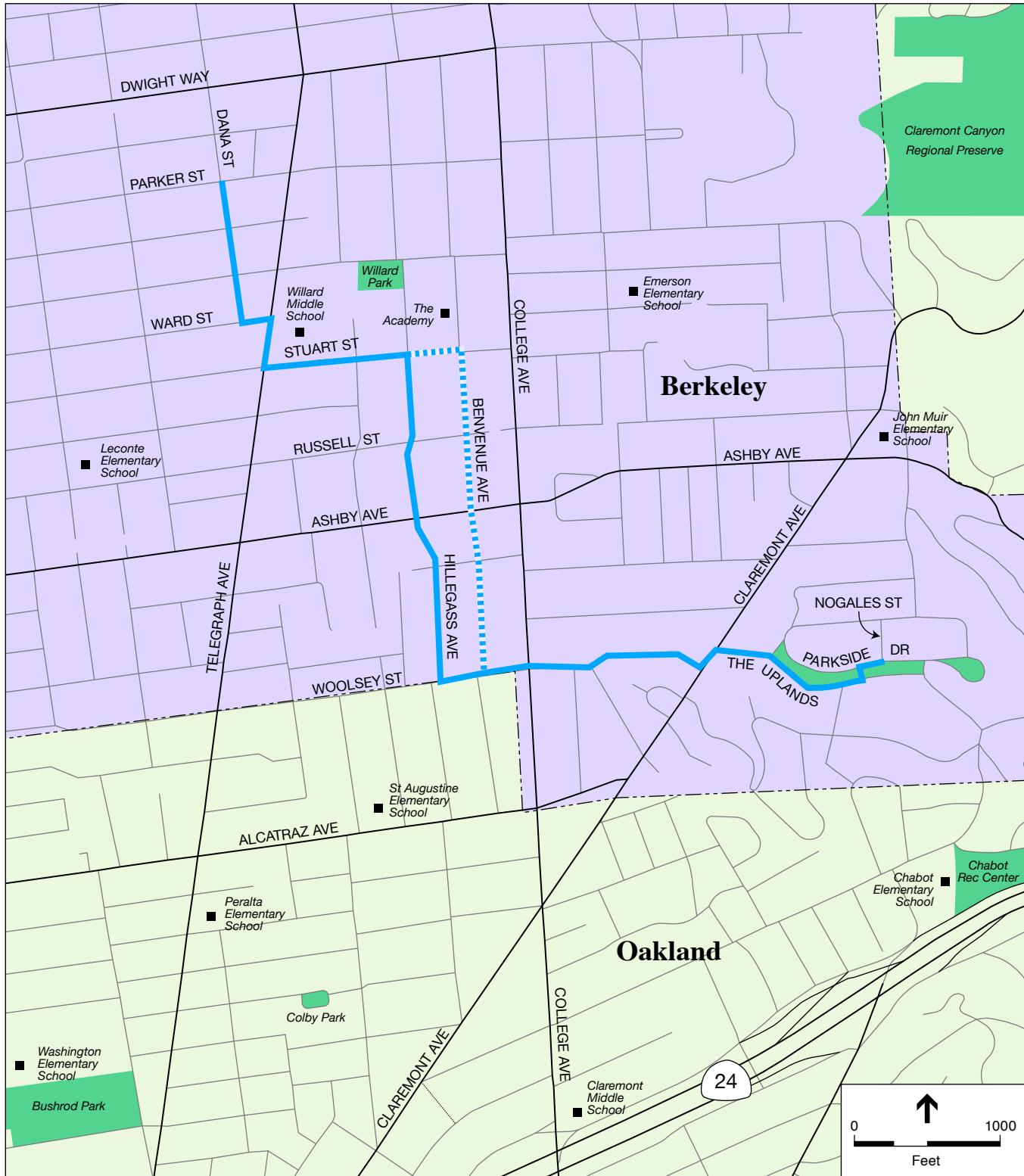
Figures/Maps:



SOURCE: ESA

EBMUD West of Hills Northern Pipelines . 211488

Figure 1
Project Location

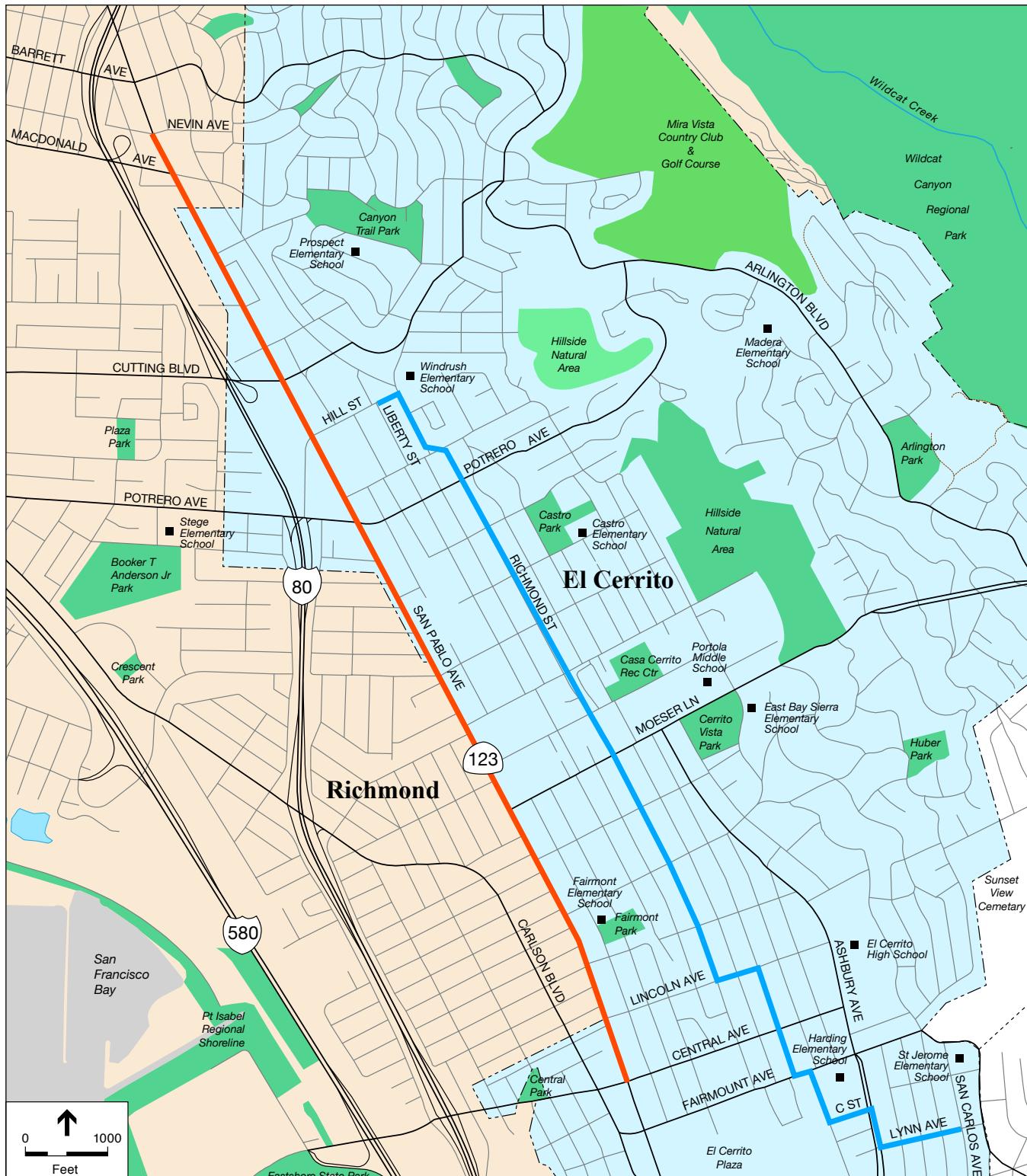


- Wildcat Pipeline (Berkeley)
···· Alternative Alignment (Benvenue Ave)

SOURCE: ESA

EBMUD West of Hills Northern Pipelines . 211488

Figure 2
Wildcat Pipeline (Berkeley)



Wildcat Pipeline (El Cerrito)

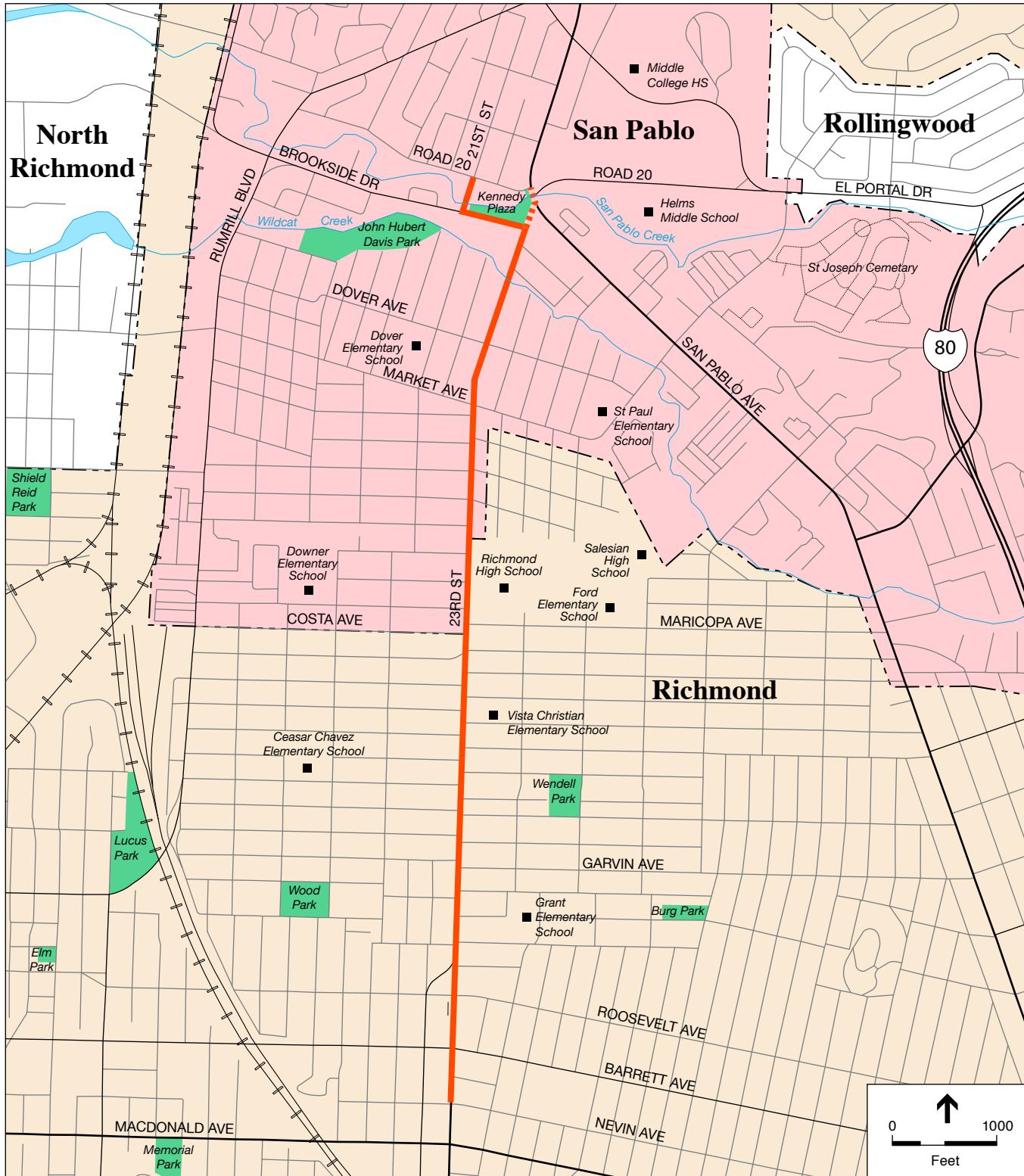
Central Pressure Zone Pipeline (El Cerrito/Richmond)

SOURCE: ESA

EBMUD West of Hills Northern Pipelines . 211488

Figure 3

Wildcat Pipeline (El Cerrito) and
Central Pressure Zone Pipeline (El Cerrito/Richmond)



— Central Pressure Zone Pipeline (Richmond/San Pablo)

···· Alternative Alignment

SOURCE: ESA

EBMUD West of Hills Northern Pipelines . 211488

Figure 4

Central Pressure Zone Pipeline
(Richmond/San Pablo)

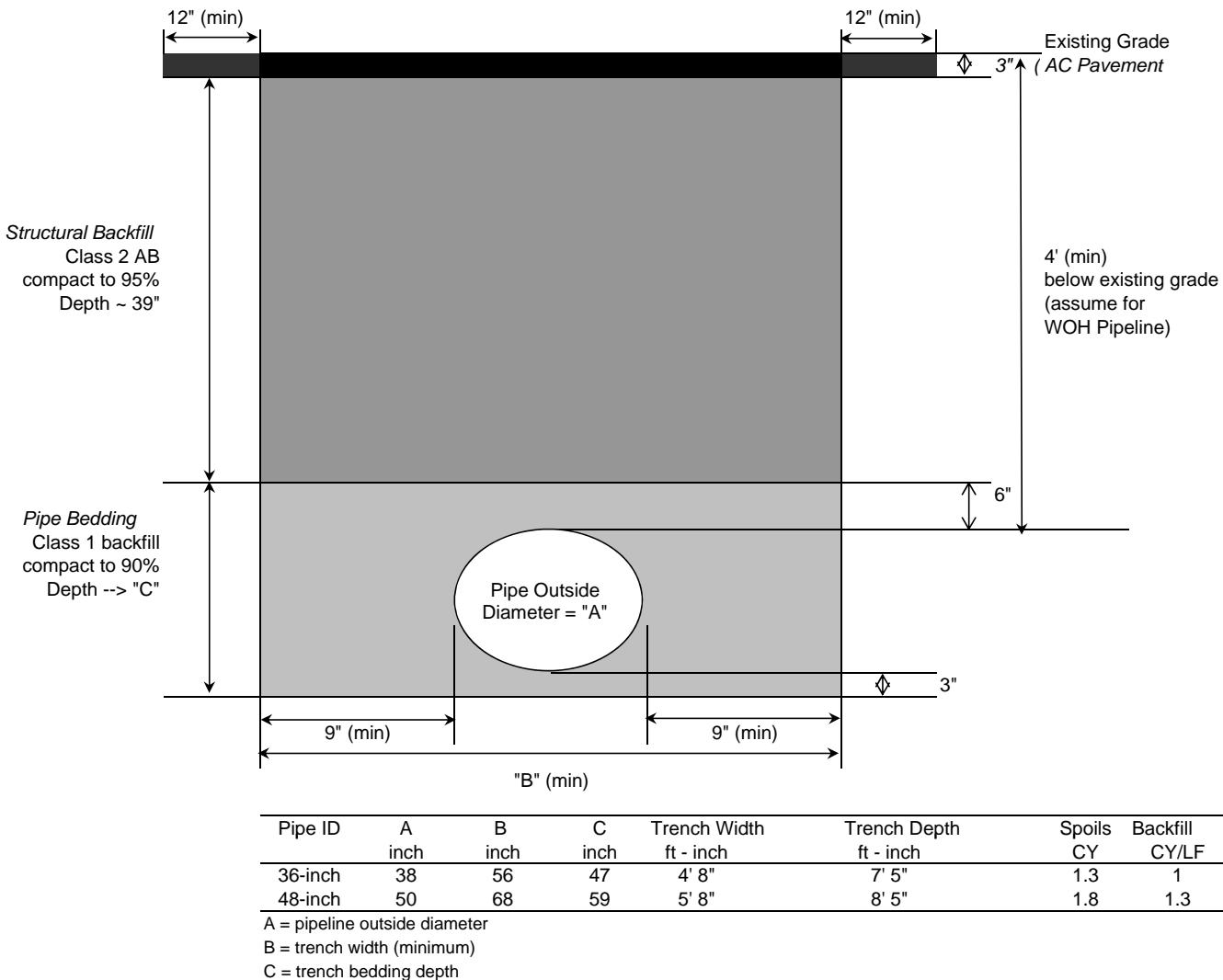
APPENDIX C

Construction Details

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Typical Trench Section: NTS

References: 1) EBMUD Std Dwg 1992-A, & 2) Utility Trench Master Permit Conditions - Exhibit A



Paving Requirement:

Per discussion with EBMUD Paving Crew foreman, AC paving thickness is 6" (Typ)

| Pipe ID | AC Thickness (typ), inch | Width | Volume, ft ³ /LF | Volume, CY/LF | Remarks |
|---------|--------------------------------|-------|--------------------------------|------------------|--|
| 36-inch | 6 | 56 | 3.3 | 0.12 | Volume is for 6" thick AC |
| 48-inch | 6 | 68 | 3.8 | 0.14 | Volume is for 6" thick AC |
| 36-inch | 12 | 56 | 6.7 | 0.25 | Volume is for 1' thick AC (e.g. along San Pablo Ave, per Caltrans trench details provided to City of Richmond Sewer Replacement Project) |

| Pipeline | City | Contractor's Work Force | | | | | | Other Work Force | | | | Total | | |
|--|----------------------|-------------------------|----------------------|------------------|--------------|-----------------------|-----------------|------------------|-----------------|-------------------|------------------|---------------------|---|-----------|
| | | Foreman | Workers ¹ | HEO ² | Truck Driver | Flaggers ³ | Crane Operators | Crew subtotal | Super-intendent | EBMUD's Inspector | City's Inspector | Caltrans' Inspector | | |
| <u>Open-Cut Trenching Method</u> | | | | | | | | | | | | | | |
| Wildcat Pipeline (El Cerrito) | El Cerrito | 2 | 9 | 4 | 2 | 4 | na | 21 | 1 | 1 | 1 | 0 | 1 | 25 |
| Wildcat Pipeline (Berkeley) | Berkeley | 2 | 9 | 4 | 2 | 7 | na | 24 | 1 | 1 | 1 | 0 | 1 | 28 |
| Central PZ Pipeline (El Cerrito / Richmond) | El Cerrito/Richmond | 2 | 9 | 4 | 2 | 2 | na | 19 | 1 | 1 | 1 | 1 | 1 | 24 |
| Central PZ Pipeline (Richmond / San Pablo) | Richmond / San Pablo | 2 | 9 | 4 | 3 | 2 | na | 20 | 1 | 1 | 1 | 0 | 1 | 24 |
| Flushing, Pressure Testing, Chlorination | | 2 | 6 | 1 | 0 | 0 | | 9 | 1 | 1 | 1 | | 1 | 13 |
| Hot Tap Connection | | 2 | 4 | 1 | 0 | 2 | | 9 | 1 | 1 | 1 | | 1 | 13 |
| Paving (per EBMUD Paving Section Foreman) | | 1 | 3 | 1 | 2 | 2 | | 9 | 1 | 1 | 1 | | 1 | 13 |
| <u>Jack & Bore Method</u> | | | | | | | | | | | | | | |
| J&B - Pits Excavation / Backfill | | 1 | 2 | 1 | 0 | 2 | na | 6 | 1 | 1 | | | 1 | 9 |
| J&B - Casing Installation | | 1 | 3 | 1 | 0 | 2 | 1 | 8 | 1 | 1 | | | 1 | 11 |
| J&B - Pipeline Installation | | 2 | 6 | 1 | 0 | 2 | 1 | 12 | 1 | 1 | | | 1 | 15 |
| <u>Pipe Bridge Method</u> | | | | | | | | | | | | | | |
| Clear and Grubbing | | 1 | 2 | 2 | 0 | 0 | 0 | 5 | 1 | 1 | | | 1 | 8 |
| Pipe Bridge Abutment 3' W x 4' D x 10'L each; 6" above grade | | 1 | 2 | 1 | 0 | 0 | 0 | 4 | 1 | 1 | | | 1 | 7 |
| Pipe Bridge Erection | | 1 | 3 | 0 | 0 | 2 | 2 | 8 | 1 | 1 | | | 1 | 11 |
| Install Pipeline on Pipe Bridge | | 1 | 2 | 0 | 0 | 0 | 2 | 5 | 1 | 1 | 1 | | 1 | 9 |

¹ Include plumbers and welder for pipeline installation, for paving include rakers.

² HEO = Heavy Equipment Operator

³ Traffic control / director detour. Number of flaggers required is site specific.

Work force estimate for open-cut pipeline installation per discussion with TRM (based on his experience on construction projects)

Work force estimate for paving per discussion with EBMUD Paving Section Foreman

Wildcat Pipeline (Berkeley) - Preferred Alignment (Alternative 4)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis.

| Reach | Construction Phase | Pipe length (LF) | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-------|---|------------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - Parkside / Nogales to Uplands / Claremont Ave via Parkside Dr & the Uplands. | 1,240 | 48 | 80 | 3.1 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 2 | Phase 2 - Uplands / Claremont to Hillegass Ave/Woolsey St via Claremont Ave, & Woolsey St. | 2,100 | 48 | 80 | 5.3 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 3 | Phase 3 - Hillegass/Woolsey to Hillegass Ave/Russell St via Hillegass Ave. | 1,700 | 48 | 80 | 4.3 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 4 | Phase 4 - Hillegass/Russell to Hillegass Ave/Stuart Ave via Hillegass Ave. | 640 | 48 | 80 | 1.6 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 5 | Phase 5 - Hillegass/Stuart Ave to Parker St / Dana St via Stuart St, Telegraph Ave, Ward St, | 2,550 | 48 | 80 | 6.4 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| | Phase 6 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 13 | 32 | 1 13 Trucks Vehicles |
| | Phase 7 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 13 | 34 | 1 13 Trucks Vehicles |
| | Phase 8 - Paving | 8,230 | na | 700 | 2.4 | 11 | 0 | 13 | 48 | 3 13 Trucks Vehicles |
| | Total | 8,230 | LF of pipe | | 32 weeks | | | | | |
| | Total Excavated Material | 14,814 | CY | | | | MAXIMUM TRIPS = | 88 | 4 28 Trucks Vehicles | |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 48-inch Wildcat Pipeline (Berkeley) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 48-inch (ID) pipe is typically 5 feet 8 inches wide and 8 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.8 cubic yard (CY) of excavated spoil and require 1.3 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & seven flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 48-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
3 material trucks per day
4. Material truck trips per day include deliveries of pipeline (1), appurtenance (1), and equipment (1), which is
5. Worker vehicle trips for pipeline installation consist of crew (24), contractor's superintendent (1), District's inspector (1), City's inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Wildcat Pipeline (Berkeley) - Preferred Alignment (Benvenue Avenue Option)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis.

| Segment | Construction Phase | Pipe length (LF) | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|---------|--|------------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - Parkside / Nogales to Uplands / Claremont Ave via Parkside Dr & the Uplands. | 1,240 | 48 | 80 | 3.1 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 2A | Phase 2 - Uplands / Claremont to Benvenue Ave / Woolsey St via Claremont Ave, & Woolsey St. | 1,800 | 48 | 80 | 4.5 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 3A | Phase 3 - Benvenue / Woolsey to Benvenue Ave / Russell St via Benvenue Ave. | 1,690 | 48 | 80 | 4.2 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 4A | Phase 4 - Benvenue / Russell to Hillegass Ave/Stuart Ave via Benvenue Ave & Stuart St. | 920 | 48 | 80 | 2.3 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| 5 | Phase 5 - Hillegass/Stuart Ave to Parker St / Dana St via Stuart St, Telegraph Ave, Ward St, | 2,550 | 48 | 80 | 6.4 | 13 | 3 | 28 | 88 | 4 28 Trucks Vehicles |
| | Phase 6 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 13 | 32 | 1 13 Trucks Vehicles |
| | Phase 7 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 13 | 34 | 1 13 Trucks Vehicles |
| | Phase 7 - Paving | 8,200 | na | 700 | 2.3 | 11 | 0 | 13 | 48 | 3 13 Trucks Vehicles |
| | Total | 8,200 | LF of pipe | | 32 weeks | | | | | |
| | Total Excavated Material | 14,760 | CY | | | | MAXIMUM TRIPS = | | 88 | 4 28 Trucks Vehicles |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 48-inch Wildcat Pipeline (Berkeley) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 48-inch (ID) pipe is typically 5 feet 8 inches wide and 8 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.8 cubic yard (CY) of excavated spoil and require 1.3 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & seven flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 48-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
3 material trucks per day
4. Material truck trips per day include deliveries of pipeline (1), appurtenance (1), and equipment (1), which is
5. Worker vehicle trips for pipeline installation consist of crew (24), contractor's superintendent (1), District's inspector (1), City's inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Wildcat Pipeline (Berkeley) - Preferred Alignment (Alternative 4)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis.

| Reach | Construction Phase | Pipe length (LF) | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-------|---|------------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - Parkside / Nogales to Uplands / Claremont Ave via Parkside Dr & the Uplands. | 1,240 | 48 | 200 | 1.2 | 31 | 5 | 28 | 128 | 9 28 |
| 2 | Phase 2 - Uplands / Claremont to Hillegass Ave/Woolsey St via Claremont Ave, & Woolsey St. | 2,100 | 48 | 200 | 2.1 | 31 | 5 | 28 | 128 | 9 28 |
| 3 | Phase 3 - Hillegass/Woolsey to Hillegass Ave/Russell St via Hillegass Ave. | 1,700 | 48 | 200 | 1.7 | 31 | 5 | 28 | 128 | 9 28 |
| 4 | Phase 4 - Hillegass/Russell to Hillegass Ave/Stuart Ave via Hillegass Ave. | 640 | 48 | 200 | 0.6 | 31 | 5 | 28 | 128 | 9 28 |
| 5 | Phase 5 - Hillegass/Stuart Ave to Parker St / Dana St via Stuart St, Telegraph Ave, Ward St, | 2,550 | 48 | 200 | 2.6 | 31 | 5 | 28 | 128 | 9 28 |
| | Phase 6 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 13 | 32 | 1 13 |
| | Phase 7 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 13 | 34 | 1 13 |
| | Phase 6 - Paving | 8,230 | na | 700 | 2.4 | 11 | 0 | 13 | 48 | 3 13 |
| | Total | 8,230 | LF of pipe | | 20 weeks | | | | | |
| | Total Excavated Material | 14,814 | CY | | | | | | 128 | 9 28 |
| | | | | | | | | | | Trucks Vehicles |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 48-inch Wildcat Pipeline (Berkeley) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 48-inch (ID) pipe is typically 5 feet 8 inches wide and 8 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.8 cubic yard (CY) of excavated spoil and require 1.3 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & seven flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 48-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
5 material trucks per day
4. Material truck trips per day include deliveries of pipeline (3), appurtenance (1), and equipment (1), which is
5. Worker vehicle trips for pipeline installation consist of crew (24), contractor's superintendent (1), District's inspector (1), City's inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Wildcat Pipeline (Berkeley) - Preferred Alignment (Benvenue Avenue Option)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis.

| Segment | Construction Phase | Pipe length (LF) | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|---------|--|------------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - Parkside / Nogales to Uplands / Claremont Ave via Parkside Dr & the Uplands. | 1,240 | 48 | 200 | 1.2 | 31 | 5 | 28 | 128 | 9 28 Trucks Vehicles |
| 2A | Phase 2 - Uplands / Claremont to Benvenue Ave / Woolsey St via Claremont Ave, & Woolsey St. | 1,800 | 48 | 200 | 1.8 | 31 | 5 | 28 | 128 | 9 28 Trucks Vehicles |
| 3A | Phase 3 - Benvenue / Woolsey to Benvenue Ave / Russell St via Benvenue Ave. | 1,690 | 48 | 200 | 1.7 | 31 | 5 | 28 | 128 | 9 28 Trucks Vehicles |
| 4A | Phase 4 - Benvenue / Russell to Hillegass Ave/Stuart Ave via Benvenue Ave & Stuart St. | 920 | 48 | 200 | 0.9 | 31 | 5 | 28 | 128 | 9 28 Trucks Vehicles |
| 5 | Phase 5 - Hillegass/Stuart Ave to Parker St / Dana St via Stuart St, Telegraph Ave, Ward St, | 2,550 | 48 | 200 | 2.6 | 31 | 5 | 28 | 128 | 9 28 Trucks Vehicles |
| | Phase 6 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 13 | 32 | 1 13 Trucks Vehicles |
| | Phase 7 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 13 | 34 | 1 13 Trucks Vehicles |
| | Phase 6 - Paving | 8,200 | na | 700 | 2.3 | 11 | 0 | 13 | 48 | 3 13 Trucks Vehicles |
| | Total | 8,200 | LF of pipe | | 20 weeks | | | | | |
| | Total Excavated Material | 14,760 | CY | | | | | | 128 | 9 28 Trucks Vehicles |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 48-inch Wildcat Pipeline (Berkeley) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 48-inch (ID) pipe is typically 5 feet 8 inches wide and 8 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.8 cubic yard (CY) of excavated spoil and require 1.3 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & seven flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 48-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
5 material trucks per day
4. Material truck trips per day include deliveries of pipeline (3), appurtenance (1), and equipment (1), which is
5. Worker vehicle trips for pipeline installation consist of crew (24), contractor's superintendent (1), District's inspector (1), City's inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Wildcat Pipeline (El Cerrito) - Preferred Alignment (Alternative 1)

Estimated Vehicle / Truck Trips that project-related activities would generate during construction phase, on both a daily and peak hourly basis.

| Reach | Construction Phase | Pipe length (LF) | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-------|---|------------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - Lynn Avenue / San Carlos Avenue to Richmond Street / Lincoln Avenue via Lynn Avenue, Ashbury Avenue, C Street, Behrens Street, Fairmount Avenue, Norvell Street, & Lincoln Avenue. | 4,830 | 36 | 80 | 12.1 | 10 | 3 | 25 | 76 | 3 25 Trucks Vehicles |
| 2 | Phase 2 - Richmond St / Lincoln Ave to Richmond Street / Schmidt Ln via Richmond Street. | 4,220 | 36 | 80 | 10.6 | 10 | 3 | 25 | 76 | 3 25 Trucks Vehicles |
| 3 | Phase 3 - Richmond St / Schmidt Ln to Hill St / Liberty St via Richmond St, Elm St, & Hill St. | 4,500 | 36 | 80 | 11.3 | 10 | 3 | 25 | 76 | 3 25 Trucks Vehicles |
| | Phase 4 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 28 | 62 | 1 28 Trucks Vehicles |
| | Phase 5 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 24 | 56 | 1 24 Trucks Vehicles |
| | Phase 7 -Paving | 13,550 | na | 700 | 3.9 | 10 | 0 | 12 | 44 | 3 12 Trucks Vehicles |
| | Total | 13,550 | LF of pipe | | 47 | weeks | | | | |
| | Total Excavated Material | 17,615 | CY | | | | MAXIMUM TRIPS = | 76 | 3 25 Trucks Vehicles | |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Wildcat Pipeline (El Cerrito) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & four flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
3 material trucks per day
4. Material truck trips per day include deliveries of pipeline (1), appurtenance (1), and equipment (1), which is
5. Worker vehicle trips for pipeline installation consist of crew (21), contractor's superintendent (1), District's inspector (1), City's inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Wildcat Pipeline (El Cerrito) - Preferred Alignment (Alternative 1)

Estimated Vehicle / Truck Trips that project-related activities would generate during construction phase, on both a daily and peak hourly basis.

| Reach | Construction Phase | Pipe length (LF) | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-------|---|------------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - Lynn Avenue / San Carlos Avenue to Richmond Street / Lincoln Avenue via Lynn Avenue, Ashbury Avenue, C Street, Behrens Street, Fairmount Avenue, Norvell Street, & Lincoln Avenue. | 4,830 | 36 | 200 | 4.8 | 23 | 4 | 25 | 104 | 7 25 |
| 2 | Phase 2 - Richmond St / Lincoln Ave to Richmond Street / Schmidt Ln via Richmond Street. | 4,220 | 36 | 200 | 4.2 | 23 | 4 | 25 | 104 | 7 25 |
| 3 | Phase 3 - Richmond St / Schmidt Ln to Hill St / Liberty St via Richmond St, Elm St, & Hill St. | 4,500 | 36 | 200 | 4.5 | 23 | 4 | 25 | 104 | 7 25 |
| | Phase 4 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 28 | 62 | 1 28 |
| | Phase 5 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 24 | 56 | 1 24 |
| | Phase 7 -Paving | 13,550 | na | 700 | 3.9 | 10 | 0 | 13 | 46 | 3 13 |
| | | | | | | | | | | |
| | Total | 13,550 | LF of pipe | | 27 | weeks | | | | |
| | | | | | | | | | | |
| | Total Excavated Material | 17,615 | CY | | | | MAXIMUM TRIPS = | | 104 | 7 25 |
| | | | | | | | | | | |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Wildcat Pipeline (El Cerrito) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & four flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY -end dump trailer
9 CY - concrete truck
4 material trucks per day
4. Material truck trips per day include deliveries of pipeline (2), appurtenance (1), and equipment (1), which is
5. Worker vehicle trips for pipeline installation consist of crew (21), contractor's superintendent (1), District's inspector (1), City's inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Central Pressure Zone Pipeline (El Cerrito / Richmond) - Preferred Alignment (Alternative 1)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis.

| Reach | Construction Phase | Pipe length | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-------|--|-------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 - San Pablo Ave / Central Ave to San Pablo Ave / Schmidt Ln via San Pablo Ave. | 4,970 | 36 | 80 | 12.4 | 10 | 3 | 24 | 74 | 3 24 Trucks Vehicles |
| 2 | Phase 2 - San Pablo Ave / Schmidt Ln to San Pablo Ave / Potrero Ave via San Pablo Ave. | 2,620 | 36 | 80 | 6.6 | 10 | 3 | 24 | 74 | 3 24 Trucks Vehicles |
| 3 | Phase 3 - San Pablo Ave / Potrero Ave to San Pablo Ave / Hill Street via San Pablo Ave. | 1,200 | 36 | 80 | 3.0 | 10 | 3 | 24 | 74 | 3 24 Trucks Vehicles |
| 4 | Phase 4 - San Pablo Ave / Hill St to San Pablo Ave / Nevin Ave via San Pablo Ave. | 4,130 | 36 | 80 | 10.3 | 10 | 3 | 24 | 74 | 3 24 Trucks Vehicles |
| | Phase 5 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 13 | 32 | 1 13 Trucks Vehicles |
| | Phase 6 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 13 | 34 | 1 13 Trucks Vehicles |
| | Phase 7 - Paving | 12,920 | na | 350 | 7.4 | 10 | 0 | 13 | 46 | 3 13 Trucks Vehicles |
| | | | | | | | | | | |
| | Total | 12,920 | LF of pipe | | 49 | weeks | | | | |
| | Total Excavated Material | 16,796 | CY | | | | | | MAXIMUM TRIPS = 74 | 3 24 Trucks Vehicles |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Central PZ Pipeline (El Cerrito / Richmond) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 12 inches (existing AC along San Pablo Ave is 10 to 14" thick) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & two flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 350 LF of trench with 12" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
3 material trucks per day
4. Material truck trips per day include deliveries of pipeline (1), appurtenance (1), and equipment (1), which is 3 material trucks per day
5. Worker vehicle trips for pipeline installation consist of crew (19), contractor's superintendent (1), District's inspector (1), City's inspector (1), Caltrans' inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Central Pressure Zone Pipeline (El Cerrito / Richmond) - Preferred Alignment (Alternative 1)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis

| Reach | Construction Phase | Pipe length | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-------|--|-------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 | Phase 1 -San Pablo Ave / Central Ave to San Pablo Ave / Schmidt Ln via San Pablo Ave. | 4,970 | 36 | 200 | 5.0 | 23 | 4 | 24 | 102 | 7 24 |
| 2 | Phase 2 - San Pablo Ave / Schmidt Ln to San Pablo Ave / Potrero Ave via San Pablo Ave. | 2,620 | 36 | 200 | 2.6 | 23 | 4 | 24 | 102 | 7 24 |
| 3 | Phase 3 - San Pablo Ave / Potrero Ave to San Pablo Ave / Hill Street via San Pablo Ave. | 1,200 | 36 | 200 | 1.2 | 23 | 4 | 24 | 102 | 7 24 |
| 4 | Phase 4 - San Pablo Ave / Hill St to San Pablo Ave / Nevin Ave via San Pablo Ave. | 4,130 | 36 | 200 | 4.1 | 23 | 4 | 24 | 102 | 7 24 |
| | Phase 5 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 24 | 54 | 1 24 |
| | Phase 6 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 13 | 34 | 1 13 |
| | Phase 7 - Paving | 12,920 | na | 350 | 7.4 | 10 | 0 | 12 | 44 | 3 12 |
| | Total (include intertie) | 12,920 | LF of pipe | | 30 weeks | | | | | |
| | Total Excavated Material | 16,796 | CY | | | | | MAXIMUM TRIPS = | 102 | 7 24 |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Central PZ Pipeline (El Cerrito / Richmond) is Open-Cut Trenching.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 12 inches (existing AC along San Pablo Ave is 10 to 14" thick) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & two flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, & two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 350 LF of trench with 12" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration.
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
4 material trucks per day
4. Material truck trips per day include deliveries of pipeline (2), appurtenance (1), and equipment (1), which is 4 material trucks per day
5. Worker vehicle trips for pipeline installation consist of crew (19), contractor's superintendent (1), District's inspector (1), City's inspector (1), Caltrans' inspector (1), and visitors (1 on average).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.

Central Pressure Zone Pipeline (Richmond_San Pablo) - Preferred Alignment (Alternative 4)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis

| Reach | Construction Phase | Pipe length | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-----------|---|-------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 & 2 | Phase 1 - 23rd St / Nevin Ave to 23rd St / Brookside Dr via 23rd Street. | 8,910 | 36 | 80 | 22.3 | 10 | 3 | 24 | 74 | 3 24 |
| 3 & 4 | Phase 2 - 23rd St / Brookside Dr to RW X574/Brookside. | 670 | 36 | 80 | 1.7 | 10 | 3 | 24 | 74 | 3 24 |
| 3 & 4 | Phase 3 - RW X574/Brookside to RW X574/Road 20. | 305 | 48 | 80 | 0.8 | 13 | 3 | 24 | 80 | 4 24 |
| Part of 2 | Phase 4 - Wildcat Creek Crossing by Jack & Bore Method⁸ | | | | | | | | | |
| | Pits Excavation ⁹ | na | na | na | 2 | 2 | 1 | 9 | 24 | 1 9 |
| | Casing Installation | 170 | 48 | 10 | 3.4 | 1 | 1 | 11 | 26 | 1 11 |
| | Pipeline Installation | 170 | 36 | 50 | 0.7 | 0 | 1 | 15 | 32 | 0.3 15 |
| | Pits Backfill ⁹ | na | na | na | 4 | 1 | 1 | 9 | 22 | 1 9 |
| Part of 3 | Phase 5 - San Pablo Creek Crossing by Pipe Bridge Method | | | | | | | | | |
| | Clear and Grubbing | na | na | na | 1 | 10 | 0 | 8 | 36 | 3 8 |
| | Abutment construction | na | na | na | 2 | 2 | 1 | 7 | 20 | 1 7 |
| | Bridge delivery / erection | na | na | na | 2 days | 0 | 2 | 11 | 26 | 1 11 |
| | Pipeline Installation | 95 | 48 | 50 | 2 days | 0 | 2 | 9 | 22 | 1 9 |
| | Phase 6 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 0 | 6 | 1 0 |
| | Phase 7 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 7 | 22 | 1 7 |
| | Phase 8 - Paving | 9,580 | na | 700 | 2.7 | 10 | 0 | 13 | 46 | 3 13 |
| | Total | 9,845 | LF of pipe | | 51 weeks | | | | | |
| | Total Excavated Material | 12,948 | CY | | | | MATERIAL TRIPS = | 80 | 3 24 | Trucks Vehicles |
| | | | | | | | | | | |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Central PZ Pipeline (Richmond / San Pablo) is Open-Cut Trenching, except at Wildcat Creek & San Pablo Creek crossing
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each lineal foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & two flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, and two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
4. Material truck trips for open-cut trench pipeline installation include deliveries of pipeline (1), appurtenance (1), and equipment (1) 3 material truck per day
5. Worker vehicle trips for pipeline installation consist of crew (20), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitors (1 on avg).
Worker vehicle trips for pits excavation & backfill consist of crew (6), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitor (1).
Worker vehicle trips for pipe bridge abutments construction consist of crew (4), contractor's superintendent (1), District's inspector (1), & City's inspector (1)
Worker vehicle trips for pipe bridge erection consist of crew (8), contractor's superintendent (1), District's inspector (1), & City's inspector (1)
Worker vehicle trips for installation pipe to pipe bridge consist of crew (5), contractor's superintendent (1), District's inspector (1), & City's inspector (1)
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.
8. Jack and bore method production rates based on Hesperian Boulevard Pipeline Relocation Project (Spec 2020).
9. Insertion pit approximately 36 ft long by 13 ft wide by 19 ft deep and receiving pit approximately 13 ft long by 9 ft wide by 16 feet deep.
Wildcat Creek is ~ 8 ft deep per 2' contours. Receiving pit depth is 8 ft below creek bottom, slope of pipeline between jacking pit and receiving pit is 2% up.

Central Pressure Zone Pipeline (Richmond_San Pablo) - Preferred Alignment (San Pablo Avenue Option)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis

| Segment | Construction Phase | Pipe length | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-----------|---|-------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 & 2 | Phase 1 - 23rd St / Nevin Ave to 23rd St / Brookside Dr via 23rd Street. | 8,910 | 36 | 80 | 22.3 | 10 | 3 | 24 | 74 | 3 24 |
| 3 & 4 | Phase 2A - 23rd St / Brookside Dr to Road 20 via 23rd St, San Pablo Avenue, as well as parcels 411-282-001 & 412-300-010 owned by City of San Pablo. | 475 | 36 | 80 | 1.2 | 10 | 3 | 24 | 74 | 3 24 |
| Part of 2 | Phase 4 - Wildcat Creek Crossing by Jack & Bore Method ⁸ | | | | | | | | | |
| | Pits Excavation ⁹ | na | na | na | 2 | 2 | 1 | 9 | 24 | 1 9 |
| | Casing Installation | 170 | 48 | 10 | 3.4 | 1 | 1 | 11 | 26 | 1 11 |
| | Pipeline Installation | 170 | 36 | 50 | 0.7 | 0 | 1 | 15 | 32 | 0.3 15 |
| | Pits Backfill ⁹ | na | na | na | 4 | 1 | 1 | 9 | 22 | 1 9 |
| Part of 3 | Phase 5 - San Pablo Creek Crossing by Pipe Bridge Method (San Pablo Avenue) | | | | | | | | | |
| | Clear and Grubbing | na | na | na | 1 | 10 | 0 | 8 | 36 | 3 8 |
| | Abutment construction | na | na | na | 2 | 2 | 1 | 7 | 20 | 1 7 |
| | Bridge delivery / erection | na | na | na | 2 days | 0 | 2 | 11 | 26 | 1 11 |
| | Pipeline Installation | 100 | 36 | 50 | 2 days | 0 | 2 | 9 | 22 | 1 9 |
| | Phase 5 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 11 | 28 | 1 11 |
| | Phase 6 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 9 | 26 | 1 9 |
| | Phase 7 - Paving | 9,385 | na | 700 | 2.7 | 10 | 0 | 13 | 46 | 3 13 |
| | Total | 9,655 | LF of pipe | | 50 | weeks | | | | |
| | Total Excavated Material | 12,694 | CY | | | | | | MAXIMUM TRIPS = | 74 |
| | | | | | | | | | | 3 24 |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Central PZ Pipeline (Richmond / San Pablo) is Open-Cut Trenching, except at Wildcat Creek & San Pablo Creek crossings.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each linear foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & two flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, and two flaggers.

Notes:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
4. Material truck trips for open-cut trench pipeline installation include deliveries of pipeline (1), appurtenance (1), and equipment (1). 3 material truck per day
5. Worker vehicle trips for pipeline installation consist of crew (20), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitors (1 on avg).
Worker vehicle trips for pits excavation & backfill consist of crew (6), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitor (1).
Worker vehicle trips for pipe bridge abutments construction consist of crew (4), contractor's superintendent (1), District's inspector (1), & City's inspector (1).
Worker vehicle trips for pipe bridge erection consist of crew (8), contractor's superintendent (1), District's inspector (1), & City's inspector (1).
Worker vehicle trips for installation pipe to pipe bridge consist of crew (5), contractor's superintendent (1), District's inspector (1), & City's inspector (1).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.
8. Jack and bore method production rates based on Hesperian Boulevard Pipeline Relocation Project (Spec 2020).
9. Insertion pit approximately 36 ft long by 13 ft wide by 19 ft deep and receiving pit approximately 13 ft long by 9 ft wide by 16 feet deep.
Wildcat Creek is ~ 8 ft deep per 2' contours. Receiving pit depth is 8 ft below creek bottom, slope of pipeline between jacking pit and receiving pit is 2% up.

Central Pressure Zone Pipeline (Richmond_San Pablo) - Preferred Alignment (Alternative 4)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis.

| Estimated Truck Trips that project would generate during each construction phase, as well as daily and peak hourly trips | | | | | | | | | | |
|--|--|-------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| Reach | Construction Phase | Pipe length | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
| 1 & 2 | Phase 1 - 23rd St / Nevin Ave to 23rd St / Brookside Dr via 23rd Street. | 8,910 | 36 | 200 | 8.9 | 23 | 4 | 24 | 102 | 7 24 |
| 3 & 4 | Phase 2 - 23rd St / Brookside Dr to RW X574/Brookside. | 670 | 36 | 200 | 0.7 | 23 | 4 | 24 | 102 | 7 24 |
| 3 & 4 | Phase 3 - RW X574/Brookside to RW X574/Road 20. | 305 | 48 | 200 | 0.3 | 31 | 4 | 24 | 118 | 9 24 |
| Part of 2 | Phase 4 - Wildcat Creek Crossing by Jack & Bore Method ⁸ | | | | | | | | | |
| | Pits Excavation ⁹ | na | na | na | 2 | 2 | 1 | 9 | 24 | 1 9 |
| | Casing Installation | 170 | 48 | 10 | 3.4 | 1 | 1 | 11 | 26 | 1 11 |
| | Pipeline Installation | 170 | 36 | 50 | 0.7 | 0 | 1 | 15 | 32 | 0 15 |
| | Pits Backfill ⁹ | na | na | na | 4 | 1 | 1 | 9 | 22 | 1 9 |
| Part of 3 | Phase 5 - San Pablo Creek Crossing by Pipe Bridge Method | | | | | | | | | |
| | Clear and Grubbing | na | na | na | 1 | 10 | 0 | 8 | 36 | 3 8 |
| | Abutment construction | na | na | na | 2 | 2 | 1 | 7 | 20 | 1 7 |
| | Bridge delivery / erection | na | na | na | 2 days | 0 | 2 | 11 | 26 | 1 11 |
| | Pipeline Installation | 95 | 48 | 50 | 2 days | 0 | 2 | 9 | 22 | 1 9 |
| | Phase 6 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 0 | 6 | 1 0 |
| | Phase 7 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 7 | 22 | 1 7 |
| | Phase 8 - Paving | 9,580 | na | 700 | 2.7 | 10 | 0 | 13 | 46 | 3 13 |
| | Total | 9,845 | LF of pipe | | 36 weeks | | | | | |
| | | | | | | | | | | |
| | Total Excavated Material | 12,948 | CY | | MAXIMUM TRIPS = | | | | 118 | 7 24 |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M - F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
 - Construction staging area and two-day material storage to occur along the alignment.
 - Construction Method for the new 36-inch Central PZ Pipeline (Richmond / San Pablo) is Open-Cut Trenching, except at Wildcat Creek & San Pablo Creek crossings.
 - Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
 - Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
 - Each lineal foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
 - New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
 - Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & two flagger
 - Paving crew consists of one foreman, one HEO, two truck driver, two rakers, and two flaggers.

Page

- Note:

 1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
 2. Duration does not include down-time, mobilization, demobilization nor reflect total duration
 3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
 4. Material truck trips for open-cut trench pipeline installation include deliveries of pipeline (2), appurtenance (1), and equipment (1) . 4 material truck per day
 5. Worker vehicle trips for pipeline installation consist of crew (20), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitors (1 on avg).
Worker vehicle trips for pits excavation & backfill consist of crew (6) , contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitor (1).
Worker vehicle trips for pipe bridge abutments construction consist of crew (4) , contractor's superintendent (1), District's inspector (1), & City's inspector (1)
Worker vehicle trips for pipe bridge erection consist of crew (8) , contractor's superintendent (1), District's inspector (1), & City's inspector (1)
Worker vehicle trips for installation pipe to pipe bridge consist of crew (5) , contractor's superintendent (1), District's inspector (1), & City's inspector (1)
Worker vehicle trips for paving consist of crew (9) , contractor's superintendent (1), District's inspector (1), City's inspector (1).
 6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
 7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estiamted by assuming all workers arriving and leaving the job site in an one-hour period.
 8. Jack and bore method production rates based on Hesperian Boulevard Pipeline Relocation Project (Spec 2020).
 9. Insertion pit approximately 36 ft long by 13 ft wide by 19 ft deep and receiving pit approximately 13 ft long by 9 ft wide by 16 feet deep.
Wildcat Creek is ~ 8 ft deep per 2' contours. Receiving pit depth is 8 ft below creek bottom, slope of pipeline between jacking pit and receiving pit is 2% up.

Central Pressure Zone Pipeline (Richmond_San Pablo) - Preferred Alignment (San Pablo Avenue Option)

Estimated Vehicle / Truck Trips that project-related activities would generate during each construction phase, on both a daily and peak hourly basis:

| Segment | Construction Phase | Pipe length | Pipe ID (inch) | Production Rate ¹ (LF/day) | Duration ² (weeks) | Haul Trucks ³ (per day) | Materials Trucks ⁴ (per day) | Worker Vehicles ⁵ (per day) | Daily One-Way Trips ⁶ | Max Hourly One-Way Trips ⁷ |
|-----------|--|-------------|----------------|---------------------------------------|-------------------------------|------------------------------------|---|--|----------------------------------|---------------------------------------|
| 1 & 2 | Phase 1 - 23rd St / Nevin Ave to 23rd St / Brookside Dr via 23rd Street. | 8,910 | 36 | 200 | 8.9 | 23 | 4 | 24 | 102 | 7 24 |
| 3 & 4 | Phase 2A - 23rd St / Brookside Dr to Road 20 via 23rd St, San Pablo Avenue, as well as parcels 411-282-001 & 412-300-010 owned by | 475 | 36 | 200 | 0.5 | 23 | 4 | 24 | 102 | 7 24 |
| Part of 2 | Phase 4 - Wildcat Creek Crossing by Jack & Bore Method ⁸ | | | | | | | | | |
| | Pits Excavation ⁹ | na | na | na | 2 | 2 | 1 | 9 | 24 | 1 9 |
| | Casing Installation | 170 | 48 | 10 | 3.4 | 1 | 1 | 11 | 26 | 1 11 |
| | Pipeline Installation | 170 | 36 | 50 | 0.7 | 0 | 1 | 15 | 32 | 0 15 |
| | Pits Backfill ⁹ | na | na | na | 4 | 1 | 1 | 9 | 22 | 1 9 |
| Part of 3 | Phase 5 - San Pablo Creek Crossing by Pipe Bridge Method (San Pablo Avenue) | | | | | | | | | |
| | Clear and Grubbing | na | na | na | 1 | 10 | 0 | 8 | 36 | 3 8 |
| | Abutment construction | na | na | na | 2 | 2 | 1 | 7 | 20 | 1 7 |
| | Bridge delivery / erection | na | na | na | 2 days | 0 | 2 | 11 | 26 | 1 11 |
| | Pipeline Installation | 100 | 36 | 50 | 2 days | 0 | 2 | 9 | 22 | 1 9 |
| | Phase 5 - Flushing, Pressure Testing, Chlorination | 0 | na | na | 4.0 | 0 | 3 | 11 | 28 | 1 11 |
| | Phase 6 - Two Hot Tap Connections | 0 | na | na | 5.0 | 1 | 3 | 9 | 26 | 1 9 |
| | Phase 7 - Paving | 9,385 | na | 700 | 2.7 | 10 | 0 | 13 | 46 | 3 13 |
| | Total | 9,655 | LF of pipe | | 36 weeks | | | | | |
| | Total Excavated Material | 12,694 | CY | | | | | MAXIMUM TRIPS = | 102 | 7 24 |
| | | | | | | | | | | Trucks Vehicles |

Assumptions:

- Work schedule: 8-hour workday, typical construction hours M-F between 7:00 am to 7:00 pm (per ESP 494 - Mitigation Guidelines for Major Capital Projects).
- Construction staging area and two-day material storage to occur along the alignment.
- Construction Method for the new 36-inch Central PZ Pipeline (Richmond / San Pablo) is Open-Cut Trenching, except at Wildcat Creek & San Pablo Creek crossings.
- Excavated spoil will be hauled off site and trench will be backfilled with imported fills.
- Trench for 36-inch (ID) pipe is typically 4 feet 8 inches wide and 7 feet 5 inches deep (see Figure A).
- Each linear foot of pipe trench will generate 1.3 cubic yard (CY) of excavated spoil and require 1 CY of imported bedding material / aggregate base.
- New pavement with 6 inches (typical) asphalt concrete (AC), pavement width is 2 feet plus pipe trench width.
- Contractor's construction crew consists of two foreman, nine laborers (include plumbers & welder), four heavy equipment operator (HEO), two truck driver, & two flaggers.
- Paving crew consists of one foreman, one HEO, two truck driver, two rakers, and two flaggers.

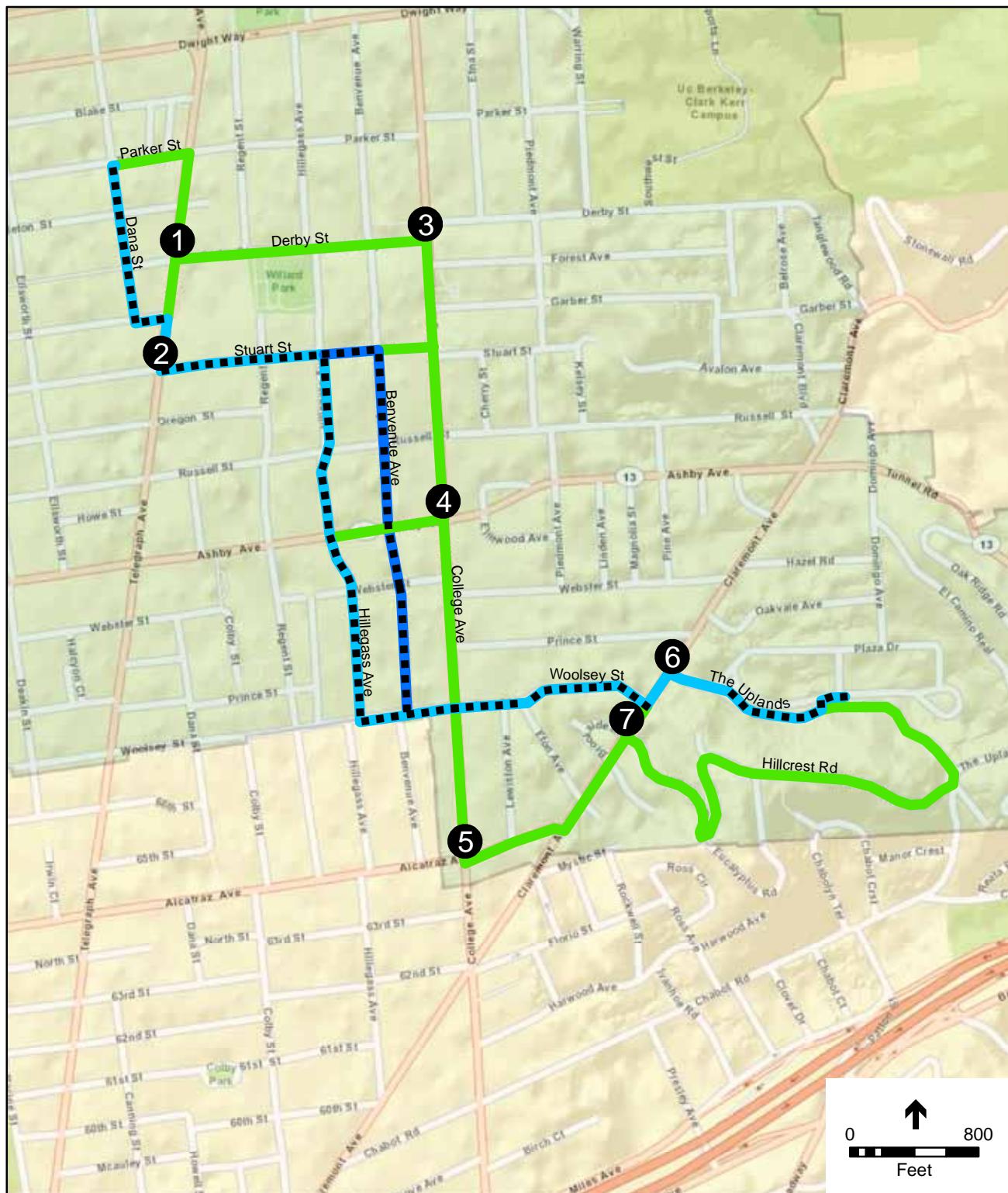
Note:

1. Contractor could typically install 80 to 200 lineal feet (LF), 100 LF on average, of 36-inch transmission pipeline per workday in paved areas.
One paving crew could typically pave 700 LF of trench with 6" AC paving per day.
2. Duration does not include down-time, mobilization, demobilization nor reflect total duration
3. Haul truck trips include spoil disposal, as well as trench backfill materials and pavement deliveries. Capacity: 20 CY - end dump trailer
9 CY - concrete truck
4. Material truck trips for open-cut trench pipeline installation include deliveries of pipeline (2), appurtenance (1), and equipment (1). 4 material truck per day
5. Worker vehicle trips for pipeline installation consist of crew (20), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitors (1 on avg).
Worker vehicle trips for pits excavation & backfill consist of crew (6), contractor's superintendent (1), District's inspector (1), City's inspector (1), & visitor (1).
Worker vehicle trips for pipe bridge abutments construction consist of crew (4), contractor's superintendent (1), District's inspector (1), & City's inspector (1).
Worker vehicle trips for pipe bridge erection consist of crew (8), contractor's superintendent (1), District's inspector (1), & City's inspector (1).
Worker vehicle trips for installation pipe to pipe bridge consist of crew (5), contractor's superintendent (1), District's inspector (1), & City's inspector (1).
Worker vehicle trips for paving consist of crew (9), contractor's superintendent (1), District's inspector (1), City's inspector (1).
6. Account for haul trucks, material trucks and worker vehicles going to and leaving the project site on a daily basis.
7. Max hourly one-way trucks is estimated by averaging the number of trucks to the job site on a daily basis over an 8-hour period.
Max hourly one-way vehicles is estimated by assuming all workers arriving and leaving the job site in an one-hour period.
8. Jack and bore method production rates based on Hesperian Boulevard Pipeline Relocation Project (Spec 2020).
9. Insertion pit approximately 36 ft long by 13 ft wide by 19 ft deep and receiving pit approximately 13 ft long by 9 ft wide by 16 feet deep.
Wildcat Creek is ~ 8 ft deep per 2' contours. Receiving pit depth is 8 ft below creek bottom, slope of pipeline between jacking pit and receiving pit is 2% up.

APPENDIX D

Traffic Control Scheme Figures

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- ■ ■ Proposed Road Closures
- Wildcat Pipeline (Berkeley)
- Alternative Alignment (Benvenue Ave)
- Detour Routes
- Study Intersections

EBMUD West of Hills Northern Pipelines . 211488

Figure TC-1
Proposed Detour Routes
Wildcat Pipeline (Berkeley)

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LEGEND:

- | | | | | | |
|--|---|---|--|---|--|
|  TRAFFIC CONE OR DELINEATOR |  TEMPORARY SIGN (SPACED AT 125') |  DIRECTION OF TRAVEL |  CONSTRUCTION WORK AREA |  FLASHING ARROW SIGN (FAS) |  FAS SUPPORT OR TRAILER |
|--|---|---|--|---|--|

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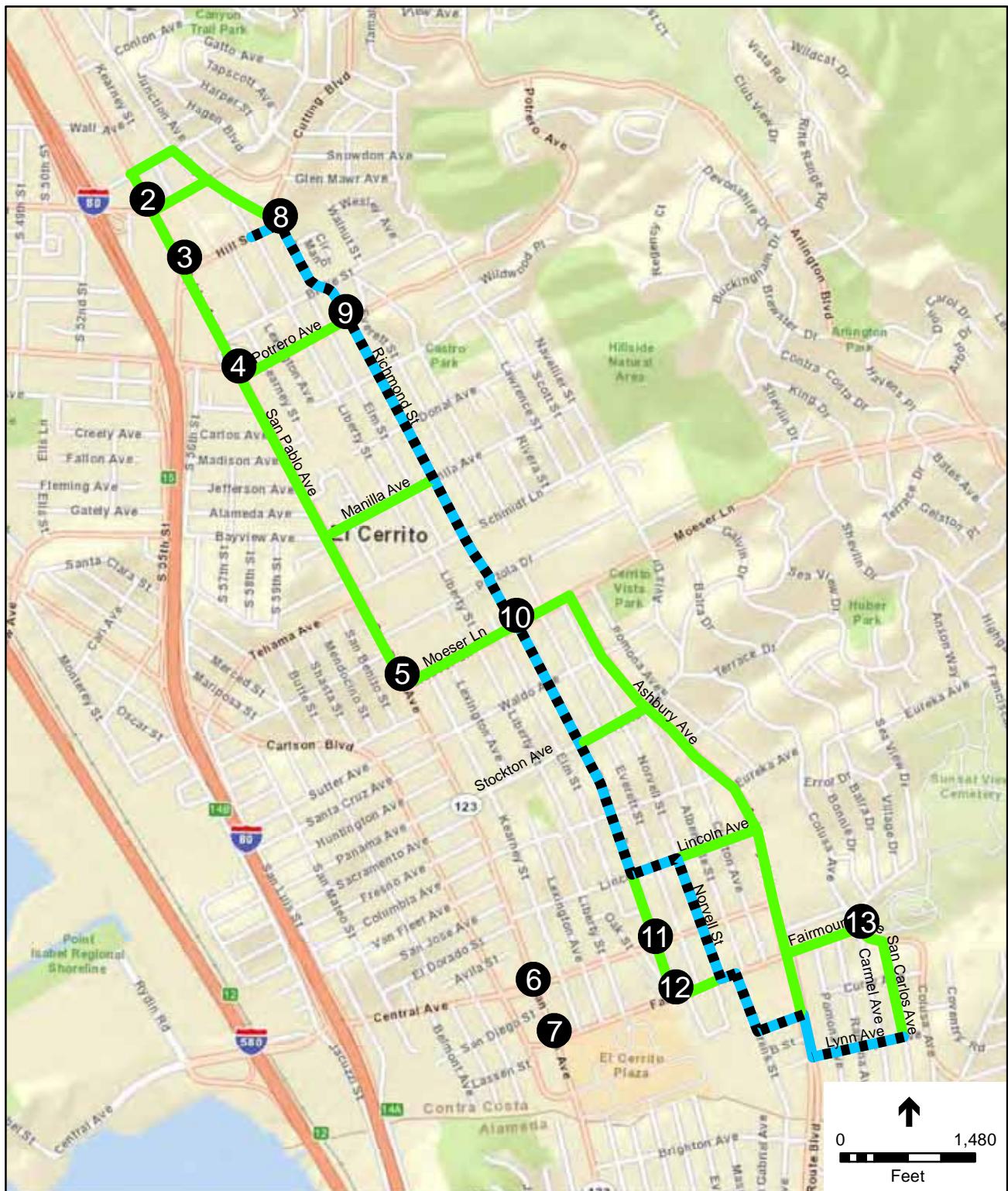


LEGEND:

- TRAFFIC CONE OR DELINEATOR
- ─ TEMPORARY SIGN (SPACED AT 125')
- DIRECTION OF TRAVEL
- FLAGGER
- ▨ CONSTRUCTION WORK AREA
- TYPE 3 BARRICADE



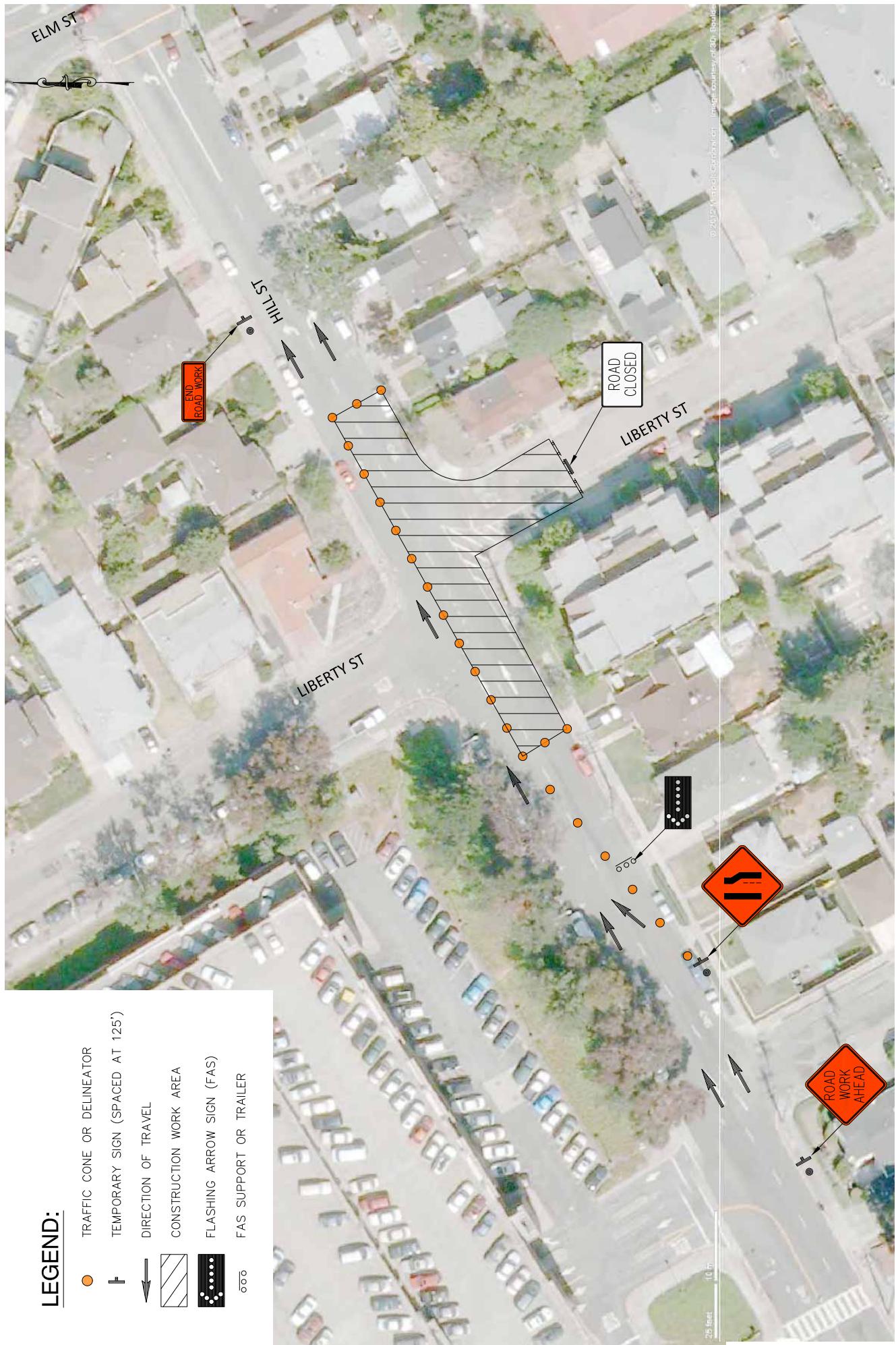
EBMUD West of Hills Northern Pipelines .211488
Figure TC-4
Traffic Control Plan - Parkside Dr./Nogales St. Tie-in
Wildcat Pipeline (Berkeley)



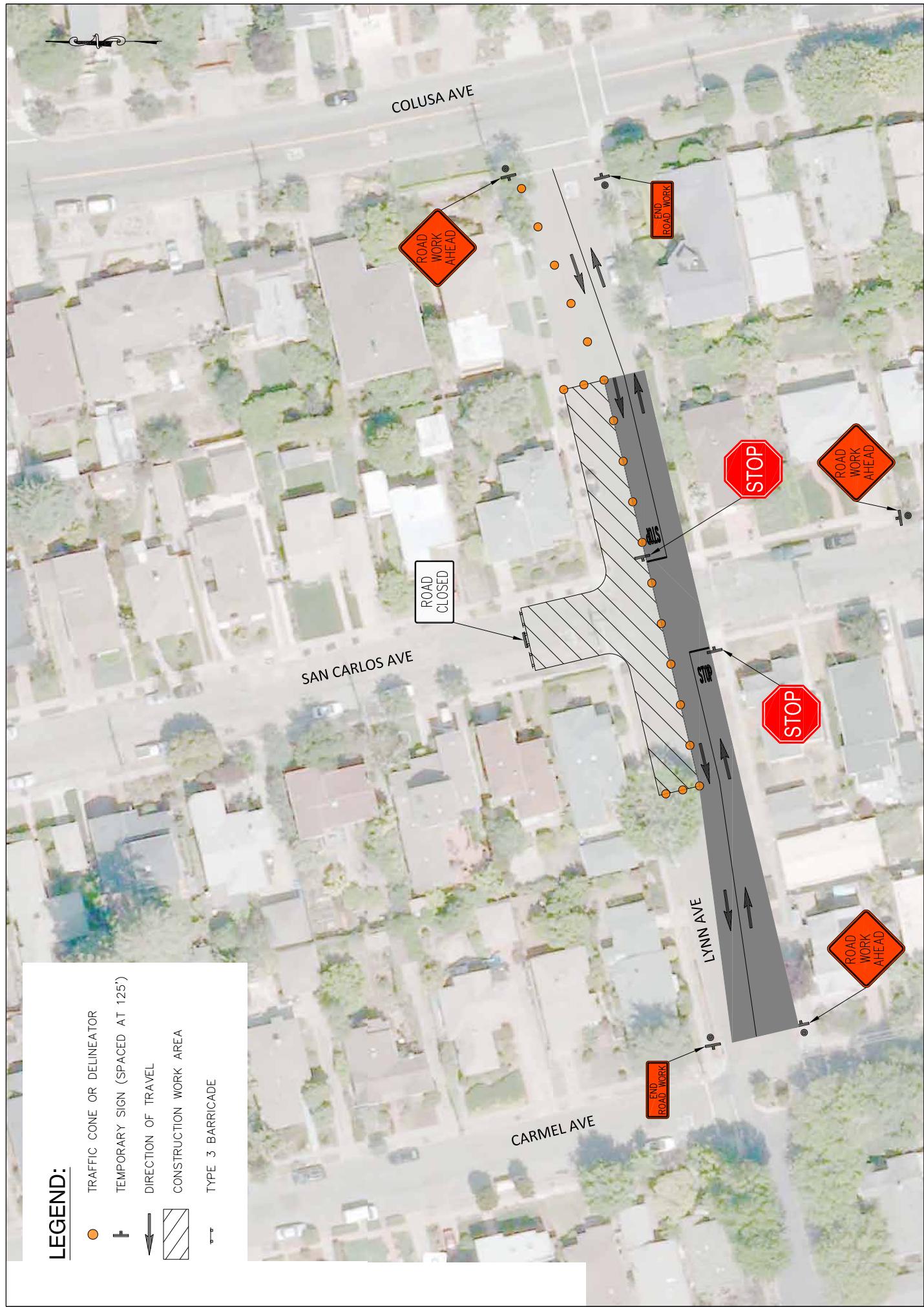
- Proposed Road Closures
- Wildcat Pipeline (El Cerrito)
- Detour Routes
- Study Intersections

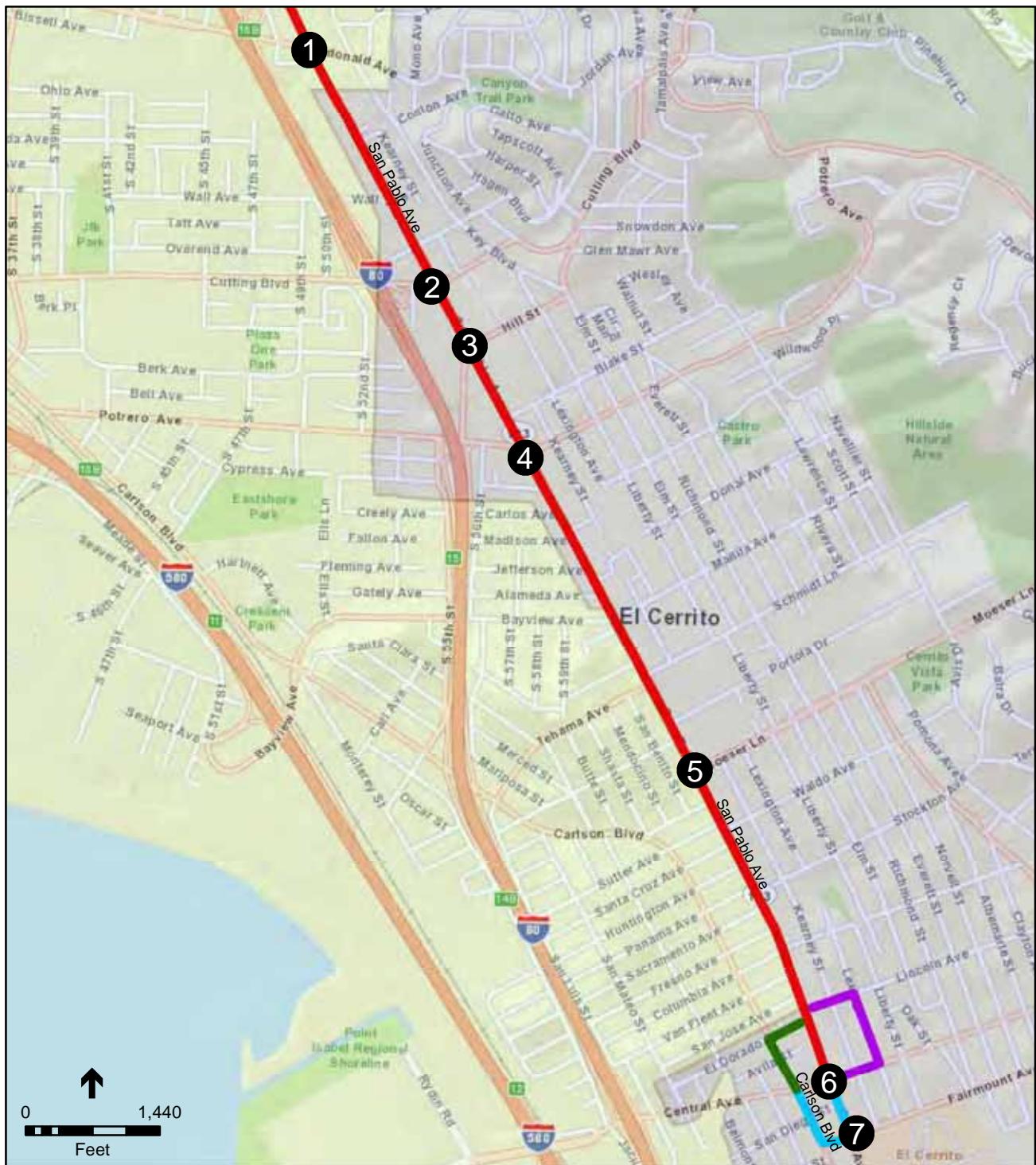
EBMUD West of Hills Northern Pipelines . 211488

Figure TC-5
Proposed Detour Routes
Wildcat Pipeline (El Cerrito)



EBMUD West of Hills Northern Pipelines - 211488
Figure TC-6
Traffic Control Plan - Hill St./Liberty St. Tie-in
Wildcat Pipeline (El Cerrito)





Central Pressure Zone Pipeline (El Cerrito/Richmond)

Detour Route for WB Central Avenue Through Traffic

Detour Route for EB LT Central Avenue Traffic

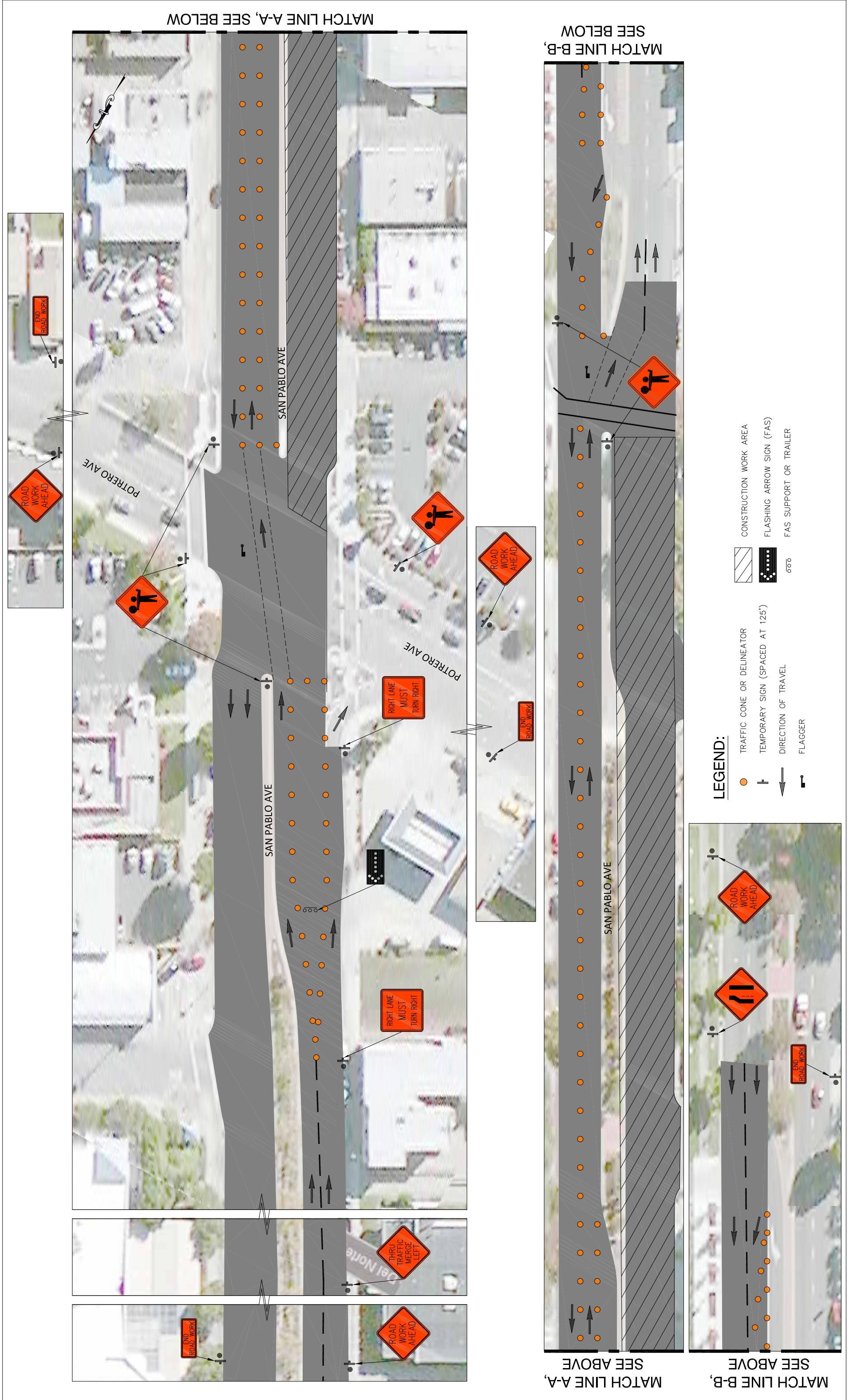
Detour Route for EB Central Avenue Buses and Trucks

② Study Intersections

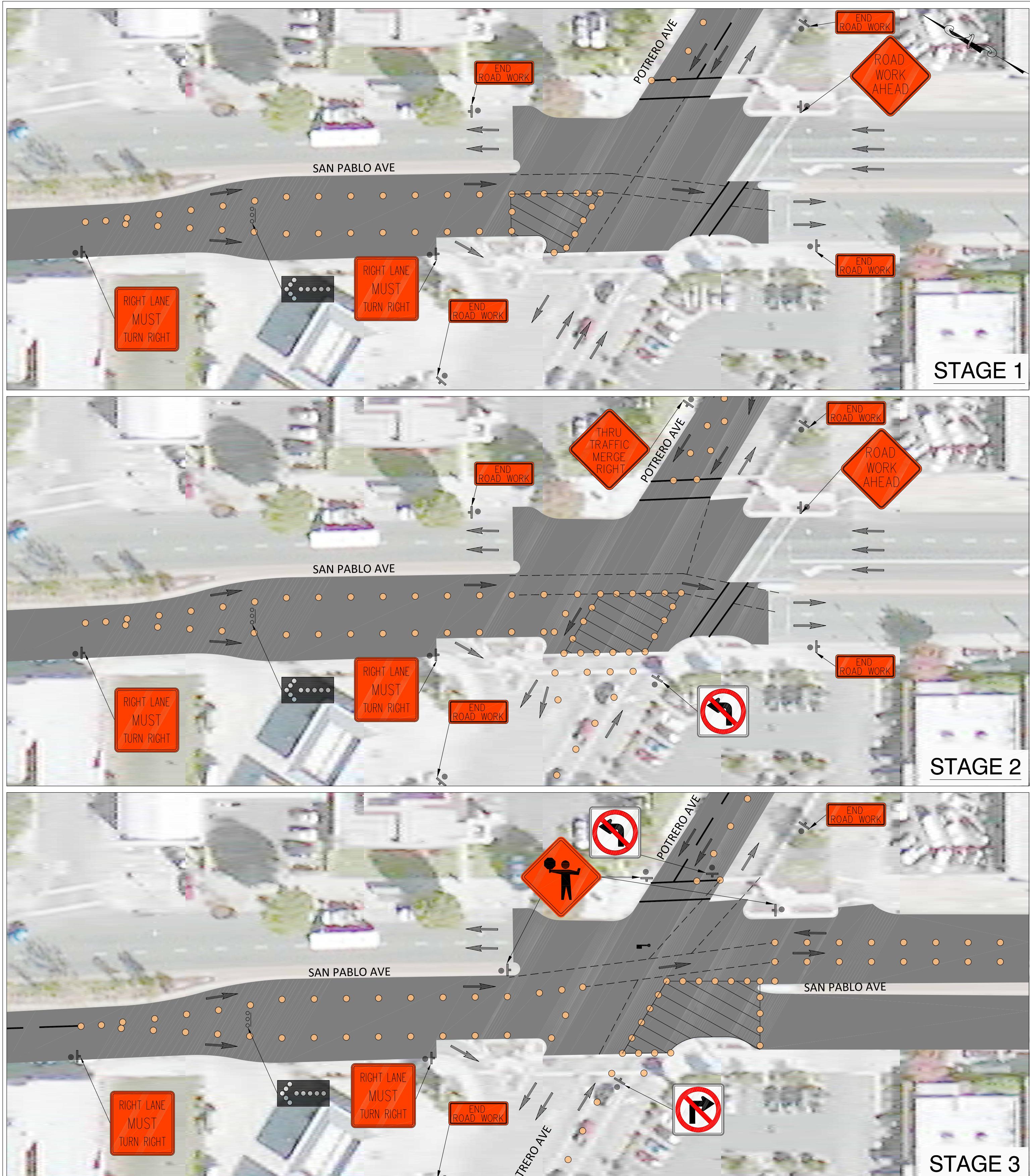
EBMUD West of Hills Northern Pipelines . 211488

Figure TC-8

Proposed Detour Routes
Central Pressure Zone Pipeline (El Cerrito/Richmond)

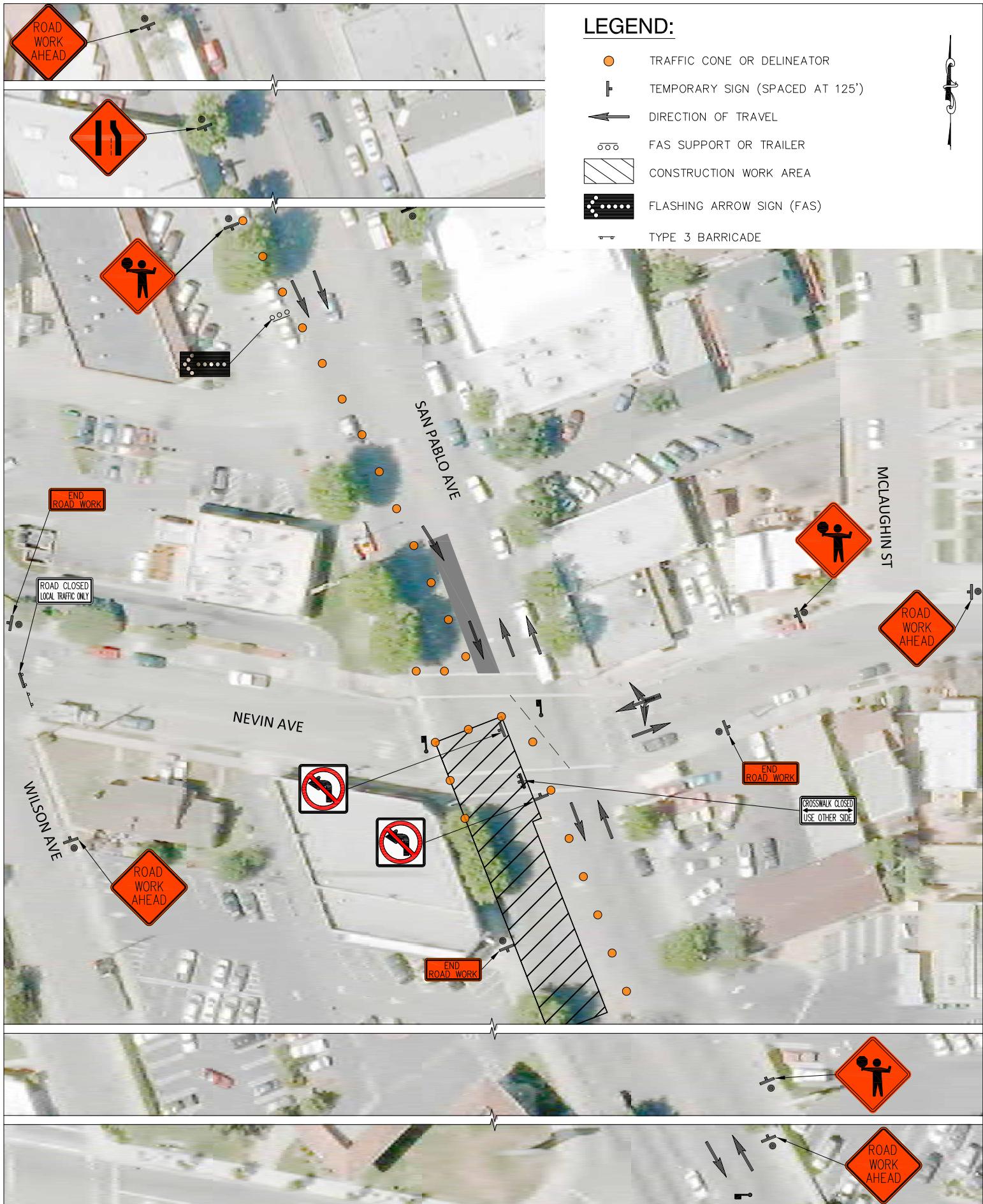


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LEGEND:

- | | | | |
|-----------------------------------|---------------------------|----------------------------|---------|
| ● TRAFFIC CONE OR DELINEATOR | CONSTRUCTION WORK AREA | ○○○ FAS SUPPORT OR TRAILER | FLAGGER |
| └ TEMPORARY SIGN (SPACED AT 125') | FLASHING ARROW SIGN (FAS) | ← DIRECTION OF TRAVEL | |



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Figure TC-11

Traffic Control Plan - San Pablo Ave./Nevin Ave. Tie-in
Central Pressure Zone Pipeline (El Cerrito/Richmond)

LEGEND:

- TRAFFIC CONE OR DELINEATOR
- ↑ TEMPORARY SIGN (SPACED AT 125')
- ← DIRECTION OF TRAVEL
- FAS SUPPORT OR TRAILER
- ▨ CONSTRUCTION WORK AREA
- FLASHING ARROW SIGN (FAS)

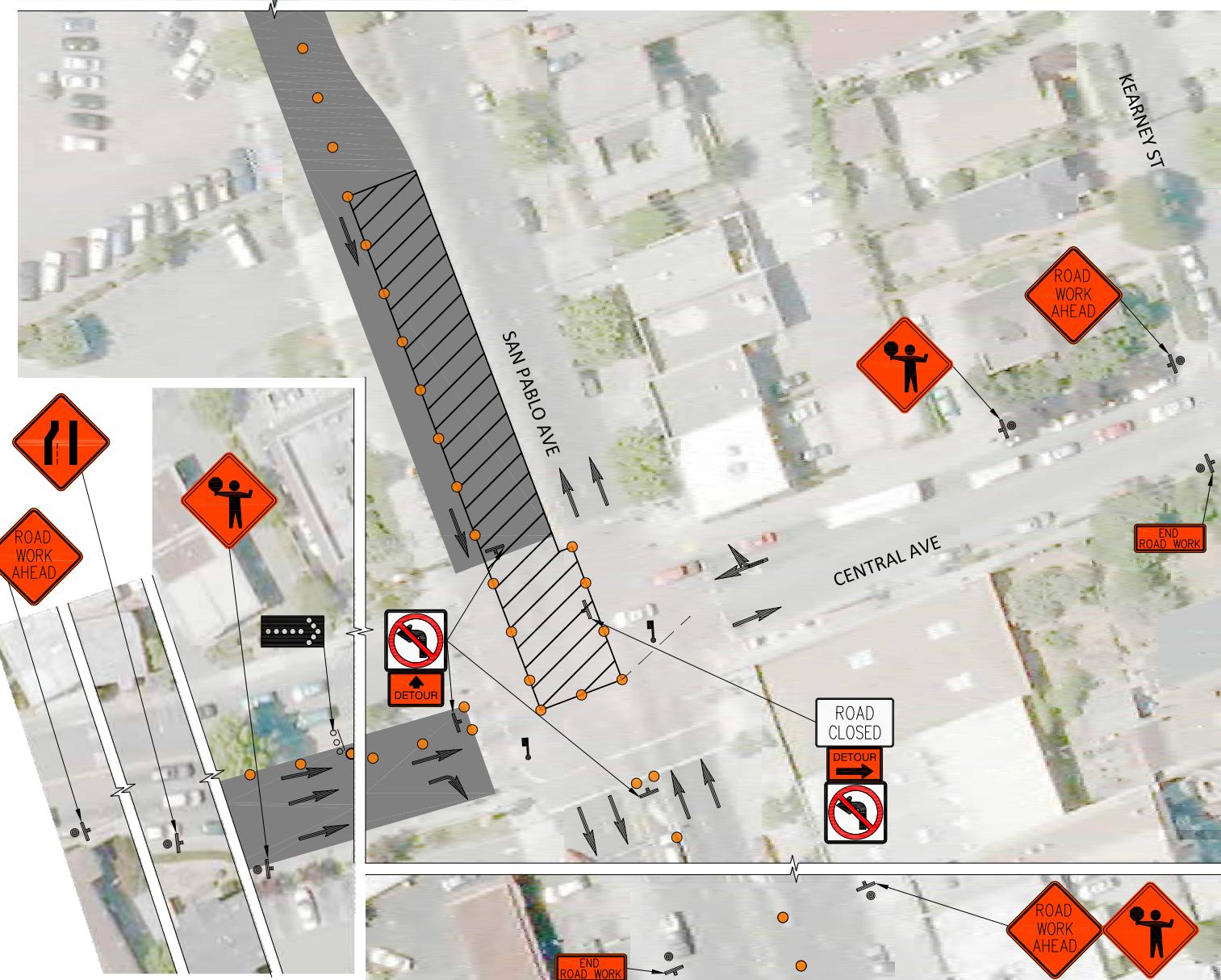
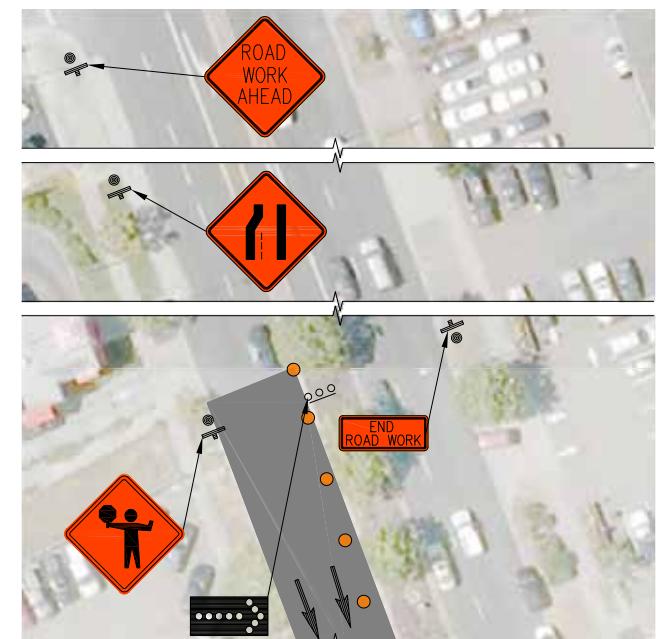
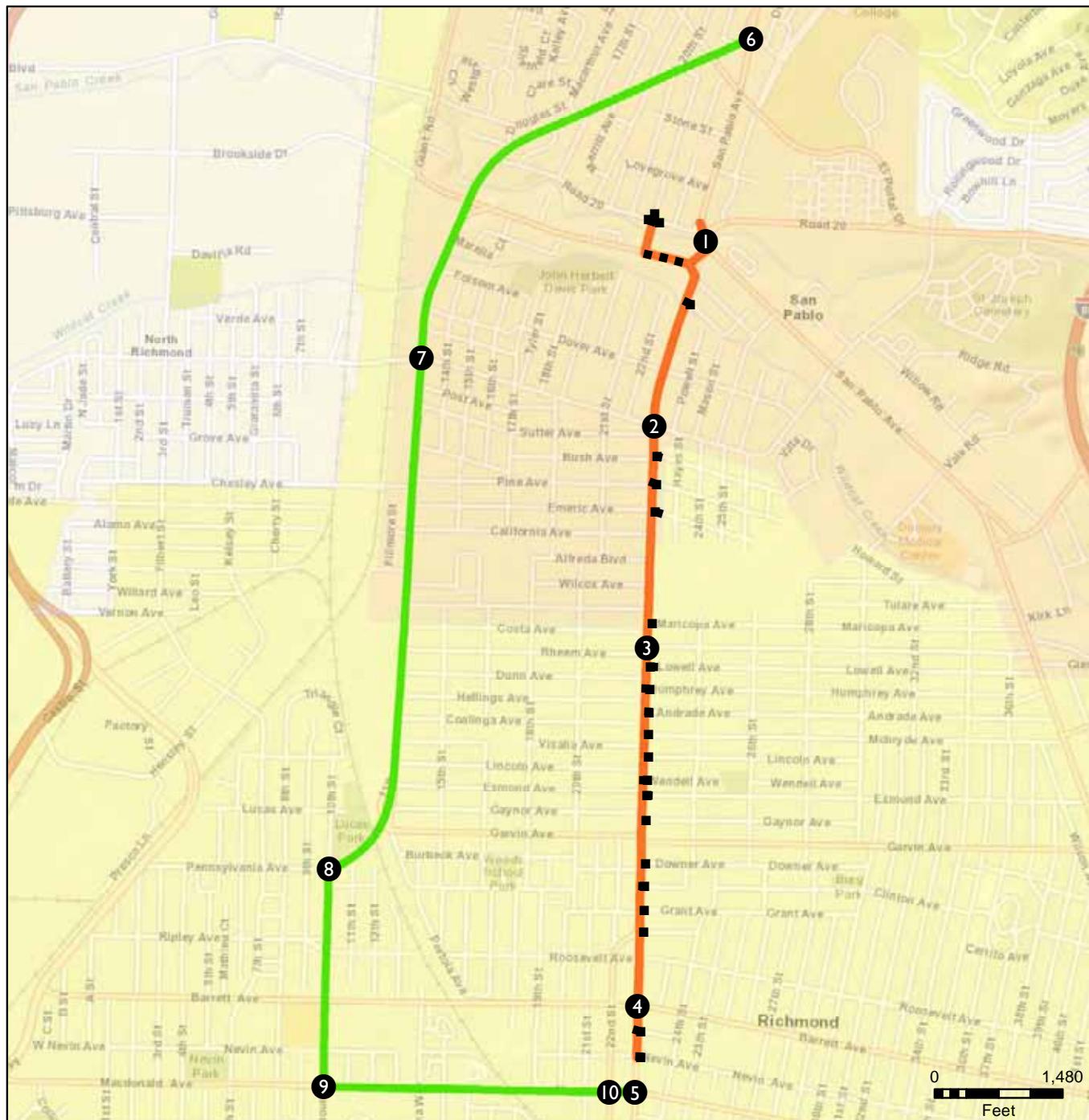


Figure TC-12

Traffic Control Plan - San Pablo Ave./Central Ave. Tie-in
Central Pressure Zone Pipeline (El Cerrito/Richmond)



2 Study Intersections

■ Proposed Road Closure

— Central PZ Pipeline (Richmond/San Pablo) Location

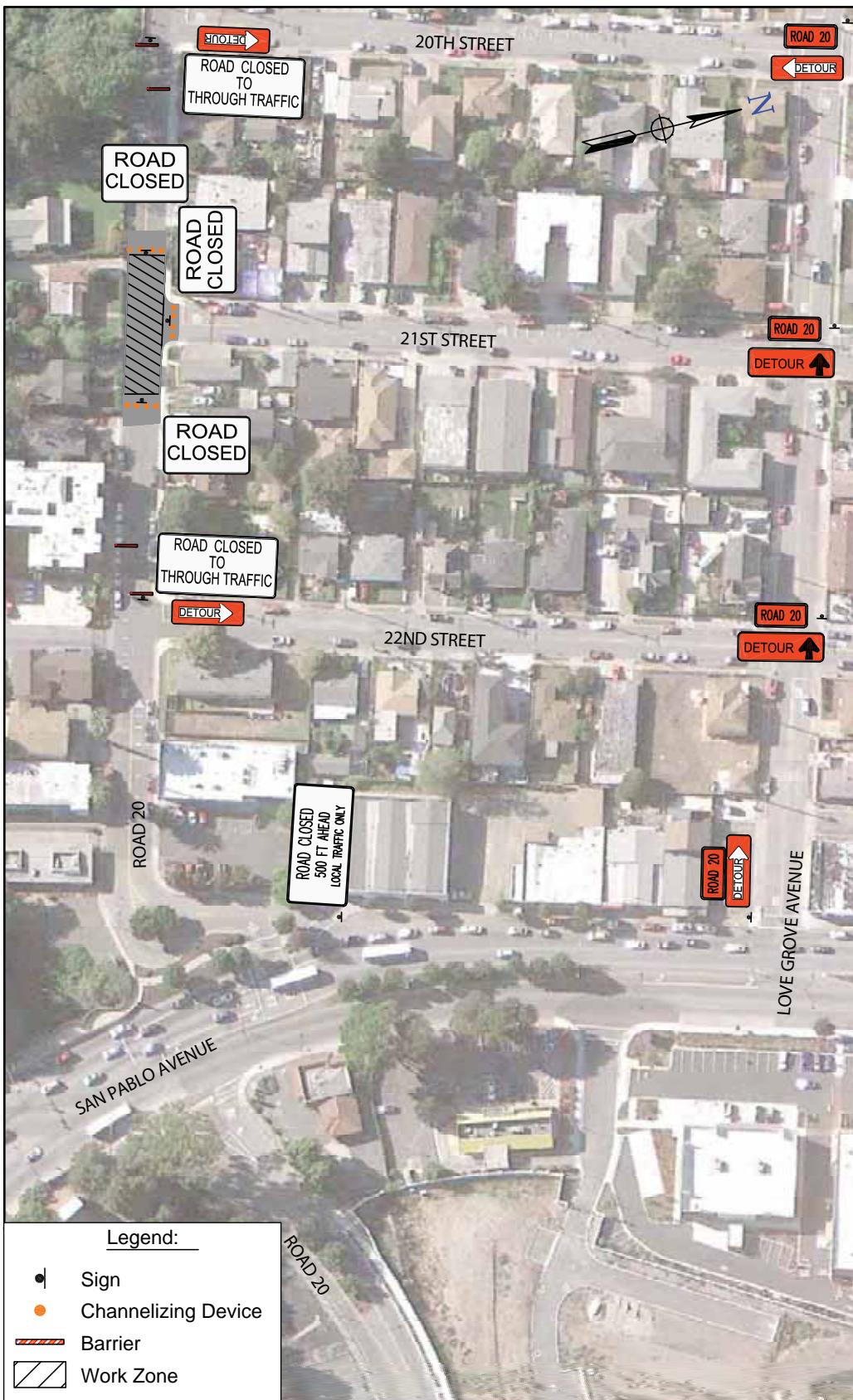
— Detour Route

SOURCE: W-Trans, ESRI

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Figure TC-13

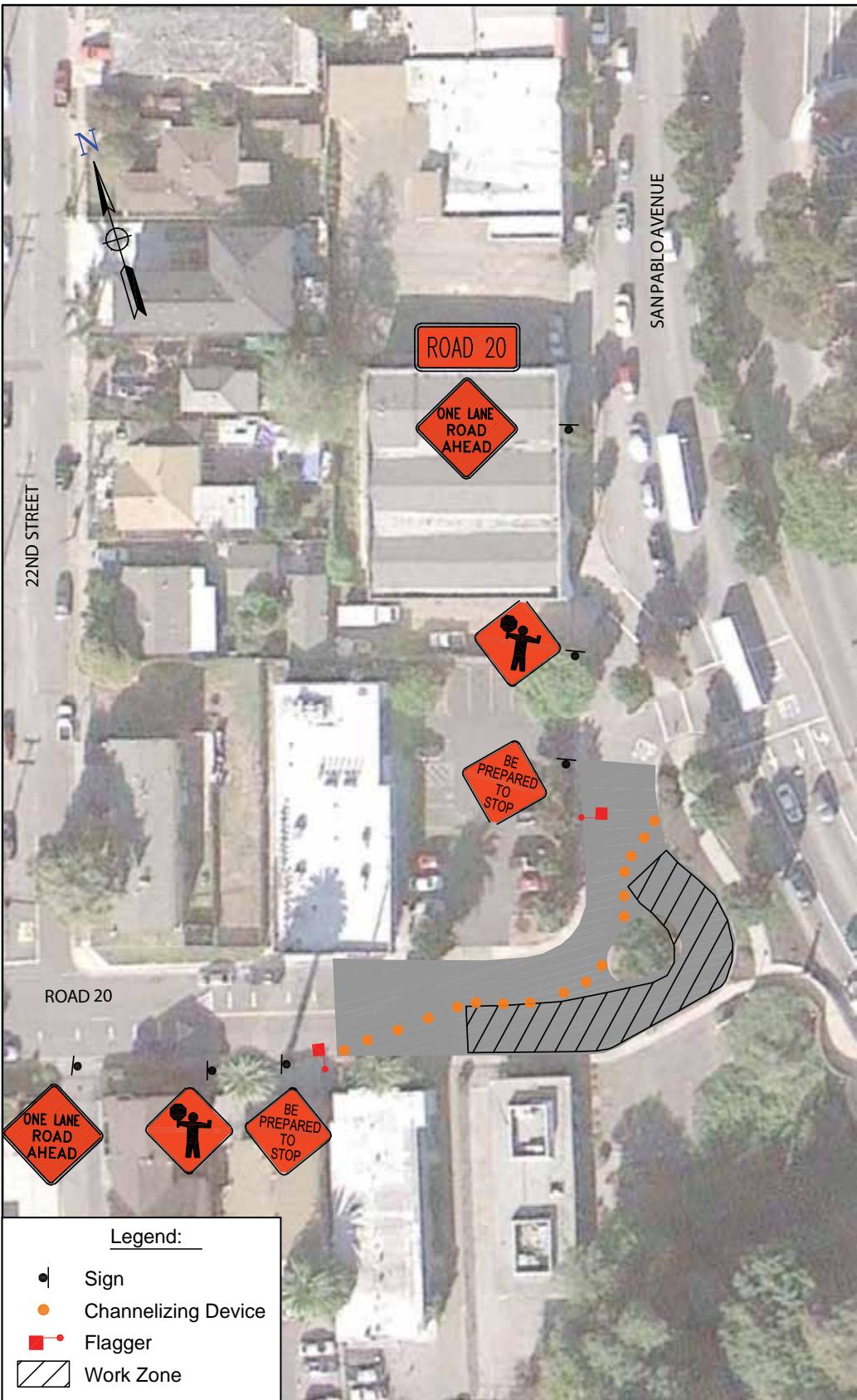
Proposed Detour Routes
Central Pressure Zone Pipeline (Richmond/San Pablo)



SOURCE: W-Trans

EBMUD West of Hills Northern Pipelines . 211488

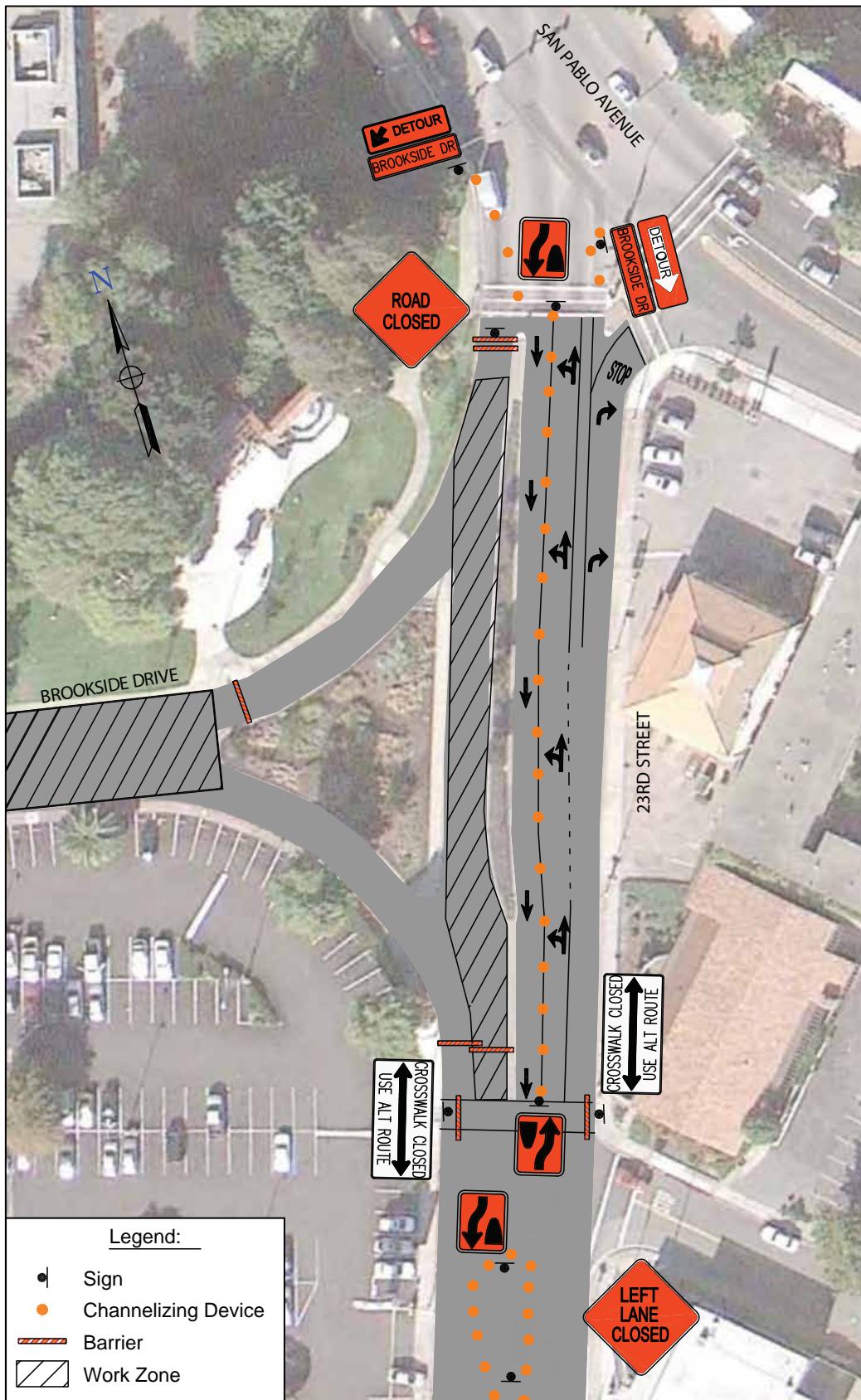
Figure TC-14
Traffic Control Plan – Road 20/21st St. Tie-in
Central Pressure Zone Pipeline (Richmond/San Pablo)



SOURCE: W-Trans

EBMUD West of Hills Northern Pipelines . 211488

Figure TC-15
Traffic Control Plan – Alternative Road 20 Tie-in
Central Pressure Zone Pipeline (Richmond/San Pablo)

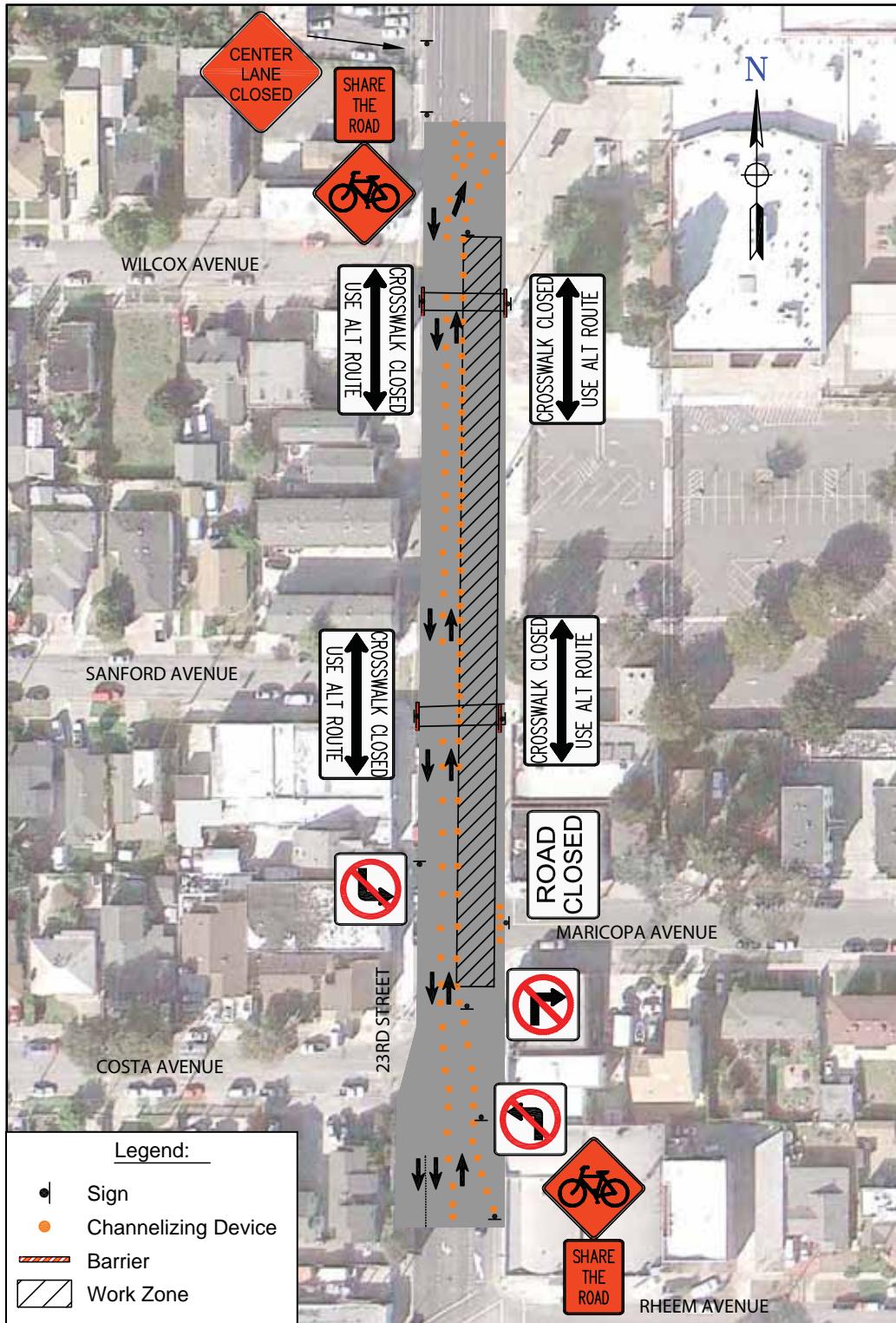


SOURCE: W-Trans

EBMUD West of Hills Northern Pipelines . 211488

Figure TC-16

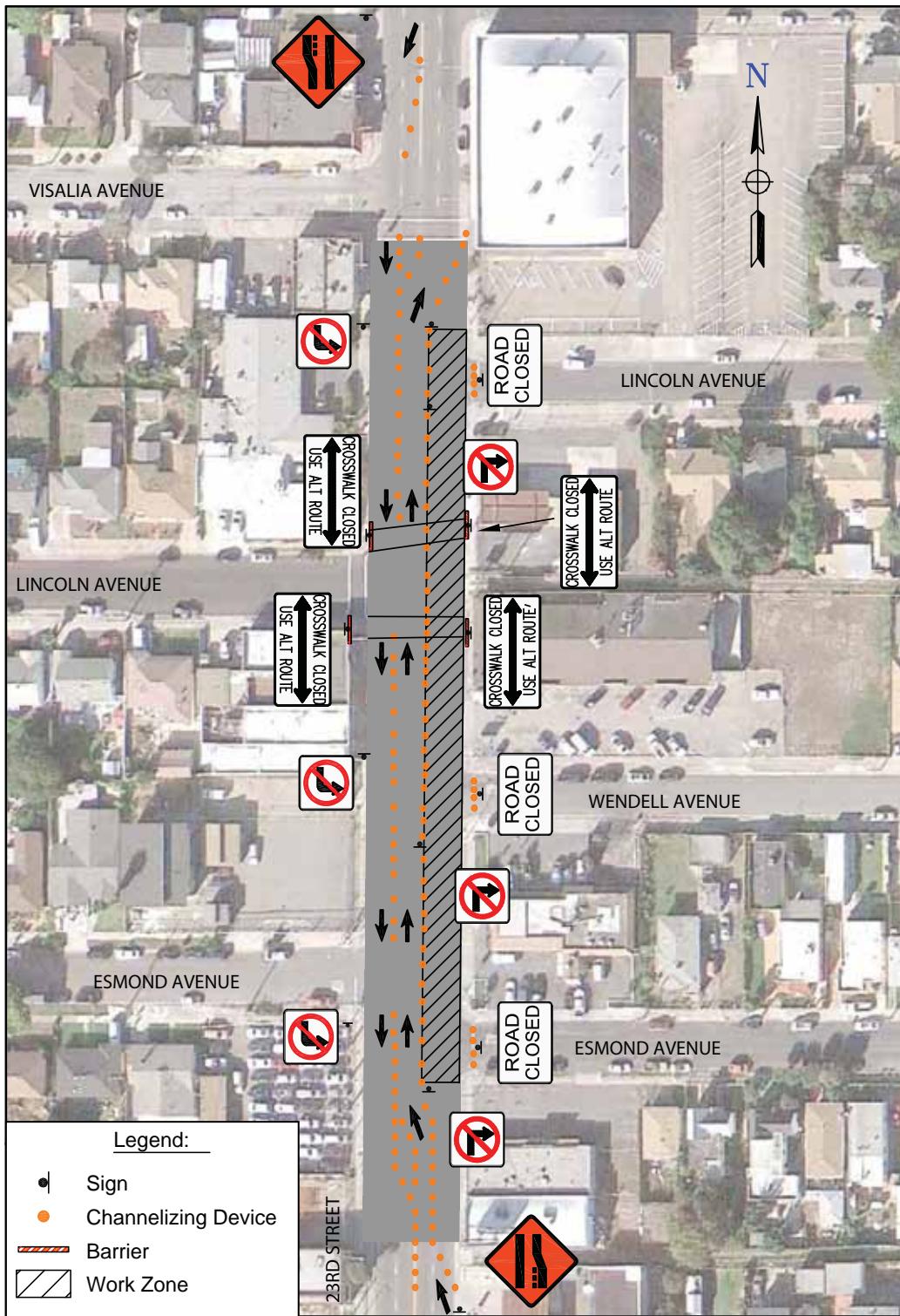
Traffic Control Plan – 23rd St. at Brookside Dr. Detail
Central Pressure Zone Pipeline (Richmond/San Pablo)



SOURCE: W-Trans

EBMUD West of Hills Northern Pipelines . 211488

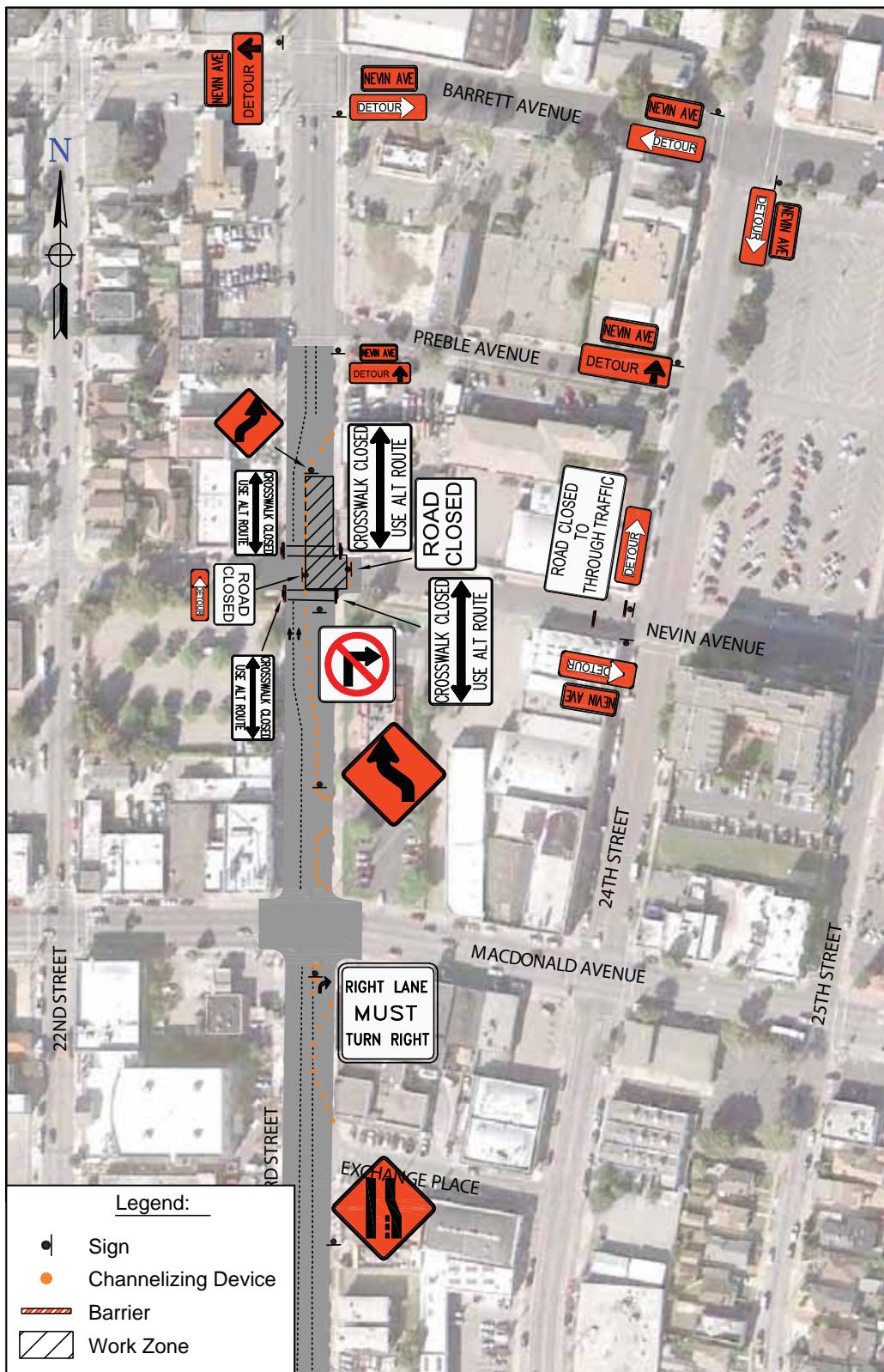
Figure TC-17
Traffic Control Plan – 23rd St 3-Lane Section Detail
Central Pressure Zone Pipeline (Richmond/San Pablo)



SOURCE: W-Trans

EBMUD West of Hills Northern Pipelines . 211488

Figure TC-18
Traffic Control Plan – 23rd St 3-Lane Section Detail
Central Pressure Zone Pipeline (Richmond/San Pablo)



SOURCE: W-Trans

EBMUD West of Hills Northern Pipelines . 211488

Figure TC-19

Traffic Control Plan – 23rd St./Nevin Ave. Tie-in
Central Pressure Zone Pipeline (Richmond/San Pablo)

APPENDIX E

California Manual on Uniform Traffic Control Typical Applications

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CHAPTER 6H. TYPICAL APPLICATIONS

Section 6H.01 Typical Applications

Support:

01 Chapter 6G contains discussions of typical TTC activities. This Chapter presents typical applications for a variety of situations commonly encountered. While not every situation is addressed, the information illustrated can generally be adapted to a broad range of conditions. In many instances, an appropriate TTC plan is achieved by combining features from various typical applications. For example, work at an intersection might present a near-side work zone for one street and a far-side work zone for the other street. These treatments are found in two different typical applications, while a third typical application shows how to handle pedestrian crosswalk closures. For convenience in using the typical application diagrams, Tables 6C-1 and 6C-4 are reproduced in this Chapter as Tables 6H-3 and 6H-4, respectively.

02 Procedures for establishing TTC zones vary with such conditions as road configuration, location of the work, work activity, duration of work, road user volumes, road vehicle mix (buses, trucks, cars, motorcycles, and bicycles), and road user speeds.

03 In general, the procedures illustrated represent minimum solutions for the situations depicted. Except for the notes (which are clearly classified using headings as being Standard, Guidance, Option, or Support), the information presented in the typical applications can generally be regarded as Guidance.

Option:

04 Other devices may be added to supplement the devices and device spacing may be adjusted to provide additional reaction time or delineation. Fewer devices may be used based on field conditions.

Support:

05 Figures and tables found throughout Part 6 provide information for the development of TTC plans. Also, Table 6H-3 is used for the determination of sign spacing and other dimensions for various area and roadway types.

06 Table 6H-1 is an index of the 46 typical applications. Typical applications are shown on the right-hand page with notes on the facing page to the left. The legend for the symbols used in the typical applications is provided in Table 6H-2. In many of the typical applications, sign spacings and other dimensions are indicated by letters using the criteria provided in Table 6H-3. The formulas for determining taper lengths are provided in Table 6H-4.

07 Most of the typical applications show TTC devices for only one direction.

Guidance:

08 *The spacing of channelizing devices should not exceed the maximum distances shown in Table 6F-101(CA).*

Table 6H-1. Index to Typical Applications

| Typical Application Description | Typical Application Number |
|---|----------------------------|
| Work Outside of the Shoulder (see Section 6G.06) | |
| Work Beyond the Shoulder | TA-1 |
| Blasting Zone | TA-2 |
| Work on the Shoulder (see Sections 6G.07 and 6G.08) | |
| Work on the Shoulders | TA-3 |
| Short Duration or Mobile Operation on a Shoulder | TA-4 |
| Shoulder Closure on a Freeway | TA-5 |
| Shoulder Work with Minor Encroachment | TA-6 |
| Work Within the Traveled Way of a Two-Lane Highway (see Section 6G.10) | |
| Road Closed with a Diversion | TA-7 |
| Roads Closed with an Off-Site Detour | TA-8 |
| Overlapping Routes with a Detour | TA-9 |
| Lane Closure on a Two-Lane Road Using Flaggers | TA-10 |
| Lane Closure on a Two-Lane Road with Low Traffic Volumes | TA-11 |
| Lane Closure on a Two-Lane Road Using Traffic Control Signals | TA-12 |
| Temporary Road Closure | TA-13 |
| Haul Road Crossing | TA-14 |
| Work in the Center of a Road with Low Traffic Volumes | TA-15 |
| Surveying Along the Center Line of a Road with Low Traffic Volumes | TA-16 |
| Mobile Operations on a Two-Lane Road | TA-17 |
| Work Within the Traveled Way of an Urban Street (see Section 6G.11) | |
| Lane Closure on a Minor Street | TA-18 |
| Detour for One Travel Direction | TA-19 |
| Detour for a Closed Street | TA-20 |
| Work Within the Traveled Way at an Intersection and on Sidewalks (see Section 6G.13) | |
| Lane Closure on the Near Side of an Intersection | TA-21 |
| Right-Hand Lane Closure on the Far Side of an Intersection | TA-22 |
| Left-Hand Lane Closure on the Far Side of an Intersection | TA-23 |
| Half Road Closure on the Far Side of an Intersection | TA-24 |
| Multiple Lane Closures at an Intersection | TA-25 |
| Closure in the Center of an Intersection | TA-26 |
| Closure at the Side of an Intersection | TA-27 |
| Sidewalk Detour or Diversion | TA-28 |
| Crosswalk Closures and Pedestrian Detours | TA-29 |
| Work Within the Traveled Way of a Multi-Lane, Non-Access Controlled Highway (see Section 6G.12) | |
| Interior Lane Closure on a Multi-Lane Street | TA-30 |
| Lane Closure on a Street with Uneven Directional Volumes | TA-31 |
| Half Road Closure on a Multi-Lane, High-Speed Highway | TA-32 |
| Stationary Lane Closure on a Divided Highway | TA-33 |
| Lane Closure with a Temporary Traffic Barrier | TA-34 |
| Mobile Operation on a Multi-Lane Road | TA-35 |
| Work Within the Traveled Way of a Freeway or Expressway (see Section 6G.14) | |
| Lane Shift on a Freeway | TA-36 |
| Double Lane Closure on a Freeway | TA-37 |
| Interior Lane Closure on a Freeway | TA-38 |
| Median Crossover on a Freeway | TA-39 |
| Median Crossover for an Entrance Ramp | TA-40 |
| Median Crossover for an Exit Ramp | TA-41 |
| Work in the Vicinity of an Exit Ramp | TA-42 |
| Partial Exit Ramp Closure | TA-43 |
| Work in the Vicinity of an Entrance Ramp | TA-44 |
| Temporary Reversible Lane Using Movable Barriers | TA-45 |
| Work in the Vicinity of a Grade Crossing (see Section 6G.18) | |
| Work in the Vicinity of a Grade Crossing | TA-46 |

Table 6H-1(CA). Index to Typical Applications

| Typical Application Description | Typical Application Number |
|---|----------------------------|
| Work affecting Pedestrian and Bicycle Facilities (see Section 6G.05) | |
| Shoulder Closure on Urban (Low Speed) Locations to Accommodate Bicyclists | TA-101(CA) |
| Lane Closure on Freeway, Expressway, Rural and Urban (High Speed) Locations to Accommodate Bicyclists | TA-102(CA) |
| Detour for Bike Lane on Roads with Closure of One Travel Direction | TA-103(CA) |
| Right Lane and Bike Lane Closure on Far Side of Intersection | TA-104(CA) |
| Work Within the Traveled Way of a Two-Lane Highway (see Section 6G.10) | |
| Lane Shift on Road with Low Traffic Volumes | TA-105(CA) |

Table 6H-2. Meaning of Symbols on Typical Application Diagrams

| | | | |
|--|--|--|--------------------------------------|
| | Arrow board | | Shadow vehicle |
| | Arrow board support or trailer (shown facing down) | | Sign (shown facing left) |
| | Changeable message sign or support trailer | | Surveyor |
| | Channelizing device | | Temporary barrier |
| | Crash cushion | | Temporary barrier with warning light |
| | Direction of temporary traffic detour | | Traffic or pedestrian signal |
| | Direction of traffic | | Truck-mounted attenuator |
| | Flagger | | Type 3 barricade |
| | High-level warning device (Flag tree) | | Warning light |
| | Longitudinal channelizing device | | Work space |
| | Luminaire | | Work vehicle |
| | Pavement markings that should be removed for a long-term project | | |

Table 6H-3. Meaning of Letter Codes on Typical Application Diagrams

| Road Type | Distance Between Signs** | | |
|---|--------------------------|------------|------------|
| | A | B | C |
| Urban (low speed)* - 25 mph or less | 100 feet | 100 feet | 100 feet |
| Urban (low speed)* - more than 25 mph to 40 mph | 250 feet | 250 feet | 250 feet |
| Urban (high speed)* - more than 40 mph | 350 feet | 350 feet | 350 feet |
| Rural | 500 feet | 500 feet | 500 feet |
| Expressway / Freeway | 1,000 feet | 1,500 feet | 2,640 feet |

* Speed category to be determined by highway agency.

** The column headings A, B, and C are the dimensions shown in Figures 6H-1 through 6H-46. The A dimension is the distance from the transition or point of restriction to the first sign. The B dimension is the distance between the first and second signs. The C dimension is the distance between the second and third signs. (The "first sign" is the sign in a three-sign series that is closest to the TTC zone. The "third sign" is the sign that is furthest upstream from the TTC zone.)

Table 6H-4. Formulas for Determining Taper Length

| Speed (S) | Taper Length (L) in feet |
|----------------|--------------------------|
| 40 mph or less | $L = \frac{WS^2}{60}$ |
| 45 mph or more | $L = WS$ |

Where: L = taper length in feet
 W = width of offset in feet
 S = posted speed limit, or off-peak 85th-percentile speed prior to work starting, or the anticipated operating speed in mph

Table 6H-4(CA). Taper Length Criteria for Temporary Traffic Control Zones (for 12 feet Offset Width)

| Speed* S (mph) | Minimum Taper Length** for Width of Offset 12 feet (W) | | | |
|----------------------|---|---------------------------|---------------------------|-----------------------------|
| | Merging L (feet) | Shifting L/2 (feet) | Shoulder L/3 (feet) | Down Stream (feet)*** |
| 20 | 80 | 40 | 27 | 50 |
| 25 | 125 | 63 | 42 | 50 |
| 30 | 180 | 90 | 60 | 50 |
| 35 | 245 | 123 | 82 | 50 |
| 40 | 320 | 160 | 107 | 50 |
| 45 | 540 | 270 | 180 | 50 |
| 50 | 600 | 300 | 200 | 50 |
| 55 | 660 | 330 | 220 | 50 |
| 60 | 720 | 360 | 240 | 50 |
| 65 | 780 | 390 | 260 | 50 |
| 70 | 840 | 420 | 280 | 50 |

* - Posted speed limit, off-peak 85th-percentile speed prior to work starting, or the anticipated operating speed in mph.

** - For other offsets use the following merging taper length formula for L:

For speeds of 40 mph or less, $L=WS^2/60$

For speeds of 45 mph or more, $L=WS$

Where:
 L = taper length in feet
 W = width of offset in feet
 S = posted speed limit, off-peak 85th-percentile speed prior to work starting, or the anticipated operating speed in mph

*** - Maximum downstream taper length is 100 feet. See Section 6C.08.

Notes for Figure 6H-8—Typical Application 8 Road Closure with an Off-Site Detour

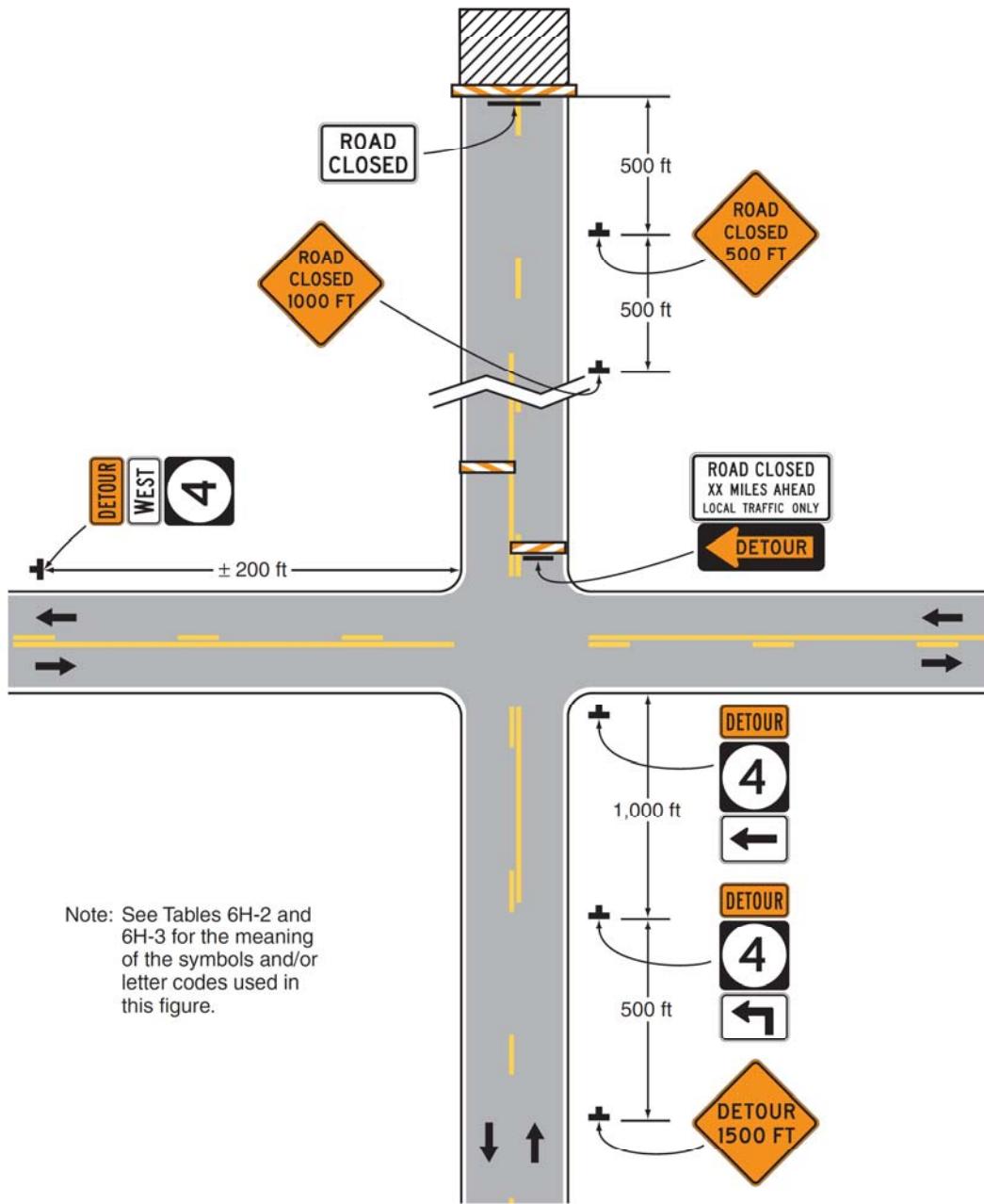
Guidance:

1. *Regulatory traffic control devices should be modified as needed for the duration of the detour.*

Option:

2. If the road is opened for some distance beyond the intersection and/or there are significant origin/ destination points beyond the intersection, the ROAD CLOSED and DETOUR signs on Type 3 Barricades may be located at the edge of the traveled way.
3. A Route Sign Directional assembly may be placed on the far left corner of the intersection to augment or replace the one shown on the near right corner.
4. Flashing warning lights and/or flags may be used to call attention to the advance warning signs.
5. Cardinal direction plaques may be used with route signs.

Figure 6H-8. Road Closure with an Off-Site Detour (TA-8)



Notes for Figure 6H-18—Typical Application 18 Lane Closure on a Minor Street

Standard:

- 1. This TTC shall be used only for low-speed facilities having low traffic volumes.**

Option:

2. Where the work space is short, where road users can see the roadway beyond, and where volume is low, vehicular traffic may be self-regulating.

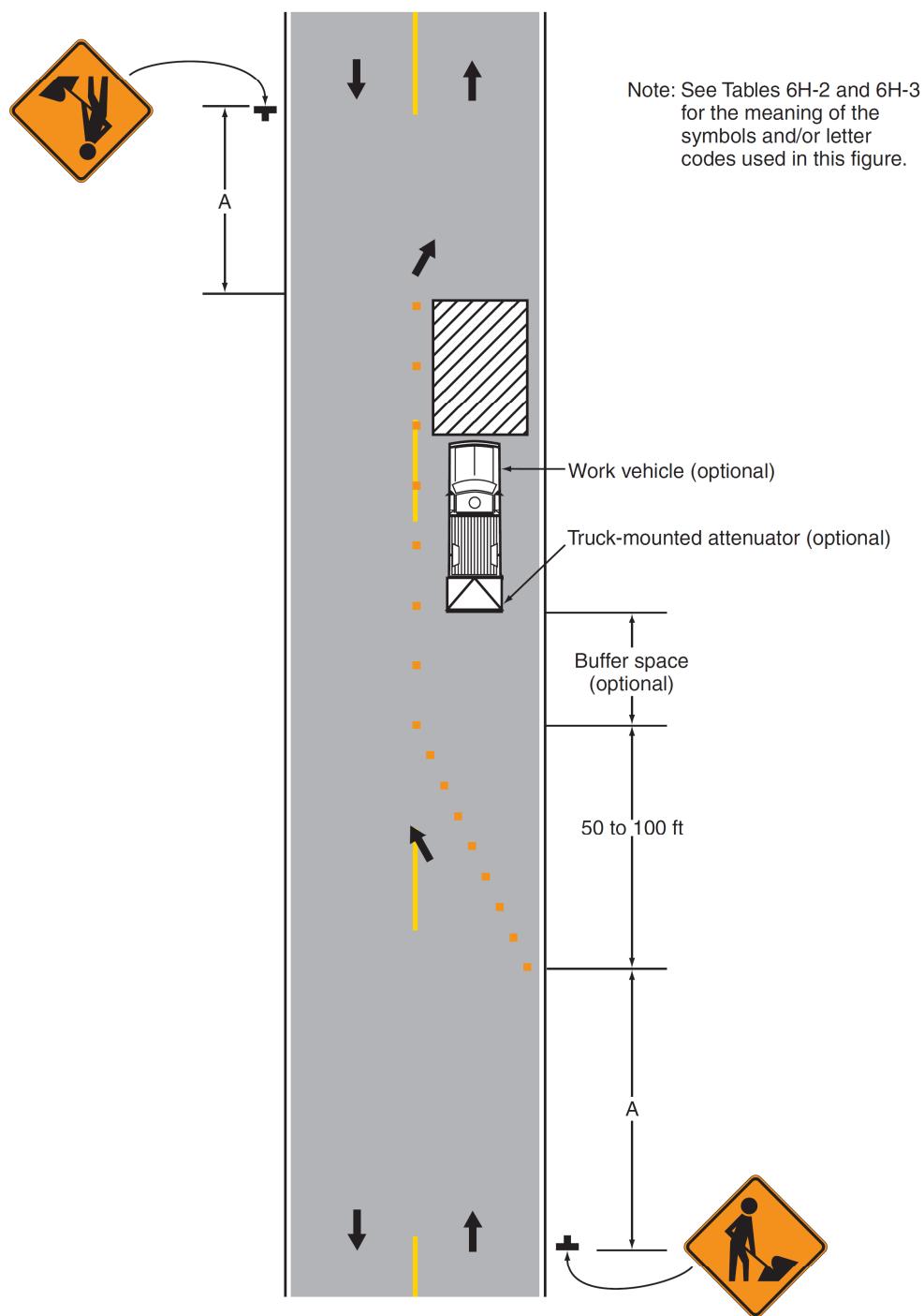
Standard:

- 3. Where vehicular traffic cannot effectively self-regulate, one or two flaggers shall be used as illustrated in Figure 6H-10 6H-10(CA).**

Option:

4. Flashing warning lights and/or flags may be used to call attention to the advance warning signs.
5. A truck-mounted attenuator may be used on the work vehicle and the shadow vehicle.

Figure 6H-18. Lane Closure on a Minor Street (TA-18)



Typical Application 18

Notes for Figure 6H-20—Typical Application 20 Detour for a Closed Street

Guidance:

1. *This plan should be used for streets without posted route numbers.*
2. *On multi-lane streets, Detour signs with an Advance Turn Arrow should be used in advance of a turn.*

Option:

3. Flashing warning lights and/or flags may be used to call attention to the advance warning signs.
4. Flashing warning lights may be used on Type 3 Barricades.
5. Detour signs may be located on the far side of intersections. A Detour sign with an advance arrow may be used in advance of a turn.
6. A Street Name sign may be mounted with the Detour sign. The Street Name sign may be either white on green or black on orange.

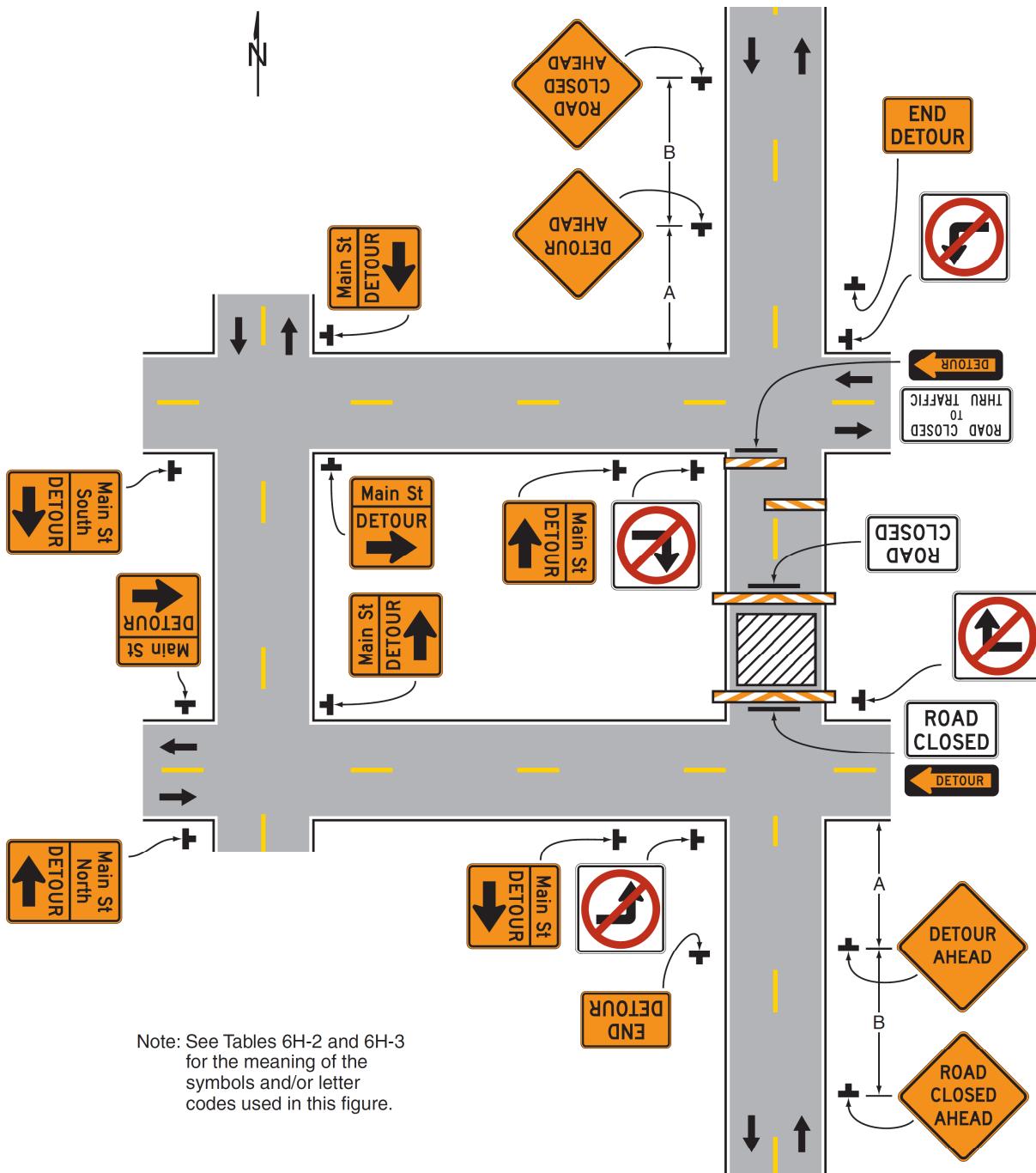
Standard:

7. **When used, the Street Name sign shall be placed above the Detour sign.**

Support:

8. See Figure 6H-9 for the information for detouring a numbered highway.

Figure 6H-20. Detour for a Closed Street (TA-20)



Typical Application 20

Notes for Figure 6H-23—Typical Application 23 Left-Hand Lane Closure on the Far Side of an Intersection

Guidance:

- 1. If the work space extends across a crosswalk, the crosswalk should be closed using the information and devices shown in Figure 6H-29.*

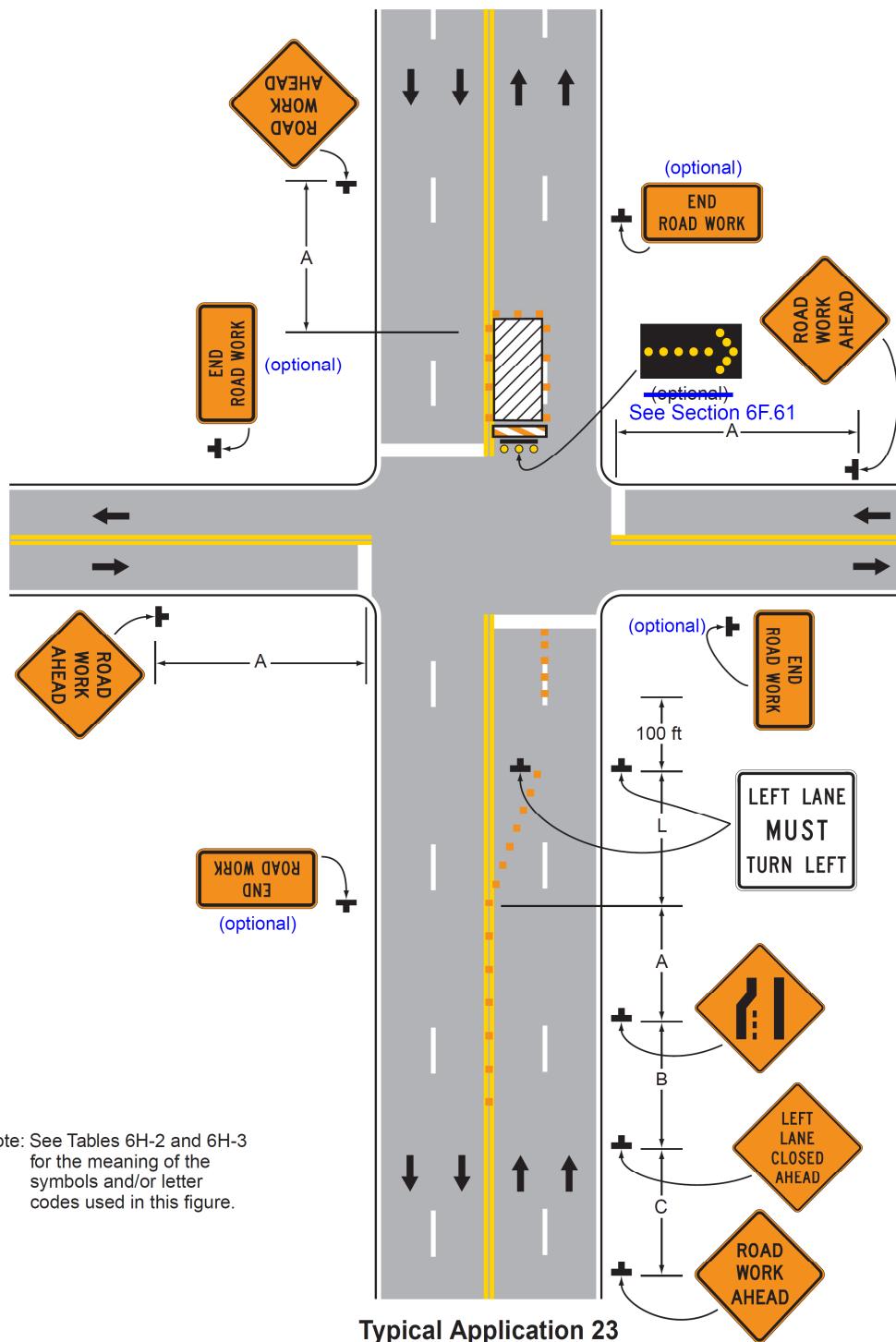
Option:

2. Flashing warning lights and/or flags may be used to call attention to the advance warning signs.
3. The normal procedure is to close on the near side of the intersection any lane that is not carried through the intersection. However, when this results in the closure of a left lane having significant left-turning movements, then the left lane may be reopened as a turn bay for left turns only, as shown.

Support:

4. By first closing off the left lane and then reopening it as a turn bay, the left-turn bay allows storage of turning vehicles so that the movement of through traffic is not impeded. A left-turn bay that is long enough to accommodate all turning vehicles during a traffic signal cycle will provide the maximum benefit for through traffic. Also, an island is created with channelizing devices that allows the LEFT LANE MUST TURN LEFT sign to be repeated on the left adjacent to the lane that it controls.

Figure 6H-23. Left-Hand Lane Closure on the Far Side of an Intersection (TA-23)



Notes for Figure 6H-24 and 6H-24A(CA) —Typical Application 24 Half Road Closure on the Far Side of an Intersection

Guidance:

1. If the work space extends across a crosswalk, the crosswalk should be closed using the information and devices shown in Figure 6H-29.
2. When turn prohibitions are implemented, two turn prohibition signs should be used, one on the near side and, space permitting, one on the far side of the intersection.

Option:

3. A buffer space may be used between opposing directions of vehicular traffic as shown in this application.
4. The normal procedure is to close on the near side of the intersection any lane that is not carried through the intersection. However, if there is a significant right-turning movement, then the right-hand lane may be restricted to right turns only, as shown.
5. Where the turning radius is large, a right-turn island using channelizing devices or pavement markings may be used.
6. There may be insufficient space to place the back-to-back Keep Right sign and No Left Turn symbol signs at the end of the row of channelizing devices separating opposing vehicular traffic flows. In this situation, the No Left Turn symbol sign may be placed on the right and the Keep Right sign may be omitted.
7. For intersection approaches reduced to a single lane, left-turning movements may be prohibited to maintain capacity for through vehicular traffic.
8. Flashing warning lights and/or flags may be used to call attention to advance warning signs.
9. Temporary pavement markings may be used to delineate the travel path through the intersection.

Support:

10. Keeping the right-hand lane open increases the through capacity by eliminating right turns from the open through lane.
11. A temporary turn island reinforces the nature of the temporary exclusive right-turn lane and enables a second RIGHT LANE MUST TURN RIGHT sign to be placed in the island.
12. Figure 6H-24 is appropriate for situations where the approach is stop-controlled (Stop sign and/or red flashing beacons) due to the abrupt transition through the intersection.
13. Figure 6H-24A(CA) is appropriate for situations where the approach is uncontrolled or controlled by traffic signals.

Figure 6H-24. Half Road Closure on the Far Side of an Intersection (TA-24)

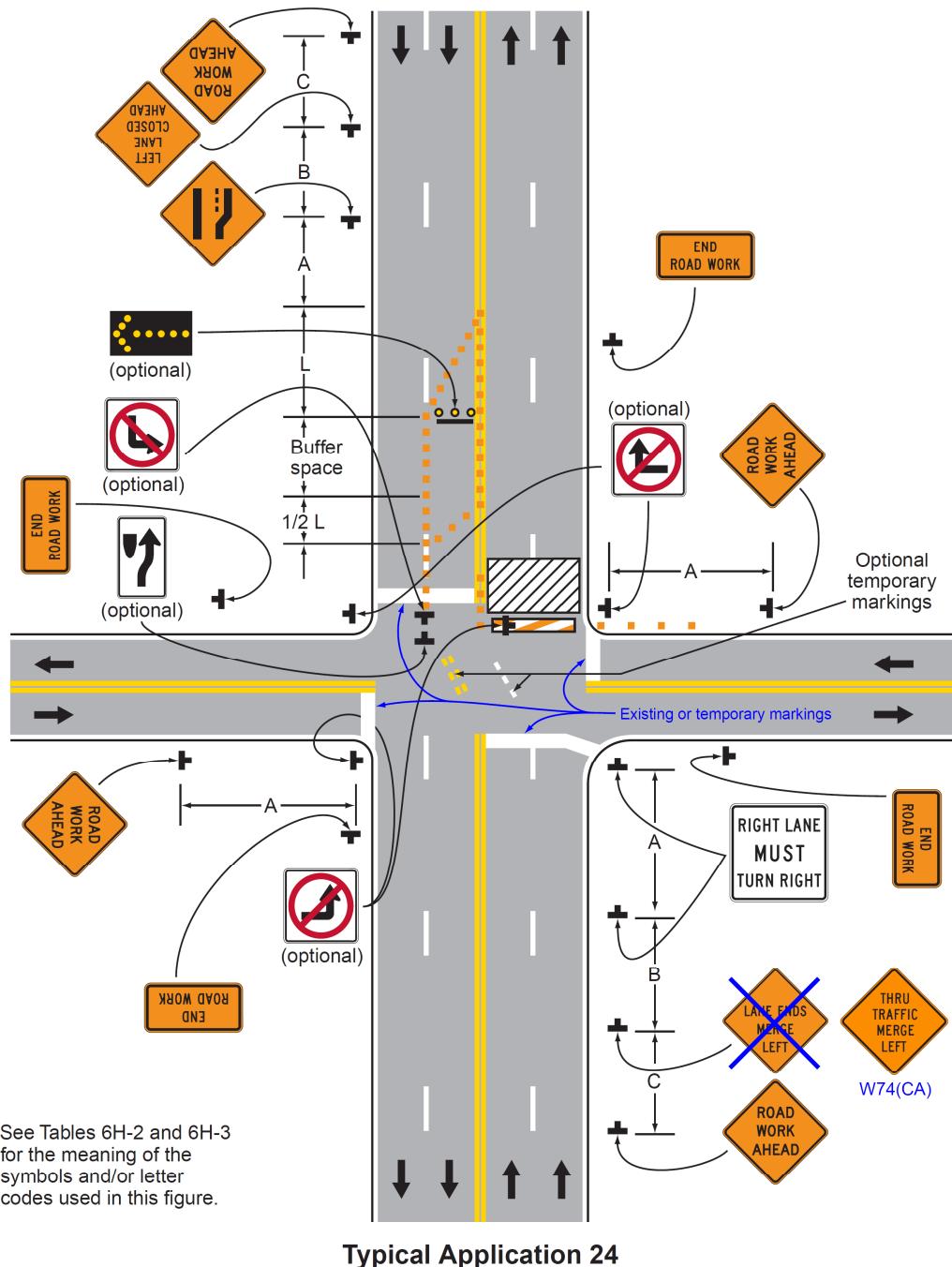
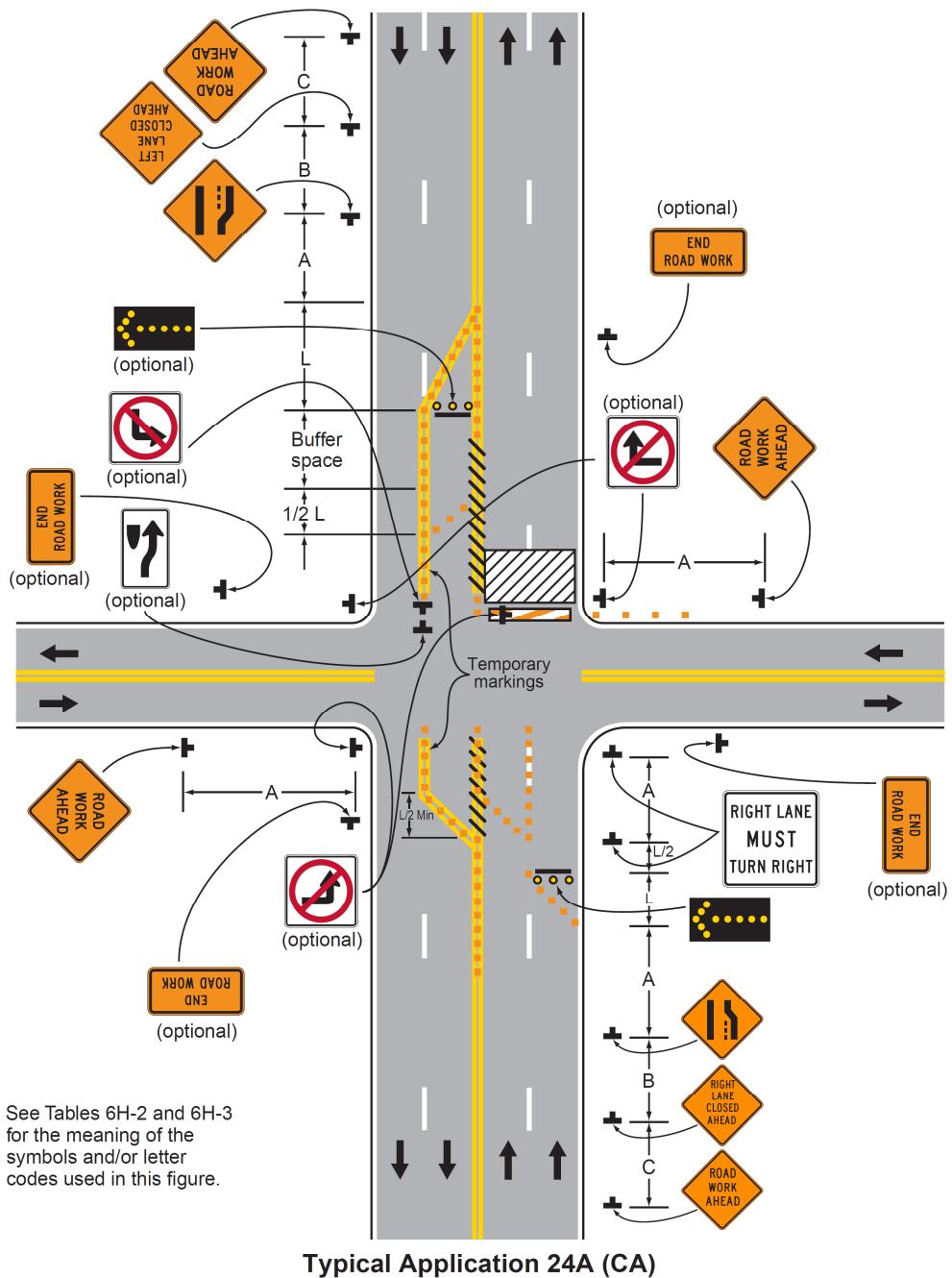


Figure 6H-24A (CA). Half Road Closure on the Far Side of an Intersection (TA-24A(CA))



Notes for Figure 6H-26—Typical Application 26 Closure in the Center of an Intersection

Guidance:

1. All lanes should be a minimum of 10 feet in width as measured to the near face of the channelizing devices.

Option:

2. A high-level warning device may be placed in the work space, if there is sufficient room.
3. For short-term use on low-volume, low-speed roadways with vehicular traffic that does not include longer and wider heavy commercial vehicles, a minimum lane width of 9 feet may be used.

Standard:

Note #3 is not applicable for State highways. Note #1 shall be used instead for State highways.

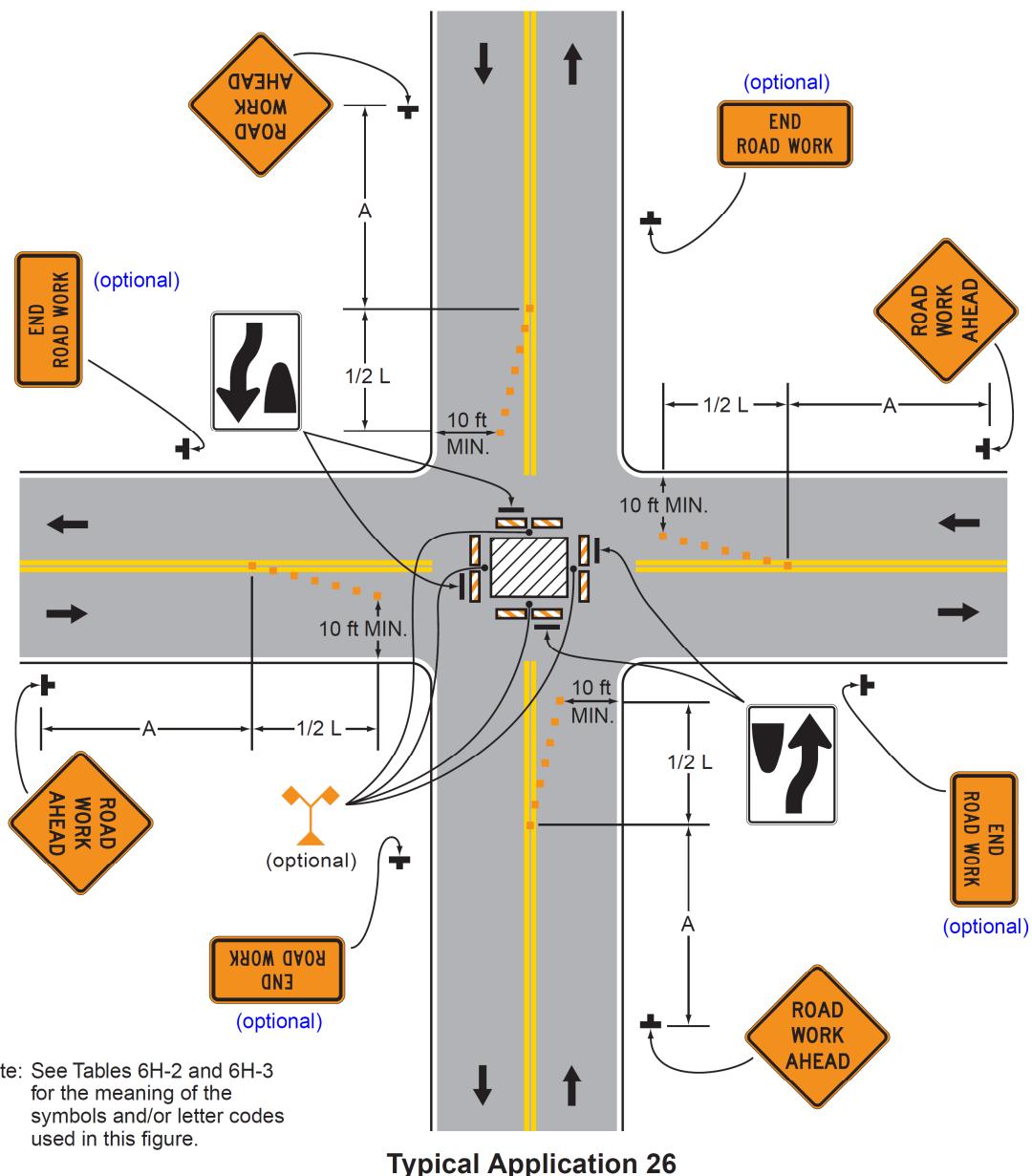
Option:

4. Flashing warning lights and/or flags may be used to call attention to advance warning signs.
5. Unless the streets are wide, it may be physically impossible to turn left, especially for large vehicles. Left turns may be prohibited as required by geometric conditions.
6. For short-duration work operations, the channelizing devices may be eliminated if a vehicle displaying high-intensity rotating, flashing, oscillating, or strobe lights is positioned in the work space.
7. Vehicle hazard warning signals may be used to supplement high-intensity rotating, flashing, oscillating, or strobe lights.

Standard:

8. **Vehicle hazard warning signals shall not be used instead of the vehicle's high-intensity rotating, flashing, oscillating, or strobe lights.**

Figure 6H-26. Closure in the Center of an Intersection (TA-26)



Note: See Tables 6H-2 and 6H-3 for the meaning of the symbols and/or letter codes used in this figure.

Notes for Figure 6H-27—Typical Application 27 Closure at the Side of an Intersection

Guidance:

1. *The situation depicted can be simplified by closing one or more of the intersection approaches. If this cannot be done, and/or when capacity is a problem, through vehicular traffic should be directed to other roads or streets.*
2. *Depending on road user conditions, flagger(s) or uniformed law enforcement officer(s) should be used to direct road users within the intersection.*

Standard:

- 3. At night, flagger stations shall be illuminated, except in emergencies.**

Option:

4. Flashing warning lights and/or flags may be used to call attention to the advance warning signs.
5. For short-duration work operations, the channelizing devices may be eliminated if a vehicle displaying high-intensity rotating, flashing, oscillating, or strobe lights is positioned in the work space.
6. A BE PREPARED TO STOP sign may be added to the sign series.

Guidance:

7. *When used, the BE PREPARED TO STOP sign should be located before after the Flagger symbol sign.*
8. *ONE LANE ROAD AHEAD signs should also be used to provide adequate advance warning.*

Support:

9. Turns can be prohibited as required by vehicular traffic conditions. Unless the streets are wide, it might be physically impossible to make certain turns, especially for large vehicles.

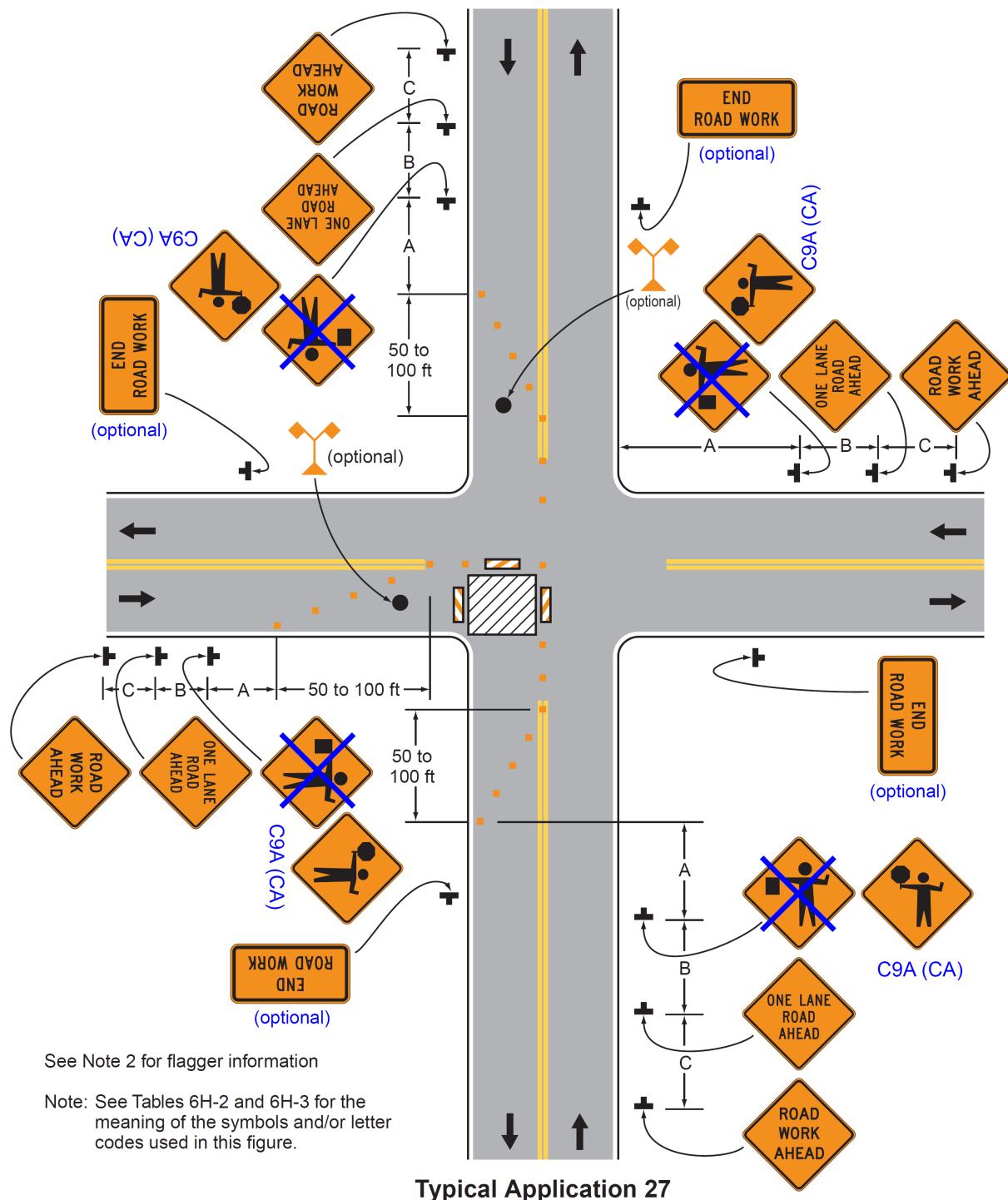
Option:

10. Vehicle hazard warning signals may be used to supplement high-intensity rotating, flashing, oscillating, or strobe lights.

Standard:

- 11. Vehicle hazard warning signals shall not be used instead of the vehicle's high-intensity rotating, flashing, oscillating, or strobe lights.**

Figure 6H-27. Closure at the Side of an Intersection (TA-27)



APPENDIX F

Air Quality Modeling Files

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APPENDIX 7

Emissions Calculations

EMFAC2011 Emissions Factors Applied to On-Road Truck Miles
Roadmod Data for Off-Road Equipment

Wildcat Berkeley 200 ft/day Total Emissions

Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | lbs/day | CO | NOx | PM-10 | PM-2.5 |
|-----------------------|----------------|-----------|------------|--------------|---------------|--------|
| Combined Total | ROG | | | | | |
| Pavement Removal | 5.5 | 16.5 | 34.4 | 11.0 | 3.0 | |
| Excavation | 5.9 | 19.0 | 35.5 | 11.4 | 3.3 | |
| Pipeline Install | 5.2 | 14.9 | 29.0 | 10.9 | 2.9 | |
| Paving | 5.6 | 17.6 | 33.9 | 1.4 | 1.2 | |
| Subtotals | | | | | | |
| ROADMOD | ROG | CO | NOx | PM-10 | PM-2.5 | |
| OffRoad Equipment | 2.6 | 15.0 | 13.9 | 10.8 | 2.8 | |
| Pavement Removal | 2.9 | 17.5 | 15.0 | 11.2 | 3.1 | |
| Excavation | 2.2 | 13.4 | 8.5 | 10.7 | 2.6 | |
| Pipeline Install | 2.6 | 16.1 | 13.4 | 1.2 | 1.0 | |
| EMFAC 2011 | lbs/day | CO | NOx | PM-10 | PM-2.5 | |
| OnRoad Haul | ROG | | | | | |
| 1960 miles/day | 2.98 | 1.52 | 20.51 | 0.22 | 0.20 | |
| GHG | Annual CO2 | tons/year | tons/year | | | |
| Roadmod | EMFAC | Total | | | | |
| 59.8 | 89.2 | 149.00 | | | | |

Wildcat Berkeley Total Emissions W Haul Truck Mitigation (Ave Year 2010)

Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | ROG | CO | lbs/day | NOx | PM-10 | PM-2.5 |
|-----------------------|------------|------------|-----------|----------------|------------|--------------|---------------|
| Combined Total | | | | | | | |
| Pavement Removal | | 2.9 | 16.8 | 19.2 | 11.0 | 3.0 | |
| Excavation | | 3.2 | 19.2 | 20.3 | 11.4 | 3.3 | |
| Pipeline Install | | 2.6 | 15.2 | 13.8 | 10.9 | 2.8 | |
| Paving | | 2.9 | 17.8 | 18.7 | 1.4 | 1.2 | |
| Subtotals | | | | | | | |
| ROADMOD | | ROG | CO | lbs/day | NOx | PM-10 | PM-2.5 |
| OffRoad Equipment | | 2.6 | 15.0 | 13.9 | 10.8 | 2.8 | |
| Pavement Removal | | 2.9 | 17.5 | 15.0 | 11.2 | 3.1 | |
| Excavation | | 2.2 | 13.4 | 8.5 | 10.7 | 2.6 | |
| Pipeline Install | | 2.6 | 16.1 | 13.4 | 1.2 | 1.0 | |
| EMFAC | | ROG | CO | lbs/day | NOx | PM-10 | PM-2.5 |
| OnRoad Haul | | 0.32 | 1.77 | 5.30 | 0.21 | 0.20 | |
| 1960 miles/day | | | | | | | |
| GHG | Annual CO2 | tons/year | | | | | |
| Roadmod | EMFAC | Total | | | | | |
| 59.8 | 87.9 | 147.70 | | | | | |

Wildcat El Cerrito 200 ft/day Total Emissions
Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | ROG | CO | lbs/day | NOx | PM-10 | PM-2.5 |
|-----------------------|-------------|-----------------------|-------------------|---------|------|-------|--------|
| Combined Total | | | | | | | |
| Pavement Removal | | 5.0 | 15.6 | 30.5 | 11.0 | 2.9 | |
| Excavation | | 5.4 | 18.7 | 32.2 | 11.4 | 3.3 | |
| Pipeline Install | | 4.6 | 14.0 | 25.2 | 10.9 | 2.8 | |
| Paving | | 5.2 | 17.3 | 30.7 | 1.4 | 1.2 | |
| Subtotals | | | | | | | |
| ROADMOD | | | | | | | |
| OffRoad Equipment | | 2.5 | 14.3 | 13.8 | 10.8 | 2.8 | |
| Pavement Removal | | 3.0 | 17.5 | 15.5 | 11.2 | 3.1 | |
| Excavation | | 2.2 | 12.8 | 8.5 | 10.7 | 2.6 | |
| Pipeline Install | | 2.8 | 16.1 | 14.0 | 1.2 | 1.1 | |
| EMFAC | Truck miles | ROG | CO | lbs/day | NOx | PM-10 | PM-2.5 |
| OnRoad Haul | | | | | | | |
| 1598 miles/day | | 2.43 | 1.24 | 16.72 | 0.18 | 0.16 | |
| GHG | | Annual CO2 Roadmod | ton/year EMFAC | Total | | | |
| | | 115.0 | 120.6 | 235.60 | | | |

Wildcat El Cerrito 200 ft/day Total Emissions W Haul Truck Mitigation (Ave Year 2010)

Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-----------------------|-----|------|------|------|-------|--------|
| Combined Total | | | | | | |
| Pavement Removal | 2.8 | 15.8 | 18.1 | 11.0 | 2.9 | |
| Excavation | 3.3 | 18.9 | 19.9 | 11.4 | 3.3 | |
| Pipeline Install | 2.5 | 14.2 | 12.8 | 10.8 | 2.8 | |
| Paving | 3.0 | 17.5 | 18.3 | 1.4 | 1.2 | |

Subtotals

| ROADMOD | ROG | CO | NOx | PM-10 | PM-2.5 |
|-------------------|-----|------|------|-------|--------|
| OffRoad Equipment | 2.5 | 14.3 | 13.8 | 10.8 | 2.8 |
| Pavement Removal | 3.0 | 17.5 | 15.5 | 11.2 | 3.1 |
| Excavation | 2.2 | 12.8 | 8.5 | 10.7 | 2.6 |
| Pipeline Install | 2.8 | 16.1 | 14.0 | 1.2 | 1.1 |
| Paving | | | | | |

| EMFAC | ROG | CO | NOx | PM-10 | PM-2.5 |
|----------------|------|------|------|-------|--------|
| OnRoad Haul | 0.26 | 1.44 | 4.32 | 0.17 | 0.16 |
| 1598 miles/day | | | | | |

| GHG | Annual CO2 Roadmod | tons/year EMFAC | Total |
|-----|-----------------------|--------------------|--------|
| | 115.0 | 120.6 | 235.60 |

CPZ EI Cerrito to Richmond 200 ft/day
Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-----------------------|-----|------|------|------|-------|--------|
| Combined Total | | | | | | |
| Pavement Removal | 1.8 | 11.6 | 14.8 | 10.6 | 2.6 | |
| Excavation | 2.0 | 15.7 | 15.4 | 10.8 | 2.9 | |
| Pipeline Install | 1.6 | 11.7 | 12.1 | 10.6 | 2.6 | |
| Paving | 1.9 | 14.4 | 15.0 | 0.8 | 0.7 | |

Subtotals

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-------------------|-----|------|------|------|-------|--------|
| ROADMOD | | | | | | |
| OffRoad Equipment | 1.6 | 10.3 | 9.4 | 10.5 | 2.5 | |
| Pavement Removal | 1.8 | 14.4 | 10.0 | 10.7 | 2.7 | |
| Excavation | 1.3 | 10.4 | 6.7 | 10.4 | 2.4 | |
| Pipeline Install | 1.6 | 13.2 | 9.6 | 0.7 | 0.5 | |
| Paving | | | | | | |

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-------------------------------|------|------|------|------|-------|--------|
| EMFAC | | | | | | |
| OnRoad Haul 1552 miles/day | 0.23 | 1.27 | 5.42 | 0.15 | 0.14 | |

| GHG | Annual CO2 Roadmod | tons/year EMFAC | Total |
|-----|-----------------------|--------------------|--------|
| | 122.0 | 99.8 | 221.80 |

CPZ Richmond to San Pablo 200 ft/day
Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-----------------------|-----|------|------|------|-------|--------|
| Combined Total | | | | | | |
| Pavement Removal | 1.8 | 11.8 | 16.2 | 10.7 | 2.6 | |
| Excavation | 2.1 | 15.9 | 16.8 | 10.9 | 2.8 | |
| Pipeline Install | 1.4 | 11.0 | 12.8 | 10.6 | 2.5 | |
| Paving | 1.9 | 14.6 | 16.4 | 0.9 | 0.8 | |

Subtotals

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-------------------|-----|------|-----|------|-------|--------|
| ROADMOD | | | | | | |
| OffRoad Equipment | 1.5 | 10.1 | 9.2 | 10.5 | 2.5 | |
| Pavement Removal | 1.8 | 14.2 | 9.8 | 10.7 | 2.6 | |
| Excavation | 1.1 | 9.4 | 5.8 | 10.4 | 2.4 | |
| Pipeline Install | 1.6 | 13.0 | 9.5 | 0.7 | 0.6 | |
| Paving | | | | | | |

| | | ROG | CO | NOx | PM-10 | PM-2.5 |
|-------------------------------|------|------|------|------|-------|--------|
| EMFAC 2011 | | | | | | |
| OnRoad Haul 1960 miles/day | 0.30 | 1.63 | 6.98 | 0.19 | 0.18 | |

| GHG | Annual CO2 Roadmod | tons/year EMFAC | Total |
|-----|-----------------------|--------------------|--------|
| | 123.0 | 100 | 223.00 |

CPZ Bridge

Roadmod for Construction Equipment and EMFAC for Truck Haul

| | | ROG | CO | NOx | PM-10 | PM-2.5 | lbs/day |
|-------------------------|------------|-----------|------|-------|--------|----------|---------|
| Combined Total | | | | | | | |
| Clear/Grub | 1.0 | 5.6 | 8.0 | 1.3 | 0.5 | 0.5 | |
| Abutment | 1.1 | 7.2 | 8.8 | 1.4 | 0.5 | 0.5 | |
| Bridge Erection | 0.9 | 7.1 | 7.6 | 2.4 | 0.7 | 0.7 | |
| Pipeline Install | 0.9 | 5.5 | 6.5 | 0.3 | 0.3 | 0.3 | |
| Subtotals | | | | | | | |
| ROADMOD | | | | | | | |
| OffRoad Equipment | ROG | CO | NOx | PM-10 | PM-2.5 | | |
| Clear/Grub | 0.9 | 5.1 | 5.7 | 1.3 | 0.4 | | |
| Abutment | 1.0 | 6.7 | 6.5 | 1.3 | 0.5 | | |
| Bridge Erection | 0.8 | 6.5 | 5.4 | 2.3 | 0.7 | | |
| Pipeline Install | 0.8 | 5.0 | 4.2 | 0.3 | 0.2 | | |
| EMFAC | | | | | | | |
| OnRoad Haul | ROG | CO | NOx | PM-10 | PM-2.5 | CO2 | |
| 640 miles/day | 0.10 | 0.53 | 2.28 | 0.06 | 0.06 | 1299.907 | |
| GHG | Annual CO2 | tons/year | | | | | |
| Roadmod | EMFAC | Total | | | | | |
| 16.1 | 22.3 | 38.40 | | | | | |

CPZ Jack and Bore

Roadmod for Construction Equipment and EMFAC for Truck Haul

| | ROG | CO | NOx | PM-10 | PM-2.5 |
|----------------|------------|-----------|------------|--------------|---------------|
| Pit Excavation | 1.2 | 8.9 | 7.8 | 1.4 | 0.5 |
| Casing Install | 0.8 | 4.5 | 4.2 | 1.2 | 0.4 |
| Pipe Install | 1.0 | 6.3 | 4.6 | 2.2 | 0.6 |
| Backfill | 0.6 | 6.0 | 3.7 | 0.2 | 0.2 |

Subtotals

| | ROG | CO | NOx | PM-10 | PM-2.5 |
|-------------------|------------|-----------|------------|--------------|---------------|
| OffRoad Equipment | 1.2 | 8.9 | 7.5 | 1.4 | 0.5 |
| Pit Excavation | 0.7 | 4.5 | 3.9 | 1.2 | 0.4 |
| Casing Install | 1.0 | 6.2 | 4.3 | 2.2 | 0.6 |
| Pipe Install | 0.6 | 6.0 | 3.4 | 0.2 | 0.2 |
| Backfill | | | | | |

EMFAC 2011

| | ROG | CO | NOx | PM-10 | PM-2.5 |
|--------------|------------|-----------|------------|--------------|---------------|
| OnRoad Haul | | | | | |
| 84 miles/day | 0.01 | 0.07 | 0.30 | 0.01 | 0.01 |

| GHG | Annual CO2 Roadmod | tons/year EMFAC | Total |
|-----|-----------------------|--------------------|-------|
| | 74.6 | 4.3 | 78.90 |

EMFAC2011 Emissions Factors Used to Calculate On-Road Truck Miles

EMFAC2011 Data

| Large Diesel Truck Emissions for Calendar Year 2016 Aggregate Years Fleet 50 MPH | | | | | | |
|--|-------------|----------------|------------|------|------------|---------------------|
| EMFAC2011 Emission Rates | | | | | | |
| Region Type: Air District | | | | | | |
| Region: Bay Area AQMD | | | | | | |
| Calendar Year: 2016 | | | | | | |
| Season: Annual | | | | | | |
| Vehicle Classification: EMFAC2011 Categories | | | | | | |
| Region | CalYr | Season | Veh_Class | Fuel | MdYr | Speed (miles/hr) |
| Bay Area A | 2016 Annual | T6 instate DSL | Aggregated | 50 | 0.06921856 | 0.07880066 |
| Large Diesel Truck Emissions for Year 2016 Fleet: 2010 or Newer, 50 MPH | | | | | | |
| EMFAC2011 Emission Rates | | | | | | |
| Region Type: Air District | | | | | | |
| Region: Bay Area AQMD | | | | | | |
| Calendar Year: 2016 | | | | | | |
| Season: Annual | | | | | | |
| Vehicle Classification: EMFAC2011 Categories | | | | | | |
| Region | CalYr | Season | Veh_Class | Fuel | MdYr | Speed (miles/hr) |
| Bay Area A | 2016 Annual | T6 instate DSL | 2010 | 50 | 0.07525322 | 0.085670068 |
| Large Diesel Truck Emissions for Calendar Year 2021Aggregate Years Fleet 50 MPH | | | | | | |
| Calendar Year: 2021 | | | | | | |
| Season: Annual | | | | | | |
| Vehicle Classification: EMFAC2011 Categories | | | | | | |
| Region | CalYr | Season | Veh_Class | Fuel | MdYr | Speed (miles/hr) |
| Bay Area A | 2021 Annual | T6 instate DSL | Aggregated | 50 | 0.06951099 | 0.079132967 |
| Large Diesel Truck Emissions for Calendar Year 2021Aggregate Years Fleet 50 MPH | | | | | | |
| Vehicle Classification: EMFAC2011 Categories | | | | | | |
| Region | CalYr | Season | Veh_Class | Fuel | MdYr | Speed (miles/hr) |
| Bay Area A | 2021 Annual | T6 instate DSL | Aggregated | 50 | 0.06951099 | 0.0790589 |
| Large Diesel Truck Emissions for Calendar Year 2021Aggregate Years Fleet 50 MPH | | | | | | |

EMFAC2011 Emissions Factors Used to Calculate On-Road Truck Miles

| CalYr | MdlYr | CO2_RUNEX(Pavley I+LCFS) | PM10_RUNEX (gms/mile) | PM2_5_RUNEX (gms/mile) |
|-------|------------|--------------------------|--------------------------|---------------------------|
| 2016 | Aggregated | 1000.355106 | 0.050839557 | 0.046772393 |

| CalYr | MdlYr | CO2_RUNEX(Pavley I+LCFS) | PM10_RUNEX (gms/mile) | PM2_5_RUNEX (gms/mile) |
|-------|-------|--------------------------|--------------------------|---------------------------|
| 2016 | 2010 | 985.9377757 | 0.049360409 | 0.045411577 |

| CalYr | MdlYr | CO2_RUNEX(Pavley I+LCFS) | PM10_RUNEX (gms/mile) | PM2_5_RUNEX (gms/mile) |
|-------|------------|--------------------------|--------------------------|---------------------------|
| 2021 | Aggregated | 923.2294683 | 0.044637782 | 0.041066676 |

| Wildcat | 200 ft./day | 2016 Aggregate Years | EMFAC2011 On-Road Haul Calculations | | | | | |
|------------------------------|-------------|----------------------|-------------------------------------|-------|------------------|------|-------------------|--|
| | | | Daily Off Road Truck Emissions | | | | (from Appendix B) | |
| | ROG | CO | NOx | PM10 | PM2.5 | CO2 | | |
| EMFAC2011 | grams/mile | 0.69219 | 0.35 | 4.76 | 0.05 | 0.05 | 1000.36 | |
| | lbs/mile | 0.001522818 | 0.00 | 0.01 | 0.00 | 0.00 | 2.20 | |
| Wildcat El Cerrito | miles/day | 1598 | | | | | | |
| Wildcat El Cerrito | lbs/day | 2.43 | 1.24 | 16.72 | 0.18 | 0.16 | 3516.85 | |
| Wildcat Berkeley | miles/day | 1960 | | | | | | |
| Wildcat Berkeley | lbs/day | 2.98 | 1.52 | 20.51 | 0.22 | 0.20 | 4313.53 | |
| | | | | | | | | |
| Mileage Per Day Calculations | | | GHG | | | | | |
| Wildcat El Cerrito | El Cerrito | 23 | Haul trips | 66 | Annual tons/year | | | |
| | | 4 | Material trips | 20 | tons CO2e | | | |
| | Total Daily | 1598 | miles | | | | | |
| Wildcat Berkeley | Berkeley | 31 | Haul trips | 60 | miles rt | | | |
| | | 5 | Material trips | 20 | miles rt | | | |
| | Total Daily | 1960 | miles | | | | | |
| | | | | | | | | |
| Wildcat El Cerrito | # haul days | | | | | | | |
| Wildcat Berkeley | 41 | 88.4 | 89.2 | | | | | |

EMFAC2011 On-Road Haul Calculations

| | Wildcat | 200 ft/day | 2016 2010 and Newer | Daily Off Road Truck Emissions (from Appendix B) | | | | |
|---|-------------|------------|---------------------|---|----------------|------|-----------|----------|
| EMFAC2011 | | | | ROG | CO | NOx | PM10 | CO2 |
| | grams/mile | 0.075 | 0.41 | | 1.23 | 0.05 | PM2.5 | 985.94 |
| | lbs/mile | 0.000165 | 0.00 | | 0.00 | 0.00 | 0.05 | 2.17 |
| WC El Cerrito | miles day | 1598 | | | | | 0.00 | |
| WC El Cerrito | lbs day | 0.26 | 1.44 | 4.32 | 0.17 | 0.16 | | 3466.16 |
| WC Berkeley | miles day | 1960 | | | | | | |
| WC Berkeley | lbs day | 0.32 | 1.77 | 5.30 | 0.21 | 0.20 | | 4251.36 |
| Mileage Per Day Calculations | | | | | | | | |
| | El Cerrito | | | 23 | Haul trips | | 66 | miles rt |
| | | | | 4 | Material trips | | 20 | miles rt |
| T-15 | Total Daily | 1598 | | | miles | | | |
| | Berkeley | | | 31 | Haul trips | | 60 | milesrt |
| | | | | 5 | Material trips | | 20 | milesrt |
| | Total Daily | 1960 | | | miles | | | |
| GHG | | | | | | | | |
| | # haul days | | Annual Tons/year | | | | | |
| WC El Cerrito | 68 | | tons CO2e | | | | tons CO2e | |
| | | | 117.85 | | | | 118.91 | |
| WC Berkeley | 41 | | | 87.15 | | | 87.94 | |

EMFAC2011 On-Road Haul Calculations

| Central Pressure Zone | 200 ft day | 2021 Aggregate Years | | EMFAC 2011 Daily Off Road Truck Emissions | | | | (from Appendix B) |
|-----------------------|------------|----------------------|------|---|------|-------|---------|-------------------|
| | | ROG | CO | NOx | PM10 | PM2.5 | CO2 | |
| EMFAC2011 | | 0.07 | 0.38 | 1.62 | 0.04 | 0.04 | 923.23 | |
| | grams/mile | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.03 | |
| CPZ El Cerrito | | 1522 | | | | | | |
| CPZ El Cerrito | miles day | 0.23 | 1.27 | 5.42 | 0.15 | 0.14 | 3091.34 | |
| CPZ Richmond | lbs day | 1960 | | | | | | |
| CPZ Richmond | miles day | 0.30 | 1.63 | 6.98 | 0.19 | 0.18 | 3980.97 | |
| | lbs day | | | | | | | |

| Mileage Per Day Calculations | | | | | |
|------------------------------|------------------|-------------|----------------|----|----------|
| CPZ El Cerrito | El Cerrito | 23 | Haul trips | 64 | miles rt |
| | | 4 | Material trips | 20 | miles rt |
| Total Daily | | 1552 | miles | | |
| CPZ Richmond | Richmond-San Pal | 31 | Haul trips | 60 | milesrt |
| | | 5 | Material trips | 20 | milesrt |
| Total Daily | | 1960 | miles | | |

| GHG | | | |
|------------------|-------------|-----------|-----------|
| Annual Tons/year | | | |
| CPZ El Cerrito | # haul days | tons CO2e | tons CO2e |
| | 64.00 | 98.92 | 99.81 |
| CPZ Richmond | | | |
| | 50.00 | 99.52 | 100.42 |

Bridge and Jack/Bore

EMFAC2011 On-Road Haul Calculations

| | | 2021 Aggregate Years | | EMFAC2011 | |
|---------------|------------|--------------------------------|------|-------------------------------|--------------|
| | | Daily Off Road Truck Emissions | | Daily On Road Truck Emissions | |
| | | CO | NOx | CO | PM2.5 |
| EMFAC2011 | grams/mile | ROG 0.07 | 0.38 | 1.62 0.04 | 0.04 0.00 |
| | lbs/mile | 0.00 | 0.00 | 0.00 0.00 | 0.00 0.00 |
| Bridge | miles/day | 640 | | | |
| Bridge | lbs/day | 0.10 | | | |
| Jack and Bore | miles/day | 84 | | | |
| Jack and Bore | lbs/day | 0.01 | | | |
| | | 0.07 | 0.30 | 0.01 0.01 | 0.01 0.01 |

| | | Mileage Per Day Calculations | | Mileage Per Day Calculations | |
|--|-------------|------------------------------|---------------------|------------------------------|-------------------------|
| | | Bridge | Bridge | Jack and Bore | Jack and Bore |
| | Total Daily | 0 | 10 | 1 | 1 |
| | | | Haul trips miles | Haul trips miles | Haul trips miles |
| | | | 640 | 64 | 64 |
| | | | | Material trips miles | Material trips miles |
| | | | | 20 | 20 |
| | Total Daily | 84 | | | |

| GHG | | Annual Tons/year | tons CO2e |
|---------------|-------------|-------------------|-----------|
| Bridge | # haul days | tons CO2 22.10 | 22.30 |
| Jack and Bore | 50 | 4.27 | 4.30 |

Road Construction Emissions Model, Version 6.3.2

| Emission Estimates for -> Wildcat Berkeley Pref Alt 4 200 LF Day | | | | | | | | | | | | | | | | | | | |
|--|---------------|--------------|---------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------|-------------------------------|----------------|--|--|--|--|--|--|--|--|--|
| Project Phases (English Units) | ROG (lbs/day) | CO (lbs/day) | NOx (lbs/day) | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) | Exhaust PM2.5 (lbs/day) | Fugitive Dust PM2.5 (lbs/day) | CO2 (lbs/day) | | | | | | | | | |
| Pavement Removal | 2.6 | 15.0 | 13.9 | 10.8 | 0.8 | 10.0 | 2.8 | 0.7 | 2.1 | 2,727.9 | | | | | | | | | |
| Grading/Excavation | 2.9 | 17.5 | 15.0 | 11.2 | 1.2 | 10.0 | 3.1 | 1.0 | 2.1 | 2,883.1 | | | | | | | | | |
| Pipe Installation | 2.2 | 13.4 | 8.5 | 10.7 | 0.7 | 10.0 | 2.6 | 0.6 | 2.1 | 2,165.0 | | | | | | | | | |
| Paving | 2.6 | 16.1 | 13.4 | 1.2 | 1.2 | - | 1.0 | 1.0 | - | 1,939.2 | | | | | | | | | |
| Maximum (pounds/day) | 2.9 | 17.5 | 15.0 | 11.2 | 1.2 | 10.0 | 3.1 | 1.0 | 2.1 | 2,883.1 | | | | | | | | | |
| Total (tons/construction project) | 0.1 | 0.4 | 0.3 | 0.3 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | 59.8 | | | | | | | | | |
| Notes: | | | | | | | | | | | | | | | | | | | |
| Project Start Year -> | 2015 | | | | | | | | | | | | | | | | | | |
| Project Length (months) -> | 3 | | | | | | | | | | | | | | | | | | |
| Total Project Area (acres) -> | 4 | | | | | | | | | | | | | | | | | | |
| Maximum Area Disturbed/Day (acres) -> | 1 | | | | | | | | | | | | | | | | | | |
| Total Soil Imported/Exported (yd ³ /day)-> | 0 | | | | | | | | | | | | | | | | | | |
| PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified. | | | | | | | | | | | | | | | | | | | |
| Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L. | | | | | | | | | | | | | | | | | | | |

PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified.
Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

| Emission Estimates for -> Wildcat Berkeley Pref Alt 4 200 LF Day | | | | | | | | | | | |
|--|---------------|--------------|---------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------|-------------------------------|----------------|--|
| Project Phases (Metric Units) | ROG (kgs/day) | CO (kgs/day) | NOx (kgs/day) | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) | Exhaust PM2.5 (kgs/day) | Fugitive Dust PM2.5 (kgs/day) | CO2 (kgs/day) | |
| Pavement Removal | 1.2 | 6.8 | 6.3 | 4.9 | 0.4 | 4.5 | 1.3 | 0.3 | 0.9 | 1,240.0 | |
| Grading/Excavation | 1.3 | 7.9 | 6.8 | 5.1 | 0.5 | 4.5 | 1.4 | 0.5 | 0.9 | 1,310.5 | |
| Pipe Installation | 1.0 | 6.1 | 3.9 | 4.9 | 0.3 | 4.5 | 1.2 | 0.3 | 0.9 | 984.1 | |
| Paving | 1.2 | 7.3 | 6.1 | 0.5 | 0.5 | - | 0.5 | 0.5 | - | 881.5 | |
| Maximum (kilograms/day) | 1.3 | 7.9 | 6.8 | 5.1 | 0.5 | 4.5 | 1.4 | 0.5 | 0.9 | 1,310.5 | |
| Total (megagrams/construction project) | 0.1 | 0.3 | 0.3 | 0.2 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | 54.2 | |

Road Construction Emissions Model, Version 6.3.2

| Emission Estimates for -> | | Wildcat EI Cerrito Pref Alt 1 200 Lf Day | | | | | |
|---|------------------|--|------------------|-------------------------|---------------------------|---------------------------------|--------------------------|
| Project Phases (English Units) | ROG (lbs/day) | CO (lbs/day) | NOx (lbs/day) | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) |
| Pavement Removal | 2.5 | 14.3 | 13.8 | 10.8 | 0.8 | 10.0 | 2.8 |
| Grading/Excavation | 3.0 | 17.5 | 15.5 | 11.2 | 1.2 | 10.0 | 3.1 |
| Pipe Installation | 2.2 | 12.8 | 8.5 | 10.7 | 0.7 | 10.0 | 2.6 |
| Paving | 2.8 | 16.1 | 14.0 | 1.2 | 1.2 | - | 0.6 |
| Maximum (pounds/day) | 3.0 | 17.5 | 15.5 | 11.2 | 1.2 | 10.0 | 3.1 |
| Total (tons/construction project) | 0.1 | 0.7 | 0.6 | 0.5 | 0.0 | 0.4 | 0.1 |
| Notes: | | | | | | | |
| Project Start Year -> | 2015 | | | | | | |
| Project Length (months) -> | 4 | | | | | | |
| Total Project Area (acres) -> | 3 | | | | | | |
| Maximum Area Disturbed/Day (acres) -> | 1 | | | | | | |
| Total Soil Imported/Exported (yd ³ /day)-> | 0 | | | | | | |

PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified.

Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

| Emission Estimates for -> | | Wildcat EI Cerrito Pref Alt 1 200 Lf Day | | | | | |
|---|------------------|--|------------------|-------------------------|---------------------------|---------------------------------|--------------------------|
| Project Phases (Metric Units) | ROG (kgs/day) | CO (kgs/day) | NOx (kgs/day) | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) |
| Pavement Removal | 1.1 | 6.5 | 6.3 | 4.9 | 0.4 | 4.5 | 1.3 |
| Grading/Excavation | 1.4 | 7.9 | 7.1 | 5.1 | 0.5 | 4.5 | 1.4 |
| Pipe Installation | 1.0 | 5.8 | 3.8 | 4.9 | 0.3 | 4.5 | 1.2 |
| Paving | 1.3 | 7.3 | 6.4 | 0.5 | 0.5 | - | 0.5 |
| Maximum (kilograms/day) | 1.4 | 7.9 | 7.1 | 5.1 | 0.5 | 4.5 | 1.4 |
| Total (megagrams/construction project) | 0.1 | 0.7 | 0.6 | 0.4 | 0.0 | 0.4 | 0.1 |

Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

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| Central Pressure Richmond-San Pablo Pref Alt 4 200 LF | | | | | | | | | |
|---|---------------|--------------|---------------|----------------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------------|
| Emission Estimates for -> Day | ROG (lbs/day) | CO (lbs/day) | NOx (lbs/day) | Total PM10 (lbs/day) | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) | Exhaust PM2.5 (lbs/day) |
| Project Phases (English Units) | | | | | | | | | Fugitive Dust PM2.5 (lbs/day) |
| Pavement Removal | 1.5 | 10.1 | 9.2 | 10.5 | 0.5 | 10.0 | 2.5 | 0.4 | 2.1 |
| Grading/Excavation | 1.8 | 14.2 | 9.8 | 10.7 | 0.7 | 10.0 | 2.6 | 0.6 | 2.1 |
| Pipe Installation | 1.1 | 9.4 | 5.8 | 10.4 | 0.4 | 10.0 | 2.4 | 0.3 | 2.1 |
| Paving | 1.6 | 13.0 | 9.5 | 0.7 | 0.7 | - | 0.6 | 0.6 | - |
| Maximum (pounds/day) | 1.8 | 14.2 | 9.8 | 10.7 | 0.7 | 10.0 | 2.6 | 0.6 | 2.1 |
| Total (tons/construction project) | 0.1 | 0.6 | 0.4 | 0.3 | 0.0 | 0.3 | 0.1 | 0.0 | 0.1 |
| Notes: | | | | | | | | | |
| Project Start Year -> | 2021 | | | | | | | | |
| Project Length (months) -> | 3 | | | | | | | | |
| Total Project Area (acres) -> | 2 | | | | | | | | |
| Maximum Area Disturbed/Day (acres) -> | 1 | | | | | | | | |
| Total Soil Imported/Exported (yd ³ /day)-> | 0 | | | | | | | | |

PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified.

Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

| Central Pressure Richmond-San Pablo Pref Alt 4 200 LF | | | | | | | | | |
|---|---------------|--------------|---------------|----------------------|----------------------|------------------------|------------------------------|-----------------------|-----------------------------|
| Emission Estimates for -> Day | ROG (kgs/day) | CO (kgs/day) | NOx (kgs/day) | Total PM10 (kgs/day) | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) | Exhaust PM2.5 (kgs/day) |
| Project Phases (Metric Units) | | | | | | | | | CO ₂ (kgs/ida y) |
| Pavement Removal | 0.7 | 4.6 | 4.2 | 4.8 | 0.2 | 4.5 | 1.1 | 0.2 | 0.9 |
| Grading/Excavation | 0.8 | 6.5 | 4.5 | 4.8 | 0.3 | 4.5 | 1.2 | 0.3 | 0.9 |
| Pipe Installation | 0.5 | 4.3 | 2.7 | 4.7 | 0.2 | 4.5 | 1.1 | 0.1 | 0.9 |
| Paving | 0.7 | 5.9 | 4.3 | 0.3 | 0.3 | - | 0.3 | 0.3 | - |
| Maximum (kilograms/day) | 0.8 | 6.5 | 4.5 | 4.8 | 0.3 | 4.5 | 1.2 | 0.3 | 0.9 |
| Total (megagrams/construction project) | 0.1 | 0.6 | 0.4 | 0.3 | 0.0 | 0.3 | 0.1 | 0.0 | 0.1 |
| Total (megagrams/day) | 0.1 | 0.6 | 0.4 | 0.3 | 0.0 | 0.3 | 0.1 | 0.0 | 0.1 |
| 1114 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |

| Emission Estimates for -> Central Pressure El Cerrito-Richmond Pref Alt 1 200 LF Day | | | | | | | | | |
|--|---------------|--------------|---------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------|-----------------------------|
| Project Phases (English Units) | ROG (lbs/day) | CO (lbs/day) | NOx (lbs/day) | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) | Exhaust PM2.5 (lbs/day) | Fugitive Dust CO2 (lbs/day) |
| Pavement Removal | 1.6 | 10.3 | 9.4 | 10.5 | 0.5 | 10.0 | 2.5 | 0.4 | 2.1 |
| Grading/Excavation | 1.8 | 14.4 | 10.0 | 10.7 | 0.7 | 10.0 | 2.6 | 0.6 | 2.1 |
| Pipe Installation | 1.3 | 10.4 | 6.7 | 10.4 | 0.4 | 10.0 | 2.4 | 0.3 | 2.1 |
| Paving | 1.6 | 13.2 | 9.6 | 0.7 | 0.7 | - | 0.6 | 0.6 | - |
| Maximum (pounds/day) | 1.8 | 14.4 | 10.0 | 10.7 | 0.7 | 10.0 | 2.6 | 0.6 | 2.1 |
| Total (tons/construction project) | 0.1 | 0.7 | 0.5 | 0.5 | 0.0 | 0.5 | 0.1 | 0.0 | 0.1 |
| Notes: | | | | | | | | | |
| Project Start Year -> | 2021 | | | | | | | | |
| Project Length (months) -> | 5 | | | | | | | | |
| Total Project Area (acres) -> | 3 | | | | | | | | |
| Maximum Area Disturbed/Day (acres) -> | 1 | | | | | | | | |
| Total Soil Imported/Exported (yd ³ /day)-> | 0 | | | | | | | | |

PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified. Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

| Emission Estimates for -> Central Pressure El Cerrito-Richmond Pref Alt 1 200 LF Day | | | | | | | | | |
|--|---------------|--------------|---------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------|-----------------------------|
| Project Phases (Metric Units) | ROG (kgs/day) | CO (kgs/day) | NOx (kgs/day) | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) | Exhaust PM2.5 (kgs/day) | Fugitive Dust CO2 (kgs/day) |
| Pavement Removal | 0.7 | 4.7 | 4.3 | 4.8 | 0.2 | 4.5 | 1.1 | 0.2 | 0.9 |
| Grading/Excavation | 0.8 | 6.6 | 4.5 | 4.9 | 0.3 | 4.5 | 1.2 | 0.3 | 0.9 |
| Pipe Installation | 0.6 | 4.7 | 3.1 | 4.7 | 0.2 | 4.5 | 1.1 | 0.2 | 0.9 |
| Paving | 0.7 | 6.0 | 4.4 | 0.3 | 0.3 | - | 0.3 | 0.3 | - |
| Maximum (kilograms/day) | 0.8 | 6.6 | 4.5 | 4.9 | 0.3 | 4.5 | 1.2 | 0.3 | 0.9 |
| Total (megagrams/construction project) | 0.1 | 0.6 | 0.4 | 0.4 | 0.0 | 0.4 | 0.1 | 0.0 | 0.1 |

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| Emission Estimates for -> CPZ Richmond to San Pablo Bridge Crossing | | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) | Exhaust PM2.5 (lbs/day) | Fugitive Dust PM2.5 (lbs/day) | | |
|---|------------------|-------------------------|---------------------------|---------------------------------|---------------------------|---------------------------------|----------------------------------|----------------------------|----------------------------------|
| Project Phases (English Units) | ROG (lbs/day) | CO (lbs/day) | NOx (lbs/day) | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) | Exhaust PM2.5 (lbs/day) | Fugitive Dust PM2.5 (lbs/day) |
| Grubbing/Land Clearing | 0.9 | 5.1 | 5.7 | 1.3 | 0.3 | 0.4 | 0.2 | 0.2 | 1,407.3 |
| Abutment Construction | 1.0 | 6.7 | 6.5 | 1.3 | 0.3 | 1.0 | 0.5 | 0.3 | 1,660.5 |
| Bridge Erection | 0.8 | 6.5 | 5.4 | 2.3 | 0.3 | 2.0 | 0.7 | 0.3 | 1,317.0 |
| Install Pipeline | 0.8 | 5.0 | 4.2 | 0.3 | 0.3 | - | 0.2 | 0.2 | - 1,083.6 |
| Maximum (pounds/day) | 1.0 | 6.7 | 6.5 | 2.3 | 0.3 | 2.0 | 0.7 | 0.3 | 1,660.5 |
| Total (tons/construction project) | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 16.1 |

Notes:

Project Start Year -> 2021

Project Length (months) -> 2

Total Project Area (acres) -> 0

Maximum Area Disturbed/Day (acres) -> 0

Total Soil Imported/Exported (yd³/day)-> 0

PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified.

Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

| Emission Estimates for -> CPZ Richmond to San Pablo Bridge Crossing | | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) | Exhaust PM2.5 (kgs/day) | Fugitive Dust PM2.5 (kgs/day) | CO ₂ (kgs/day) | |
|---|------------------|-------------------------|---------------------------|---------------------------------|---------------------------|---------------------------------|----------------------------------|------------------------------|----------------------------------|
| Project Phases (Metric Units) | ROG (kgs/day) | CO (kgs/day) | NOx (kgs/day) | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) | Exhaust PM2.5 (kgs/day) | Fugitive Dust PM2.5 (kgs/day) |
| Grubbing/Land Clearing | 0.4 | 2.3 | 2.6 | 0.6 | 0.1 | 0.5 | 0.2 | 0.1 | 0.1 |
| Abutment Construction | 0.5 | 3.0 | 3.0 | 0.6 | 0.1 | 0.5 | 0.2 | 0.1 | 0.1 |
| Bridge Erection | 0.4 | 3.0 | 2.4 | 1.0 | 0.1 | 0.9 | 0.3 | 0.1 | 0.2 |
| Install Pipeline | 0.4 | 2.3 | 1.9 | 0.1 | 0.1 | - | 0.1 | 0.1 | - 492.5 |
| Maximum (kilograms/day) | 0.5 | 3.0 | 3.0 | 1.0 | 0.1 | 0.9 | 0.3 | 0.1 | 0.2 |
| Total (megagrams/construction project) | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.6 |

Road Construction Emissions Model, Version 6.3.2

| Emission Estimates for -> CPZ Richmond to San Pablo Jack and Bore | | ROG (lbs/day) | | NOx (lbs/day) | | Total PM10 (lbs/day) | Exhaust PM10 (lbs/day) | Fugitive Dust PM10 (lbs/day) | Total PM2.5 (lbs/day) | Exhaust PM2.5 (lbs/day) | Fugitive Dust PM2.5 (lbs/day) |
|---|------------|---------------|--------------|---------------|--------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------|-------------------------------|
| Project Phases (English Units) | | CO (lbs/day) | CO (lbs/day) | CO (lbs/day) | CO (lbs/day) | | | | | | |
| Pit Excavation | 1.2 | 8.9 | 7.5 | 1.4 | 0.4 | 1.0 | 0.5 | 0.3 | 0.2 | 2,049.4 | |
| Casing Installation | 0.7 | 4.5 | 3.9 | 1.2 | 0.2 | 1.0 | 0.4 | 0.2 | 0.2 | 1,297.1 | |
| Pipeline Installation | 1.0 | 6.2 | 4.3 | 2.2 | 0.2 | 2.0 | 0.6 | 0.2 | 0.4 | 2,222.0 | |
| Backfill | 0.6 | 6.0 | 3.4 | 0.2 | 0.2 | - | 0.2 | 0.2 | - | 1,118.5 | |
| Maximum (pounds/day) | 1.2 | 8.9 | 7.5 | 2.2 | 0.4 | 2.0 | 0.6 | 0.3 | 0.4 | 2,222.0 | |
| Total (tons/construction project) | 0.0 | 0.3 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 74.6 | |

Notes:
 Project Start Year -> 2021
 Project Length (months) -> 2
 Total Project Area (acres) -> 0
 Maximum Area Disturbed/Day (acres) -> 0
 Total Soil Imported/Exported (yd³/day)-> 0

PM10 and PM2.5 estimates assume 50% control of fugitive dust from watering and associated dust control measures if a minimum number of water trucks are specified.

Total PM10 emissions shown in column F are the sum of exhaust and fugitive dust emissions shown in columns H and I. Total PM2.5 emissions shown in Column J are the sum of exhaust and fugitive dust emissions shown in columns K and L.

| Emission Estimates for -> CPZ Richmond to San Pablo Jack and Bore | | ROG (kgs/day) | | NOx (kgs/day) | | Total PM10 (kgs/day) | Exhaust PM10 (kgs/day) | Fugitive Dust PM10 (kgs/day) | Total PM2.5 (kgs/day) | Exhaust PM2.5 (kgs/day) | Fugitive Dust PM2.5 (kgs/day) |
|---|------------|---------------|--------------|---------------|--------------|----------------------|------------------------|------------------------------|-----------------------|-------------------------|-------------------------------|
| Project Phases (Metric Units) | | CO (kgs/day) | CO (kgs/day) | CO (kgs/day) | CO (kgs/day) | | | | | | |
| Pit Excavation | 0.5 | 4.0 | 3.4 | 0.6 | 0.2 | 0.5 | 0.2 | 0.1 | 0.1 | 931.6 | |
| Casing Installation | 0.3 | 2.0 | 1.8 | 0.5 | 0.1 | 0.5 | 0.2 | 0.1 | 0.1 | 589.6 | |
| Pipeline Installation | 0.4 | 2.8 | 2.0 | 1.0 | 0.1 | 0.9 | 0.3 | 0.1 | 0.2 | 1,010.0 | |
| Backfill | 0.3 | 2.7 | 1.5 | 0.1 | 0.1 | - | 0.1 | 0.1 | - | 508.4 | |
| Maximum (kilograms/day) | 0.5 | 4.0 | 3.4 | 1.0 | 0.2 | 0.9 | 0.3 | 0.1 | 0.2 | 1,010.0 | |
| Total (megagrams/construction project) | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 67.7 | |

Pipeline Installation

| | |
|--------------------------|--|
| Pavement Removal | 1 Concrete Saw 1 Dozer 4 Signal Boards 1 Water Truck 1 Tractor/Loader/Backhoe |
| Excavation | 1 Excavator 1 Forklift 1 Water Truck 1 Tractor/Loader/Backhoe 2 Trenchers 1 Pump |
| Pipe Installation | 4 Signal Boards 2 Forklifts 1 Compactor 3 Welders 1 Water Truck 1 Pump 4 Signal Boards |
| Pave | 1 Paver 1 Paving equipment 1 Roller 4 Signal Boards 1 Pump 1 Sweeper/Scrubber |

Jack and Bore

| | |
|----------------------------|---|
| Pit Excavation | 1 Excavator 1 Dozer 1 Loader 1 Tractor/Loader/Backhoe 1 Water Truck |
| Casing Installation | 1 Crane 1 Forklift 1 Tractor/Loader/Backhoe 3 Welders 1 Water Truck |
| Pipe Installation | 1 Drill Rig 1 Crane 3 Welders 1 Forklift 1 Water Truck |
| Backfill | 2 Backhoes 1 Loader 1 Compactor 1 Water Truck |

Bridge Crossing

| | |
|------------------------------|--|
| Clear Grub | 1 Concrete Saw 1 Dozer 1 Water Truck 1 Tractor/Loader/Backhoe |
| Abutment Construction | 1 Loader 1 Dozer 1 Tractor/Loader/Backhoe 1 Water Truck 1 Compactor |
| Bridge Erection | 1 Generator Set 1 Crane 3 Welders 1 Forklift 1 Air Compressor 1 Water Truck |
| Pipeline Install | 3 Welders 1 Forklift 1 Crane |

APPENDIX G

Plant Species Observed

TABLE G-1
PLANT SPECIES OBSERVED ON WEST OF HILLS PIPELINE SEGMENTS

| Family | Scientific Name | Common Name | Wildcat Pipeline (Berkeley) | Wildcat Pipeline (El Cerrito) | Central Pressure Zone Pipeline (El Cerrito) | Central Pressure Zone (Richmond/San Pablo) |
|----------------|--|-------------------------------|-----------------------------|-------------------------------|---|--|
| Adoxaceae | <i>Sambucus nigra</i> ssp. <i>caerulea</i> (= <i>S. mexicana</i>) | Blue elderberry | | | | x |
| Altingiaceae | <i>Liquidambar</i> sp. | Sweetgum (ornamental) | x | x | | |
| Amaryllidaceae | <i>Agapanthus</i> sp. | Lily of the Nile | x | x | x | |
| Amaryllidaceae | <i>Narcissus</i> sp. | Narcissus (ornamental) | | x | | |
| Apiaceae | <i>Foeniculum vulgare</i> | Fennel | | | x | x |
| Araliaceae | <i>Hedera canariensis</i> | Canary ivy | | | x | x |
| Arecaceae | <i>Phoenix canariensis</i> | Canary island date palm | x | | | x |
| Asteraceae | <i>Artemisia californica</i> | Coastal sage brush | | | | x |
| Asteraceae | <i>Baccharis pilularis</i> ssp. <i>consanguinea</i> | Coyote brush | | | | x |
| Asteraceae | <i>Bellis perennis</i> | English lawn daisy | | | | x |
| Asteraceae | <i>Delairea odorata</i> (= <i>Senecio mikanioides</i>) | Cape ivy | | | | x |
| Asteraceae | <i>Erigeron canadensis</i> (= <i>Conyza c.</i>) | Horseweed | | | x | x |
| Asteraceae | <i>Helminthotheca echioides</i> (= <i>Picris e.</i>) | Bristly ox-tongue | x | x | x | |
| Asteraceae | <i>Pseudognaphalium</i> sp. | Cudweed | | | x | |
| Asteraceae | <i>Sonchus asper</i> ssp. <i>asper</i> | Sow thistle | x | | | |
| Asteraceae | <i>Taraxacum officinale</i> | Red seeded dandelion | | | x | x |
| Berberidaceae | <i>Nandina domestica</i> | Heavenly bamboo | x | | x | |
| Betulaceae | <i>Alnus rhombifolia</i> | White alder | | | | x |
| Betulaceae | <i>Betula</i> sp. | Birch (ornamental) | | x | | |
| Brassicaceae | <i>Brassica oleracea</i> | Broccoli | | | | x |
| Cactaceae | <i>Opuntia</i> sp. | Beavertail, tuna (ornamental) | | | | x |
| Celastraceae | <i>Maytenus boaria</i> | Mayten tree | x | | | |
| Crassulaceae | <i>Crassula ovata</i> | Jade plant (ornamental) | x | x | | |
| Cupressaceae | <i>Juniperus</i> sp. | Juniper (ornamental) | | x | | x |
| Cupressaceae | <i>Sequoia sempervirens</i> | Coast redwood | x | | | |
| Cyperaceae | <i>Carex</i> sp. | Sedge | | | | x |
| Cyperaceae | <i>Cyperus eragrostis</i> | Tall cyperus | | | | x |
| Equisetaceae | <i>Equisetum hyemale</i> ssp. <i>affine</i> | Giant scouring rush | | | | x |
| Ericaceae | <i>Arbutus unedo</i> | Strawberry tree | | | | x |
| Ericaceae | <i>Rhododendron</i> sp. | Azalea (ornamental) | | x | | |
| Fabaceae | <i>Medicago polymorpha</i> | California burclover | | | | x |
| Fagaceae | <i>Quercus agrifolia</i> var. <i>agrifolia</i> | Coast live oak | | | | x |
| Geraniaceae | <i>Geranium dissectum</i> | Wild geranium | | | | x |
| Geraniaceae | <i>Pelargonium</i> sp. | Geranium (ornamental) | | | | x |
| Iridaceae | <i>Iris</i> sp. | Horticultural iris | x | | | |
| Juglandaceae | <i>Juglans regia</i> | English walnut | | | | x |
| Juncaceae | <i>Juncus</i> sp. | Rush | | | | x |
| Lauraceae | <i>Umbellularia californica</i> | California laurel | | | | x |
| Magnoliaceae | <i>Magnolia</i> sp. | Magnolia (ornamental) | x | x | | |
| Malvaceae | <i>Malva parviflora</i> | Cheeseweed | | x | x | |
| Myrtaceae | <i>Eucalyptus globulus</i> | Blue gum | | x | | x |
| Oleaceae | <i>Ligustrum</i> sp. | Privet (ornamental) | x | | | x |
| Oxalidaceae | <i>Oxalis pes-caprae</i> | Bermuda buttercup | x | x | x | x |
| Papaveraceae | <i>Eschscholzia californica</i> | California poppy | | x | | |
| Pinaceae | <i>Pinus radiata</i> | Monterey pine | | | | x |
| Pinaceae | <i>Pinus</i> sp. | Pine (ornamental) | x | | x | |
| Pittosporaceae | <i>Pittosporum</i> sp. | Pittosporum (ornamental) | | | | x |
| Plantaginaceae | <i>Plantago lanceolata</i> | Ribwort | | | | x |
| Plantaginaceae | <i>Plantago major</i> | Common plantain | | | | x |
| Platanaceae | <i>Platanus x acerifolia</i> | London plane tree | | | x | |
| Poaceae | <i>Abrostis</i> sp. | Bentgrass | | | x | |
| Poaceae | <i>Avena barbata</i> | Slim oat | | x | x | x |
| Poaceae | <i>Bromus diandrus</i> | Ripgut brome | | x | | |
| Poaceae | <i>Festuca</i> sp. | Fescue (lawn) | | | | x |

TABLE G-1
PLANT SPECIES OBSERVED ON WEST OF HILLS PIPELINE SEGMENTS

| Family | Scientific Name | Common Name | Wildcat Pipeline (Berkeley) | Wildcat Pipeline (El Cerrito) | Central Pressure Zone Pipeline (El Cerrito) | Central Pressure Zone (Richmond/San Pablo) |
|---------------|--|--------------------------|-----------------------------|-------------------------------|---|--|
| Poaceae | <i>Festuca microstachys</i> (= <i>Vulpia m.</i>) | Few-flowered fescue | | x | | |
| Poaceae | <i>Hordeum murinum</i> ssp. <i>leporinum</i> | Farmer's foxtail | | | x | |
| Poaceae | <i>Pennisetum clandestinum</i> | Kikuyu grass | | | x | |
| Polygonaceae | <i>Muehlenbeckia complexa</i> | Mattress vine | | | x | |
| Polygonaceae | <i>Rumex crispus</i> | Rhubarb | | | x | |
| Primulaceae | <i>Primula</i> sp. | Primrose (ornamental) | x | | | |
| Rhamnaceae | <i>Ceanothus</i> sp. | Ceanothus | x | | | |
| Rosaceae | <i>Cotoneaster</i> sp. | Cotoneaster | | | x | |
| Rosaceae | <i>Photinia</i> sp. | Photinia (ornamental) | | x | | x |
| Rosaceae | <i>Prunus cerasifera</i> | Cherry plum | x | | | x |
| Rosaceae | <i>Pyracantha angustifolia</i> | Firethorn | x | | | |
| Rosaceae | <i>Pyrus</i> sp. | Flowering pear | | | x | x |
| Rosaceae | <i>Rosa</i> sp. | Rose (ornamental) | x | | | |
| Rosaceae | <i>Rubus armeniacus</i> (= <i>Rubus discolor</i>) | Himalayan blackberry | | x | x | |
| Salicaceae | <i>Salix lasiolepis</i> | Arroyo willow | | | x | |
| Sapindaceae | <i>Acer negundo</i> var. <i>californicum</i> | California box elder | | | x | |
| Sapindaceae | <i>Acer palmatum</i> | Japanese maple | x | | | |
| Sapindaceae | <i>Aesculus californica</i> | Buckeye | | | x | |
| Solanaceae | <i>Solanum</i> sp. | Potato vine (ornamental) | | | x | |
| Theaceae | <i>Camellia</i> sp. | Camellia (ornamental) | | x | | |
| Tropaeolaceae | <i>Tropaeolum majus</i> | Garden nasturtium | | | x | |
| Ulmaceae | <i>Ulmus</i> sp. | Elm (ornamental) | | x | | |
| Urticaceae | <i>Urtica dioica</i> ssp. <i>holosericea</i> | Stinging nettle | | | x | |
| Valerianaceae | <i>Centranthus ruber</i> | Jupiter's beard | | | x | x |
| Verbenaceae | <i>Verbena</i> sp. | Verbena (ornamental) | | | x | |

APPENDIX H

List of Special Status Species

TABLE H-1
SPECIAL-STATUS PLANTS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/ CDFG/CNPS ¹ | General Habitat | Potential to Occur |
|---|--|---|---|
| Species Listed or Proposed for Listing | | | |
| Pallid manzanita <i>Arctostaphylos pallida</i> | FT/CE/1B.1 | Broadleafed upland forest, closed-cone coniferous forest, chaparral, cismontane woodland, coastal scrub; on siliceous shale, sandy or gravelly substrates; 600-1600 ft. | Not present. Natural habitat suitable for this species is lacking in project area and species was not observed. Nearest population is on Sobrante Ridge. |
| Robust spineflower <i>Chorizanthe robusta</i> var. <i>robusta</i> | FE/--/1B.1 | Openings in cismontane woodland, coastal dunes, coastal scrub; sandy terraces or bluffs in loose sand; 10-1000 ft. | Not present. Loose sandy substrate not present in project area. Only one historic record in general vicinity; presumed extirpated from the East Bay. |
| Presidio clarkia <i>Clarkia franciscana</i> | FE/CE/1B.1 | Coastal scrub, valley and foothill grassland; serpentine outcrops in grassland or scrub; 80-1000 ft. | Not present. Natural serpentine habitat is lacking in project area. Nearest known locality is along Skyline Boulevard in Oakland. |
| Santa Cruz tarplant <i>Holocarpha macradenia</i> | FT/CE/1B.1 | Grassland, coastal prairie; often with non-natives in light sandy or sandy clay soil; 30 to 850 ft. | Low. Natural coastal prairie and grassland habitat lacking in project area. All naturally occurring San Francisco Bay area populations presumed extirpated. |
| Beach layia <i>Layia carnosa</i> | FE/CE/1B.1 | Coastal dunes, coastal scrub; on semi-stabilized dunes, usually behind foredunes; 0-200 ft. | Not present. Coastal dune and scrub habitat lacking in project area. Nearest known occurrence is an extirpated site in former sand dunes in San Francisco. |
| San Francisco popcorn-flower <i>Plagiobothrys diffusus</i> | --/CE/1B.1 | Coastal prairie, valley and foothill grassland; historically on grasslands with marine influence; 200-1200 ft. | Low. Natural grasslands not present within project area. Nearest known occurrence is on Skyline Boulevard in Oakland. |
| Adobe sanicle <i>Sanicula maritima</i> | --/CR/1B.1 | Chaparral, coastal prairie, meadows, seeps, valley and foothill grassland; moist serpentinite clay soil; 100-800 ft. | Not present. Moist clay serpentinite substrate not present in project area. Nearest known occurrence is an apparently extirpated site in the vicinity of Alameda. |
| California sea-blite <i>Suaeda californica</i> | FE/--/1B.1 | Coastal salt marshes and swamps, coastal dunes; 0-20 ft. | Not present. No suitable habitat within project area. All naturally occurring San Francisco Bay area populations thought to have been extirpated. Reintroduced on San Francisco Peninsula. |
| Other Special-Status Species | | | |
| <i>Plants</i> | | | |
| Bent-flowered fiddleneck <i>Amsinckia lunaris</i> | --/--/1B.2 | Coastal bluff scrub, valley and foothill grassland; 10-1700 ft. | Low. All upland habitat in project area has been disturbed; no suitable habitat remains for this species. Nearest known localities are on San Pablo and Sobrante ridges. |

¹ Key to listing status codes can be found at the end of Table 1.

TABLE H-1 (Continued)
SPECIAL-STATUS PLANTS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/ CDFG/CNPS ² | General Habitat | Potential to Occur |
|---|--|--|---|
| Other Special-Status Species (cont.) | | | |
| Alkalil milk vetch <i>Astragalus tener</i> var. <i>tener</i> | --/~/1B.2 | Adobe clay soils in valley and foothill grassland; 3-300 ft. | Low. Adobe clay soils not present on project site. All upland habitat in survey area has been disturbed in the past. Nearest historic records are flats near bay in present-day Emeryville, Oakland, Richmond. |
| San Joaquin spearscale <i>Atriplex joquiniana</i> | --/~/1B.2 | Chenopod scrub, meadows and seeps, playas, valley and foothill grassland; seasonal wetlands in alkaline soils; 0-825 ft. | Not present. Suitable habitat not present survey area. Nearest locality is Oakland marshes but population is possibly extirpated; last seen in 1929. |
| Big-scale balsamroot <i>Balsamorhiza macrolepis</i> var. <i>macrolepis</i> | --/~/1B.2 | Chaparral, cismontane woodland, valley and foothill grassland; sometimes on serpentinite; 300-4620 ft. | Low. Suitable habitat not observed in survey area. Nearest record is Anthony Chabot Regional Park; all other nearby records are farther to south and east. |
| Round-leaved filaree <i>California macrophylla</i> | --/~/1B.1 | Cismontane woodland, valley and foothill grassland; clay substrate, in low, somewhat moist sites; 50-4000 ft. | Low. Natural habitat for this species has probably been eliminated from nearly all of the Bay Area. Four localities are known from the three-quadrat study area; all are possibly extirpated. |
| Pacific false bindweed <i>Calystegia purpurata</i> ssp. <i>saxicola</i> | --/~/1B.2 | Coastal dunes, coastal scrub, coniferous forest; 50-350 ft. | Low. All upland habitat in survey area has been disturbed in the past, no suitable habitat remains. Nearest records are from Richmond and Red Rock Island. |
| Bristly sedge <i>Carex comosa</i> | --/~/2.1 | Coastal prairie, marshes and swamps, valley and foothill grassland; 0-1400 ft. | Low. Suitable habitat not observed in survey area. Nearest locality is in San Francisco, presumed extirpated. |
| Point Reyes bird's-beak <i>Chloropyron maritimum</i> ssp. <i>palustre</i> | --/~/1B.2 | Coastal salt marshes and swamps; 0-35 ft. | Not present. Salt marsh habitat is not present in survey area. Presumed extirpated from Alameda County. Nearest occurrences are Shell Mound, Bay Farm Island. |
| San Francisco spineflower <i>Chorizanthe cuspidata</i> var. <i>cuspidata</i> | --/~/1B.2 | Coastal scrub, coastal dunes, coastal prairie, coastal bluff scrub; 10-710 ft. | Not present. Suitable coastal habitat not present in survey area. Only known locality from a non-specific locality in Oakland, west of Lake Merritt, which is presumed extirpated. |
| Western leatherwood <i>Dirca occidentalis</i> | --/~/1B.2 | Mesic situations in many habitats, including riparian woodland and forest, chaparral, broadleafed upland forest, and cismontane woodland; 100-1800 ft. | Low. Many nearby records, including Wildcat Regional Park. Riparian woodland understory in the survey area was highly disturbed and dominated by non-native species. |

² Key to listing status codes can be found at the end of Table 1.

TABLE H-1 (Continued)
SPECIAL-STATUS PLANTS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/ CDFG/CNPS ² | General Habitat | Potential to Occur |
|---|--|---|--|
| Other Special-Status Species (cont.) | | | |
| Tiburon buckwheat <i>Eriogonum luteolum</i> var. <i>caninum</i> | --/1B.2 | Chaparral, coastal prairie, valley and foothill grassland; sandy to gravelly sites, usually on serpentinite; 0- 2300 ft. | Not present. Serpentinite substrate not present in survey area. Nearest records are from Skyline Drive in Oakland. |
| Fragrant fritillary <i>Fritillaria liliacea</i> | FSC/--/ 1B.2 | Coastal prairie and scrub, grasslands, often on serpentine soils; 10-1350 ft. | Not present. Serpentine soils not present. Nearest recorded observation is historical and from Point Richmond. |
| Blue coast gilia <i>Gilia capitata</i> ssp. <i>chamissonis</i> | --/1B.1 | Coastal dunes and scrub, sandy soils; 10-700 ft. | Not present. Suitable sandy substrate not present in survey area. Nearest records are from San Francisco sandy habitats. |
| Diablo helianthella <i>Helianthella castanea</i> | --/List 1B.2 | Broadleaved upland forest, chaparral, cismontane woodland, coastal scrub, riparian woodland, valley and foothill grassland; 200-4000 ft. | Low. Only marginally suitable habitat, dominated by non-native species is available within the survey area. Nearest record is San Pablo Ridge. |
| White seaside tarplant <i>Hemizonia congesta</i> ssp. <i>congesta</i> | --/1B.2 | Grassy sites, marshy edges; less than 330 ft. | Low. Native grasslands and marshes are no longer present in survey area. According to CCH (2012), nearest known populations are in Marin County, while CalFlora (2012) reports some occurrences in West Oakland. |
| Loma Prieta hoita <i>Hoita strobilina</i> | --/1B.2 | Mesic areas, usually on serpentinite, riparian or cismontane woodland, chaparral; 100-2000 ft. | Low. No serpentine soils present. Only marginally suitable habitat, dominated by non-native species is available in survey area. Nearest records are in the Oakland Hills. |
| Kellogg's horkelia <i>Horkelia cuneata</i> ssp. <i>sericea</i> | --/1B.1 | Closed-cone coniferous forest, chaparral (maritime), coastal scrub; sandy or gravelly openings; 30-650 ft. | Low. Suitable habitat not observed in survey area. Alameda County records are very old and CNPS considers the species extirpated from the county. |
| Rose leptosiphon <i>Leptosiphon rosaceus</i> | --/1B.1 | Coastal bluff scrub, 0-350 ft. | Not present. Suitable coastal bluff scrub habitat not present in survey area. Nearest, and possibly only known, locality is near Pacifica. |
| Oregon meconella <i>Meconella oregana</i> | FSC/--/1B.1 | Coastal scrub and prairie; typically on north-facing, rocky slopes; 800-1600 ft. | Low. Only marginally suitable habitat, dominated by non-native species is available within in survey area. Known only from five occurrences, including Oakland East, Richmond, and Briones Valley quads. |
| Woodland woollythreads <i>Monolopia gracilens</i> | --/1B.2 | Serpentine grassland, open chaparral, oak woodland; 350- 3800 ft. | Low. No suitable natural habitat was observed in survey area; nearest known localities are in Oakland Hills and foothills of Mount Diablo. |
| Choris' popcorn-flower <i>Plagiobothrys chorisianus</i> | --/1B.2 | Chaparral, coastal prairie, coastal scrub; mesic habitats; 50-350 ft. | Low. No suitable natural habitat was observed in survey area; nearest known localities are San Francisco and San Mateo counties; presumed extirpated from Alameda County. |

TABLE H-1 (Continued)
SPECIAL-STATUS PLANTS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/ CDFG/CNPS ² | General Habitat | Potential to Occur |
|---|--|---|---|
| Other Special-Status Species (cont.) | | | |
| Most beautiful jewel-flower <i>Streptanthus albidus</i> ssp. <i>peramoenus</i> (= <i>S. glandulosus</i> ssp. <i>glandulosus</i>) | FSC/--/1B.2 | Ridges and slopes; chaparral, valley and foothill grassland, and woodland; on serpentine outcrops; 360-3300 ft. | Not present. No serpentine soils or outcrops within the survey area. Nearest known localities are Richmond and the Berkeley Hills. |
| Slender-leaved pondweed <i>Stuckenia filiformis</i> | --/--/2.2 | Marshes and swamps (assorted shallow freshwater); 990-7000 ft. | Not present. Suitable marsh and ponded freshwater habitats not present within survey area; nearest known record is from Sibley Regional Park. |
| Suisun marsh aster <i>Symphyotrichum lenticum</i> (= <i>Aster latus</i>) | --/--/1B.2 | Marshes and swamps (brackish and freshwater); 0-10 ft. | Low. Suitable habitat nearby, but not observed within survey area. Nearest recorded location is at Point Molate. |
| Saline clover <i>Trifolium hydrophilum</i> | --/--/1B.2 | Marshes and swamps, valley and foothill grassland, vernal pools; mesic, alkaline sites; 0-1000 ft | Low. Mesic, alkaline natural habitats not observed in survey area; nearest known localities are from Richmond, the Berkeley shoreline, and West Oakland, but many sites are old records and may be extirpated. |

STATUS CODES:**FEDERAL: (U.S. Fish and Wildlife Service)**

FE = Listed as Endangered (in danger of extinction) by the Federal Government.

FT = Listed as Threatened (likely to become Endangered within the foreseeable future) by the Federal Government.

FP = Proposed for Listing as Endangered or Threatened.

FC = Candidate to become a *proposed* species.

FSC = Former FWS Species of Concern. The USFWS no longer lists Species of Concern but recommends that species considered to be at potential risk by a number of organizations and agencies be addressed during project environmental review.

STATE: (California Department of Fish and Game)

CE = Listed as Endangered by the State of California

CT = Listed as Threatened by the State of California

CR = Listed as Rare by the State of California (plants only)

CSC = California Species of Special Concern

California Native Plant Society

List 1A=Plants presumed extinct in California

List 1B=Plants rare, Threatened, or Endangered in California and elsewhere

List 2= Plants rare, Threatened, or Endangered in California but more common elsewhere

List 3= Plants about which more information is needed

List 4= Plants of limited distribution

An extension reflecting the level of threat to each species is appended to each rarity category as follows:

.1 – Seriously endangered in California

.2 – Fairly endangered in California

.3 – Not very endangered in California

SOURCE: CDFG, 2012a; CNPS, 2012; USFWS, 2012; Consortium of California Herbaria, 2012; CalFlora, 2012

TABLE H-2
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ³ | General Habitat | Potential to Occur |
|--|---|--|--|
| Species Listed or Proposed for Listing | | | |
| Animals | | | |
| Invertebrates | | | |
| Vernal pool fairy shrimp <i>Branchinecta lynchii</i> | FT/ | Small, clear-water sandstone depression pools and grassy swales. | Not present. No suitable habitat present. No CNDB records from 3-quad study area. |
| Bay checkerspot butterfly <i>Euphydryas editha bayensis</i> | FT/ | Serpentine bunchgrass and valley needlegrass grassland. Larval food plants are <i>Plantago erecta</i> , <i>Castilleja densiflora</i> and <i>C. exserta</i> . Adult food plants are <i>Lomatium</i> spp., <i>Lasthenia californica</i> and <i>Layia platyglossa</i> . | Not present. No suitable habitat present. No CNDB records from 3-quad study area. |
| Callippe silverspot butterfly <i>Speyeria callippe callippe</i> | FE/ | Grasslands with larval food plant <i>Viola pedunculata</i> and nearby adult nectar sources. | Not present. No native grassland habitat present. No CNDB records from 3-quad study area. |
| Fish | | | |
| Southern DPS green sturgeon <i>Acipenser medirostris</i> | FT/CSC | Inhabit near-shore marine waters from Mexico to the Bering Sea. Utilize the waters of the Delta for juvenile rearing, adult holding, and migratory movements to and from Upper Sacramento River spawning grounds. | Not Present. May migrate through bay waters downstream of project area and juveniles may be present in bay year-round. Not known from San Pablo or Wildcat Creek watersheds (Leidy, 2007) |
| Tidewater goby <i>Eucyclogobius newberryi</i> | FE/CSC | Shallow waters of bays and estuaries, in lower stream reaches, in coastal stream lagoons | Not present. Estuary and lagoon habitat not present in project area. |
| Delta smelt <i>Hypomesus transpacificus</i> Critical Habitat designated | FT/CT | Shallow, open waters of the estuary where salinities are 2-7 ppt. Spawn and rear in sloughs and edge waters shallow of channels in upper Delta and Sacramento River, Suisun Marsh and Bay. | Not present. Estuary and lagoon habitat not present in project area. |
| Coho salmon – Central California coast ESU <i>Oncorhynchus kisutch</i> Critical Habitat designated | FE/CE | Accessible Bay Area and coastal rivers and streams with cover, cool water and sufficient dissolved oxygen. Require beds of loose, silt-free gravel for spawning. | Low. San Francisco Bay/Sacramento – San Joaquin River system is within the historical range of the species, but coho salmon are currently considered extirpated in project area. |
| Central California coast steelhead <i>Oncorhynchus mykiss</i> Critical Habitat designated | FT/CSC | Spawns and rears in coastal streams between the Russian River and Aptos Creek, as well as drainages of the San Francisco and San Pablo bays. Requires gravelly substrate and shaded riparian habitat. | Moderate. May occasionally stray into Wildcat and San Pablo creeks, but flow, temperature, fine sediments, water quality, and barriers to passage are limiting for spawning and rearing. Resident rainbow trout populations occur in Wildcat Creek and have occurred in San Pablo Creek. Historical steelhead run in San Pablo Creek thought to be extirpated or nearly so (Moyle, 2007). |

³ Key to listing status codes can be found at the end of Table 1.

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|--|---|---|---|
| Species Listed or Proposed for Listing (cont.) | | | |
| Animals (cont.) | | | |
| Fish (cont.) | | | |
| California Central Valley steelhead <i>Oncorhynchus mykiss</i> Critical Habitat designated | FT/CSC | Spawns and rears in the Sacramento/San Joaquin River systems and tributaries where gravelly substrate and shaded riparian habitat occurs. | Low to moderate. Migrates through bay waters downstream of project area. Could occasionally stray into San Pablo or Wildcat creeks but suitable spawning habitat very limited. |
| Sacramento winter-run Chinook salmon <i>Oncorhynchus tshawytscha</i> Critical Habitat designated | FE/CE | Spawns and rears in Sacramento River and tributaries where gravelly substrate and shaded riparian habitat occurs. | Low. Migrates through bay waters downstream of project area. Not known to occur in either the San Pablo or Wildcat Creek. Populations are at all time low numbers, highly unlikely to occur in project area creeks. |
| Central Valley spring-run Chinook salmon <i>Oncorhynchus tshawytscha</i> Critical Habitat designated | FT/CT | Spawns and rears in Sacramento River and tributaries where gravelly substrate and shaded riparian habitat occurs. | Low. Migrates through bay waters downstream of project area. Not known to occur in either the San Pablo or Wildcat Creek. Populations are at all-time low numbers, highly unlikely to occur in project area creeks. |
| Amphibians | | | |
| California tiger salamander <i>Ambystoma californiense</i> | FT/CT | Natural pools and artificial ponds (usually ephemeral) for breeding and upland mammal burrows in annual grassland for adult cover and foraging. | Not present. Pools and ponds not present in survey area; upland habitat and burrows very limited and fragmented; CNDB considers extirpated from three-quadrat study area. |
| California red-legged frog <i>Rana draytonii</i> | FT/CSC | Breed in stock ponds, pools, and slow-moving streams | Low to Moderate. Potentially suitable aquatic habitat present in San Pablo and Wildcat creeks. Nearest documented location is just below San Pablo Reservoir 5 miles distant. Potential for movement downstream into project area. |
| Reptiles | | | |
| Alameda whipsnake <i>Masticophis lateralis euryxanthus</i> | FT/CT | Most often in coastal scrub and chaparral; also can be present in grassland, woodland, and forest natural communities. Rock outcrops important in foraging for lizards. | Low. No natural coastal scrub or grassland habitat present in survey area, and ruderal habitat highly fragmented. |
| Birds | | | |
| Western snowy plover <i>Charadrius alexandrinus nivosus</i> | FT/ | Forage for small invertebrates on dry or wet beach sand; breeds from southern Washington to Baja California on open sandy beaches, sand spits, dunes, and salt pans. | Not present. Suitable sandy habitat not present in survey area. No CNDB records from vicinity of project area. |

⁴ Key to listing status codes can be found at the end of Table 1.

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|---|---|--|--|
| Species Listed or Proposed for Listing (cont.) | | | |
| Animals (cont.) | | | |
| Birds (cont.) | | | |
| California black rail <i>Laterallus jamaicensis</i> <i>coturniculus</i> | --/CT | Salt marshes along large bays, also freshwater marshes | Not present. Documented in both San Pablo and Wildcat marshes downstream, but no suitable habitat present in project area. |
| California brown pelican <i>Pelecanus occidentalis</i> <i>californicus</i> | FT/ | Forages for fish in open coastal waters; colonial nester on rocky sites. | Not present. Suitable habitat not present in survey area. |
| California clapper rail <i>Rallus longirostris</i> <i>obsoletus</i> | FE/CE | Salt-water and brackish marshes with tidal sloughs. | Not present. Documented in Giant, San Pablo and Wildcat marshes downstream, but no suitable habitat within the project area. |
| California least tern <i>Sternula antillarum</i> <i>browni</i> | FE/ | Breeds in colonies on open sand, tidal flats, sparsely vegetated beaches. Feed on small fish and crustaceans. | Not present. No suitable habitat present in project area. Known from San Pablo Bay National Wildlife Refuge. |
| Mammals | | | |
| Salt marsh harvest mouse <i>Reithrodontomys</i> <i>raviventris</i> | FE/CE | Saline emergent wetlands of San Francisco Bay and tributaries. | Not present. No suitable habitat within project area. Documented in San Pablo, Wildcat, Giant, and Breuner marshes downstream. |
| Other Special Status Species | | | |
| Animals | | | |
| Invertebrates | | | |
| Sandy beach tiger beetle <i>Cicindela hirticollis</i> <i>gravida</i> | --/SA | Found in moist sand near the ocean, for example in swales behind dunes or upper beaches beyond normal high tides. | Not present. Sandy beach and dune habitats not present in survey area. Nearest CNDDB is an extirpated site in San Francisco. |
| Monarch butterfly <i>Danaus plexippus</i> | --/* Wintering sites only | Winter roosts located in wind-protected tree groves (eucalyptus, Monterey pine, cypress) with nectar and water sources nearby. | Low. Potential winter roosting habitat very limited in vicinity of San Pablo Creek. Nearest documented wintering roost is at Point Pinole. |
| Bridges' coast range shoulderband snail <i>Helminthoglypta nickliniana</i> <i>bridgesii</i> | --/SA | Found in hillside habitats of Alameda and Contra Costa counties; colonizes under tall grass and weeds. | Low. Hillside habitats with natural vegetation not found in survey area. Nearest CNDDB record is from San Pablo Creek, about 1 mile east of project area. |
| Lee's microblind harvestman <i>Microcina leei</i> | --/SA | Xeric (dry) habitats in the San Francisco Bay region; beneath sandstone rocks in open oak grassland. | Low. Sandstone rock and oak-grassland habitats not found in survey area. |
| A leaf-cutter bee <i>Trachusa gummifera</i> | --/SA | May inhabit brushy hillsides or slopes with tall grasses. | Low. All known records are from San Francisco. |
| Mimic tryonia <i>Tryonia imitator</i> | --/SA | Permanently submerged areas in coastal lagoons, salt marshes, and estuaries; tolerates a wide range of salinities. | Not present. Brackish water habitats not present in survey area. Nearest CNDDB record is from Lake Merritt. |

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|---|---|---|--|
| Other Special Status Species (cont.) | | | |
| Animals (cont.) | | | |
| Fish | | | |
| Sacramento perch <i>Archoplites interruptus</i> | --/CSC | Tidal waters, freshwater lower-elevation pools in slow moving streams, and floodplain lakes, often with emergent vegetation. | Low. Species was introduced to and documented from Jewel Lake and Lake Anza (manmade lakes on upper Wildcat Creek) in Tilden Regional Park from the 1980's. Since thought to be extirpated from Lake Anza and to persist in small numbers in Jewel Lake. Species is thought to be extinct throughout most of its native range. |
| Central Valley fall/late fall-run Chinook salmon <i>Oncorhynchus tshawytscha</i> | FSC/CSC | Spawns and rears in Sacramento River and tributaries where gravelly substrate and shaded riparian habitat occurs. | Low. Migrates through waters of San Pablo Bay to spawning grounds. May occasionally stray into San Pablo and Wildcat creeks within the project area. |
| Longfin smelt <i>Spirinchus thaleichthys</i> | --/CSC | Occur in the middle or bottom of water column in salt or brackish water. Concentrated in Suisun Bay, Montezuma Slough, and the lower reaches of the Sacramento and San Joaquin Rivers, but may be found throughout San Francisco Bay. | Not present. Migrates through waters of San Pablo Bay to spawning grounds. Not expected to occur in San Pablo and Wildcat creeks. |
| Reptiles | | | |
| Western pond turtle <i>Emys marmorata</i> | FSC/CSC | Freshwater ponds and slow streams edged with sandy soils for laying eggs. | Moderate. Aquatic habitat available in San Pablo Creek within the project area. Known from San Pablo Reservoir, about 5 miles upstream. |
| Foothill yellow-legged frog <i>Rana boylii</i> | --/CSC | Partly shaded, shallow streams and riffles with rocky substrate on permanent streams. | Low. Historically known from San Pablo Creek in Orinda, but no recent CNDB records from this or Wildcat Creek watersheds. |
| Birds | | | |
| Cooper's hawk <i>Accipiter cooperii</i> | --/* 3503.5 | Nests in conifers or deciduous stands near riparian areas | Moderate. Suitable nesting habitat present in larger trees along the San Pablo and Wildcat Creek riparian corridors. |
| Sharp-shinned hawk <i>Accipiter striatus</i> | --/CSC 3503.5 | Nests in mountainous woodlands and forests in either coniferous or deciduous trees | Low. Do not generally breed in the region. May winter in the project area. |
| Golden eagle <i>Aquila chrysaetos</i> | --/* 3503.5 | Nests in large trees, snags, and cliffs, winters on lakes and reservoirs. | Not present. Suitable nesting and foraging habitat absent. |
| Great egret <i>Ardea alba</i> | --/* Rookeries only | Nest colonially in groves of trees. Rookery sites located near marshes, tide-flats, irrigated pastures, and margins of rivers and lakes. | Low. May forage along San Pablo and Wildcat creeks. Unlikely to nest in immediate vicinity of project area because of high ambient levels of activity and disturbance. No rookeries are recorded in the immediate vicinity of the project area. |

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|--|---|--|---|
| Other Special Status Species (cont.) | | | |
| Animals (cont.) | | | |
| Birds (cont.) | | | |
| Great blue heron <i>Ardea herodias</i> | --/* Rookeries only | Nest colonially in groves of trees. Rookery sites located near marshes, tide-flats, irrigated pastures, and margins of rivers and lakes. | Low. May forage along San Pablo and Wildcat creeks, but suitable nesting habitat is not available in project area and no rookeries are recorded in the immediate vicinity. |
| <i>Burrowing owl</i> <i>Athene cunicularia</i> | --/CSC | Nests and forages in low-growing grasslands that support burrowing mammals. | Low. Only marginally suitable grassland habitat present. Not documented from the immediate area. |
| Great horned owl <i>Bubo virginianus</i> | --/3503.5 | Often uses abandoned nests of corvids or squirrels; nests in large oaks, conifers, eucalyptus. | High. Suitable nesting habitat present in larger trees along the San Pablo and Wildcat Creek riparian corridors. |
| <i>Red-tailed hawk</i> <i>Buteo jamaicensis</i> | --/3503.5 | Usually nests in large trees, often in woodland or riparian deciduous habitats | High. Suitable nesting habitat present in larger trees along the San Pablo and Wildcat Creek riparian corridors. |
| <i>Red-shouldered hawk</i> <i>Buteo lineatus</i> | --/3503.5 | Usually nests in large trees, often in woodland or riparian deciduous habitats. Forages over open grasslands and woodlands | High. Suitable nesting habitat present in larger trees along the San Pablo and Wildcat Creek riparian corridors. |
| Northern harrier <i>Circus cyaneus</i> | --/CSC | Mostly nests in emergent vegetation, wet meadows or near rivers and lakes, but may nest in grasslands away from water. | Not present. Suitable nesting and foraging habitat not present in project area. Recorded as occurring in Wildcat Marsh. |
| Snowy egret <i>Egretta thula</i> | --/* Rookeries only | Nest colonially in groves of trees. Rookery sites located near marshes, tide-flats, irrigated pastures, and margins of rivers and lakes. | Low. Likely to forage along San Pablo and Wildcat creeks, but suitable nesting habitat is limited and no rookeries are recorded in the immediate vicinity. |
| <i>White-tailed kite</i> <i>Elanus leucurus</i> | FSC/Fully Protected | Nests in trees adjacent to grasslands, forages over grasslands and agricultural lands | Low. Very limited foraging and nesting habitat in project area. Documented nearby as occurring in Wildcat Marsh. |
| American kestrel <i>Falco sparverius</i> | --/3503.5 | Nests in cavities in large trees near open areas. | Moderate. May nest in cavities of mature riparian corridor trees along San Pablo and Wildcat creeks. Limiting foraging habitat in project area. |
| <i>Salt-marsh common yellowthroat</i> <i>Geothlypis trichas sinuosa</i> | FSC/CSC | Emergent wetlands | Not present. Associated with salt and fresh water marshes, habitats not present in project area. |
| <i>Caspian tern</i> <i>Hydroprogne caspia</i> | --/SA | Nests on sandy or gravelly beaches and shell banks in small colonies inland and along the coast. | Not present. Sandy or gravelly beach habitat is not present in survey area. Nearest recorded locality is on Brooks Island. |
| Alameda song sparrow <i>Melospiza melodia pusillula</i> | --/CSC | Endemic to central San Francisco Bay. Found in pickleweed marshes, nests in low shrubs and pickleweed above high tide levels | Not present. Suitable marsh habitat not present in project area. Nearby Wildcat Marsh contains potential habitat. |

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|---|---|--|--|
| Other Special Status Species (cont.) | | | |
| Animals (cont.) | | | |
| Birds (cont.) | | | |
| San Pablo song sparrow <i>Melospiza melodia</i> <i>samuelis</i> | --/CSC | Salt marshes along northern S.F. and San Pablo Bays. | Not present. Salt marsh habitat not present within project area Recorded nearby from Wildcat Marsh. |
| Black-crowned night heron <i>Nycticorax nycticorax</i> | --/* Rookeries only | Various wetland habitats, including salt, brackish, and freshwater marshes, swamps, streams, lakes, and agricultural fields. Nest in large trees, often with other herons or egrets. | Low. May forage along San Pablo and Wildcat Creeks, but relatively high levels of disturbance likely preclude nesting. No rookeries documented nearby. |
| Allen's hummingbird <i>Selasphorus sasin</i> | FSC/* (AWLY) | Inhabits coastal scrub and a variety of woodlands and riparian habitat, as well as gardens in the urban-wildland interface. | Moderate to High. Suitable nesting and foraging habitat is present in landscaped areas and riparian woodlands. Known records are from Pt. Pinole Regional Park and Miller/Knox Regional Shoreline. |
| Yellow-headed blackbird <i>Xanthocephalus xanthocephalus</i> | --/CSC | Nests in freshwater emergent wetlands with dense vegetation and deep water, often along borders of lakes or ponds. | Not present. Suitable freshwater emergent wetlands not present in survey area. Nearest known CNDDDB record is Pinole. |
| Mammals | | | |
| Pallid bat <i>Antrozous pallidus</i> | FSC/CSC | Various habitats including grasslands, scrubs, woodlands, and mixed conifer forests, but is most common in open, dry habitats with rocky areas for roosting. Day roosts include hollow trees, buildings, caves, crevices, and mines. | Low. Potential roosting habitat may be available in trees on or within the vicinity of the project area. However there is a general lack of foraging habitat in the vicinity. Most CNDDDB records from vicinity of project are old. |
| Berkeley kangaroo rat <i>Dipodomys heermanni</i> <i>berkeleyensis</i> | --/SA | Open grassy hilltops and open spaces in chaparral and blue oak-gray pine woodlands; requires fine, deep, well-drained soil for burrowing. | Low. Natural vegetation such as grassy hilltops, open spaces and oak-pine woodland are not present in survey area. |
| Silver-haired bat <i>Lasionycteris noctivagans</i> | --/* | Commonly associated with old growth forests. Maternity colonies found in tree cavities or small hollows. Hibernation roosts include small tree hollows, beneath exfoliating bark, in wood piles, cliff faces, and cave entrances. Feed predominantly in disturbed areas, often in small clearings and along roadways or water courses. | Low. May occur on a transient basis within the project area during spring and fall migration. |

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name Scientific Name | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|---|---|--|--|
| Other Special Status Species (cont.) | | | |
| Animals (cont.) | | | |
| Mammals (cont.) | | | |
| Hoary bat <i>Lasiurus cinereus</i> | --/* | A relatively common, solitary species that occurs throughout California, wintering along the coast and in southern California, and breeds in areas inland and north of the winter range. Prefers open habitats or habitat mosaics, with trees for cover and open areas or habitat edges for feeding. Roosts in dense foliage of medium to large trees. | Low. Potential roosting habitat is available in large riparian trees in the project area. Not expected to breed in the area but may migrate through and may potentially winter there as well. |
| San Pablo vole <i>Microtus californicus sanpabloensis</i> | --/CSC | Salt marshes and adjacent riparian habitat of San Pablo Creek, San Pablo Bay. | Low. Recorded in 1986 from riparian corridors of both San Pablo and Wildcat Creeks west of project area. |
| Long-eared myotis <i>Myotis evotis</i> | FSC-- | Inhabits woodlands and forests up to approximately 8,200 feet in elevation; roosts in crevices and snags. | Moderate. Suitable foraging habitat is limited in the project area. Roosting habitat available in riparian woodlands along San Pablo and Wildcat creeks. |
| Fringed myotis <i>Myotis thysanodes</i> | FSC-- | Inhabits a variety of woodland habitats, roosts in crevices or caves, and forages over water and open habitats. | Moderate. Suitable foraging habitat is limited in the project area. Roosting habitat available in riparian woodlands along San Pablo and Wildcat creeks. |
| Yuma myotis <i>Myotis yumanensis</i> | FSC/CSC | Open forests and woodlands below 8,000 feet in close association with water bodies | Moderate. Vacant or underutilized structures may provide roosting habitat. Suitable foraging habitat is limited and is mainly along San Pablo and Wildcat creeks. |
| Big free-tailed bat <i>Nyctinomops macrotis</i> | --/CSC | Known from isolated populations throughout southwestern U.S., into Mexico. Lives in rocky areas of desert scrub or coniferous forests. Roosts by day in crevices on cliff faces. Feeds on insects. Forms colonies and bear one young each year, in the early summer. | Low. Rare and not known to breed in California. One known record (a suspected vagrant) documented locally (from Alameda County). May migrate through area and be present occasionally on a transient basis. |
| Alameda Island vole <i>Scapanus latimanus parvus</i> | --/CSC | Moist, friable but not flooded soils in a variety of habitats, mostly annual and perennial grasslands. | Not present. All known CNDB records are from Alameda Island. |
| Salt marsh wandering shrew <i>Sorex vagrans halicoetes</i> | FSC/CSC | Salt marsh habitat 6-8 feet above sea level, with abundant pickleweed and driftwood. | Not present. Suitable salt marsh habitat not present in project area. Recorded from San Pablo Creek Marsh and Giant Marsh. |

TABLE H-2 (Continued)
SPECIAL STATUS ANIMALS CONSIDERED IN THE EVALUATION OF THE PROJECT

| Common Name <i>Scientific Name</i> | Listing Status USFWS/CDFG ⁴ | General Habitat | Potential to Occur |
|---|---|--|--|
| Other Special Status Species (cont.) | | | |
| Animals (cont.) | | | |
| Mammals (cont.) | | | |
| American badger <i>Taxidea taxus</i> | --/CSC | Known from many shrub, forest and herbaceous habitats, usually in drier, more open examples; requires friable soils for digging; preferred prey is rodents | Low. This species requires fairly large home ranges and a reliable prey base and therefore is unlikely to be found in project area. Nearest CNDDB records are Orinda and Mills College. |

STATUS CODES:

FEDERAL: (U.S. Fish and Wildlife Service)

FE = Listed as Endangered (in danger of extinction) by the Federal Government.

FT = Listed as Threatened (likely to become Endangered within the foreseeable future) by the Federal Government.

FP = Proposed for Listing as Endangered or Threatened.

FC = Candidate to become a *proposed* species.

FSC = Former FWS Species of Concern. The USFWS no longer lists Species of Concern but recommends that species considered to be at potential risk by a number of organizations and agencies be addressed during project environmental review. Also may be NMFS Species of Concern, which are still listed.

MMPA = Marine Mammal Protection Act

STATE: (California Department of Fish and Game)

CE = Listed as Endangered by the State of California

CT = Listed as Threatened by the State of California

CR = Listed as Rare by the State of California (plants only)

CSC = California Species of Special Concern

3503.5=Protection for nesting species of Falconiformes (hawks) and Strigiformes (owls)

*Special animal—listed on CDFG's Special Animals List

SOURCE: CDFG, 2012a; USFWS, 2012

APPENDIX I

Supplemental Noise Information

Noise Descriptors

Sound is a phenomenon that occurs in a medium (such as air or water), and the manner in which sound travels through this medium is influenced by the physical properties of the medium (such as temperature, density, and humidity). The amount of energy in the sound is proportional to the pressure it generates in the medium. The sound pressure level has become the most common descriptor used to characterize the loudness of an ambient sound, and the decibel (**dB**) scale is used to quantify sound intensity. Sound can vary in intensity by more than 1 million times within the range of human hearing; therefore, a logarithmic scale is used to keep sound pressure measurements within a convenient and manageable range. Because the human ear is not equally sensitive to all sound frequencies within the entire spectrum, human response is factored into sound descriptions in a process called “A-weighting,” which is expressed as **dBA**. The A-weighted decibel, dBA, refers to a scale of noise measurement that approximates the range of sensitivity of the human ear to sounds of different frequencies. On this scale, the normal range of human hearing extends from about 0 dBA to about 140 dBA. A 10-dBA increase in the level of a continuous noise represents a perceived doubling of loudness. The noise levels presented in this report are expressed in terms of dBA unless otherwise indicated. **Table I-1** shows some representative noise sources and their corresponding noise levels in dBA.

Planning for acceptable noise exposure must take into account the types of activities and corresponding noise sensitivity in a specified location for a generalized land-use type. Some general guidelines are as follows: noise levels above 35 dBA can disturb sleep; noise levels of 60 dBA begin to interfere with human speech; prolonged exposure to noise levels greater than 85 dBA can damage hearing (USEPA, 1974).

Variations in noise exposure over time are typically expressed in terms of a steady-state energy level (called **Leq**) that represents the acoustical energy of a given measurement. Leq (24) is the steady-state energy level measured over a 24-hour period. Because community receptors are more sensitive to unwanted noise intrusion during the evening and at night, state law requires that, for planning purposes, an artificial dBA increment be added to “quiet time” noise levels to form a 24-hour noise descriptor called the community noise equivalent level (**CNEL**). CNEL adds a 5-dBA “penalty” during the evening hours (7 p.m. to 10 p.m.) and a 10-dBA penalty during nighttime hours (10 p.m. to 7 a.m.). Another 24-hour noise descriptor, called the day-night noise level (**Ldn**), is similar to CNEL. Both CNEL and Ldn add a 10-dBA penalty to all nighttime noise events between 10 p.m. and 7 a.m., but Ldn does not add the 5-dBA evening penalty. In

TABLE I-1
TYPICAL SOUND LEVELS MEASURED IN THE ENVIRONMENT

| Examples of Common, Easily Recognized Sounds | A-Weighted Decibels (dBA) | Subjective Evaluations |
|--|---------------------------|------------------------|
| Near Jet Engine | 140 | Deafening |
| Threshold of Pain | 130 | |
| Threshold of Feeling – Hard Rock Band | 120 | |
| Accelerating Motorcycle (at a few feet away) | 110 | |
| Loud Horn (at 10 feet away) | 100 | Very Loud |
| Noisy Urban Street | 90 | |
| Noisy Factory | 85 ^a | |
| School Cafeteria with Untreated Surfaces | 80 | Loud |
| Lawnmower | 70 ^b | |
| Near Freeway Auto Traffic | 60 ^b | Moderate |
| Average Office | 50 ^b | |
| Soft Radio Music in Apartment | 40 | Faint |
| Average Residence without Stereo Playing | 30 | |
| Average Whisper | 20 | Very Faint |
| Rustle of Leaves in Wind | 10 | |
| Human Breathing | 5 | |
| Threshold of Audibility | 0 | |

^a Continuous exposure above 85 dBA is likely to degrade the hearing of most people.

^b The range of speech is 50 to 70 dBA.

SOURCE: U.S. Department of Housing and Urban Development, 1985.

practice, Ldn and CNEL usually differ by less than 1 dBA at any given location for transportation noise sources. **Lmax** is the maximum, instantaneous noise level registered during a measurement period.

Vibration Descriptors

Vibrations caused by construction activities can be interpreted as energy transmitted in waves through the ground. These energy waves generally dissipate with distance from the vibration source (e.g., pile driving or sheet pile driving). Energy is lost during the transfer of energy from one particle to another, and vibration becomes less perceptible as distance from the source increases. Vibration attenuates as a function of the distance between the source and receptor. Vibration emanating from a single location (a “point source”) attenuates at a rate of approximately 50 percent for each doubling of distance from the source (termed the “inverse square law”). This calculation tends to underestimate attenuation, and thus provides a worst-case estimate of vibration at the receptor.

Vibration is an oscillatory motion that can be described in terms of displacement, velocity, or acceleration. Peak particle velocity (PPV) is defined as the maximum instantaneous positive or

negative peak of the vibration signal. PPV is used to assess the potential for damage to buildings and structures and is expressed in inches per second (in/sec).

The responses of human receptors and structures to vibration are influenced by a combination of factors, including soil/rock type, distance from the source, duration, and the number of perceived vibration events. Energy transmitted through the ground as vibration can reach levels that cause structural damage; however, humans are very sensitive to vibration, and the vibration amplitudes that can be perceived by humans are well below the levels that cause architectural or structural damage.

Some reference values for vibration are as follows: (1) a freight train passing at a distance of 100 feet can result in vibrations of 0.1 in/sec PPV, and (2) a strong earthquake can produce vibrations in the range of 10 in/sec PPV.

Regulatory Setting

Federal and State Regulations

No federal or state standards related to noise are applicable to the proposed project. The Federal Noise Control Act of 1972 divides powers between federal, state, and local governments, in which the primary federal responsibility is for noise source emission control. State and local governments are responsible for controlling the use of noise sources and determining the levels of noise to be permitted in their environment (USEPA, 1974).

Local Regulations and Policies

At the local level, noise is addressed through the implementation of general plan policies, including noise and land use compatibility guidelines, and through enforcement of noise ordinances. General plan policies provide guidelines for determining whether a noise environment is appropriate for a proposed or planned land use. Local noise ordinances regulate such sources as mechanical equipment and amplified sounds, as well as prescribe hours of heavy equipment operation. Pursuant to California Government Code Section 53091, the East Bay Municipal Utility District (EBMUD)—as a local agency and utility district serving a broad regional area—is not subject to building and land use zoning ordinances (such as noise ordinances) for projects involving facilities that would produce, generate, store, or transmit water. However, it is the practice of EBMUD to work with local jurisdictions and neighboring communities during project planning, and to conform to local environmental protection policies to the extent feasible.

City of Berkeley

The Berkeley Noise Ordinance (Chapter 13.40, Section 13.40.070[B][7], Construction/Demolition) specifies construction and demolition noise limits for various land uses and types of construction activities. **Table I-2** lists the noise limits for residential uses.

TABLE I-2
CITY OF BERKELEY CONSTRUCTION NOISE LIMITS

| Equipment Type | Zone | Time Period | Allowable Exterior Noise Level (dBA) |
|--|----------------------|--|--------------------------------------|
| Mobile (non-scheduled, intermittent, operating <10 days) | R-1, R-2 Residential | Daily, 7:00 a.m. to 7:00 p.m. Weekends, 9:00 a.m. to 8:00 p.m. and Legal Holidays | 75 60 |
| Stationary (repetitively scheduled, long-term, operating >10 days) | R-1, R-2 Residential | Daily, 7:00 a.m. to 7:00 p.m. Weekends, 9:00 a.m. to 8:00 p.m. and Legal Holidays | 60 50 |

SOURCE: Berkeley Municipal Code (Chapter 13.40, Community Noise, Section 13.40.070[B][7], Construction/ Demolition).

Exterior noise limits for the R-1 and R-2 residential zones specified in Section 13.40.050 convert to the Leq and CNEL noise limits listed in **Table I-3**.

TABLE I-3
CITY OF BERKELEY EXTERIOR NOISE STANDARDS AND CONVERTED Leq AND CNEL EQUIVALENTS

| Ordinance Noise Limits | | | |
|-----------------------------|-------------------------------|----------------------------|-------------------------------|
| Maximum Time (minutes/hour) | Model Duration (minutes/hour) | Daytime (7 a.m. to 7 p.m.) | Nighttime (10 p.m. to 7 a.m.) |
| 30 | 30 | 55 | 45 |
| 5 | 25 | 65 | 55 |
| 1 | 4 | 70 | 60 |
| 0 | 1 | 75 | 65 |

| Converted Leq and CNEL Noise Limit Equivalents ^a | | | |
|---|------------|------|------|
| Leq | 60 minutes | 64.3 | 54.3 |

^a Since construction noise levels vary with location and use of equipment during any given modeling period, construction noise levels are not comparable to these simpler ordinance noise energy calculations. Therefore, the above-listed noise limits for each modeled daytime and nighttime hour and their specified durations were converted to Leq levels assuming that the maximum permitted noise levels occur during the modeled hour (WIA, 2000).

SOURCE: Berkeley Municipal Code (Chapter 13.40.050, Exterior Noise Standards).

City of El Cerrito

The El Cerrito Municipal Code does not specifically address construction time or noise limits. However, the Municipal Code does include outdoor noise standards for residential development, which are listed in **Table I-4**. The Municipal Code states:

TABLE I-4
CITY OF EL CERRITO OUTDOOR NOISE LIMITS

| Land Use Type | Exterior Noise Exposure (Ldn or CNEL) | | |
|--|---------------------------------------|--------------------------|--------------|
| | Normally Acceptable | Conditionally Acceptable | Unacceptable |
| Residential, Hotel and Motels, Schools, Libraries, Hospitals | 60 | 75 | >75 |
| Office Buildings, Business, Commercial and Professional | 60 | 80 | >80 |

SOURCE: El Cerrito Municipal Code (Title 19, Zoning, Chapter 19.21, General Site Standards, Section 19.21.050[B][2], Performance Standards).

The goal for maximum outdoor noise levels in residential areas is an Ldn of 60 dB. This level is a requirement to guide the design and location of future development and is a goal for the reduction of noise in existing development. This goal will be applied where outdoor use is a major consideration (e.g., backyards in single-family housing developments and open space areas in multi-family housing projects). The outdoor standard will not normally be applied to the small decks associated with apartments and condominiums but these will be evaluated on a case-by-case basis. Where the Zoning Administrator determines that providing an Ldn of 60 dB or lower outdoors is not feasible, the outdoor goal may be increased to an Ldn of 65 dB at the discretion of the Planning Commission. (Section 19.21.050.B.2.a, Outdoor Noise Levels for Residential Areas)

The noise environment in existing residential areas shall be protected. The City of El Cerrito shall require the evaluation of mitigation measures for projects under the following circumstances:

- a. The project would cause the Ldn to increase 3 dBA or more.
- b. Any increase would result in an Ldn greater than 60 dBA.
- c. The Ldn already exceeds 60 dBA.
- d. The project has the potential to generate significant adverse community response.

(Section 19.21.050.B.4, Evaluation of Noise Impacts in Existing Residential Areas)

Municipal Code Section 19.21.050.E (Performance Standards, Vibration) states that no use, activity, or process will produce vibrations that are perceptible without instruments by a reasonable person at or beyond the property line of the site on which they are situated.

Municipal Code Section 10.30.010 prohibits any person from making any unnecessary noises or sounds that are physically annoying to persons of ordinary sensitiveness, or so harsh or so prolonged or unnatural or unusual in their use, time, or place as to cause physical discomfort to the inhabitants of the neighborhood.

For construction work within the public right-of-way, the City of El Cerrito requires an encroachment permit. The City's standard encroachment permit conditions indicate that time

limits within the public right-of-way shall be 8:00 to 5:00 p.m., Monday – Friday (excluding holidays) or as directed by the City Engineer (City of El Cerrito, 2009).

City of Richmond

The City of Richmond Municipal Code contains two chapters governing noise: Chapter 9.52, Community Noise Ordinance, and Chapter 15.04, Zoning. The City of Richmond Community Noise Ordinance (No. 43-95 or Chapter 9.52 of the Richmond Municipal Code) includes provisions to limit noise impacts generated by construction activity in residential areas. The Noise Ordinance limits the hours that construction activities can occur to 7:00 a.m. to 7:00 p.m. on weekdays and 9:00 a.m. to 8:00 p.m. on weekends and legal holidays. For short-term (temporary), non-scheduled, intermittent operation of mobile construction equipment, the Noise Ordinance limits maximum noise levels to 75 dBA on weekdays (7:00 a.m. to 7:00 p.m.) and 60 dBA on weekends and legal holidays (9:00 a.m. to 8:00 p.m.). For scheduled, long-term operation of stationary equipment (15 days or more), the Noise Ordinance limits maximum noise levels to 60 dBA on weekdays (7:00 a.m. to 7:00 p.m.) and 55 dBA on weekends and legal holidays (9:00 a.m. to 8:00 p.m.). These limits apply to construction activities, wherever technically and economically feasible. This ordinance also specifies exterior noise limits of 60 dBA (a level not to be exceeded more than 30 minutes in any hour) in single-family residential zoning districts (measured at the property boundary).

Section 15.04.840.020, Noise Standards, of Chapter 15.04, Zoning, stipulates that the noise level between 10 p.m. and 7:00 a.m. at the property line of a single-family residence must not exceed 50 dBA for more than 30 minutes in any hour. During those nighttime hours, the standards permit a noise level (at the property line of a single-family residence) of 55 dBA for no more than a cumulative period of 5 minutes in any hour, and 60 dBA for no more than a cumulative period of 1 minute in any hour. The standards result in a converted Leq noise limit equivalent of 54 dBA for nighttime construction activities, as indicated in **Table I-5**.

TABLE I-5
CITY OF RICHMOND NIGHTTIME EXTERIOR NOISE STANDARDS FOR SINGLE-FAMILY RESIDENTIAL ZONING DISTRICT AND CONVERTED Leq EQUIVALENT

| Ordinance Noise Limits | | |
|-----------------------------|------------------------|-------------------------------|
| Maximum Time (minutes/hour) | Model Duration | Nighttime (10 p.m. to 7 a.m.) |
| 30 | 30 minutes at 49.9 dBA | 50 dBA |
| 5 | 25 minutes at 54.9 dBA | 55 dBA |
| 1 | 5 minutes at 59.9 dBA | 60 dBA |

| Converted Leq ^a | | |
|----------------------------|------------|--------|
| Leq | 60 minutes | 54 dBA |

^a Since construction noise levels vary with location and use of equipment during any given modeling period, construction noise levels are not comparable to these simpler ordinance noise energy calculations. Therefore, the above-listed noise limits were converted to Leq levels assuming that the maximum permitted noise levels occur during the modeled hour (WIA, 2000).

SOURCE: Richmond Municipal Code (Section 15.04.840.020, Noise Standards).

City of San Pablo

Section 9.12.010 of the San Pablo Municipal Code prohibits the operation of the following equipment between the hours of 10:00 p.m. and 7:00 a.m.: pile driver, steam shovel, pneumatic hammer, derrick, steam or electric hoist, power-driven saw, or any other tool or apparatus the use of which is attended by loud or unusual noise, except by written permission of the building inspector, and then only in case of emergency. In addition, the San Pablo General Plan Noise Element, Action PS 4.G prohibits construction hours near sensitive land uses between 9:00 p.m. and 7:00 a.m. on weekdays and 5:00 p.m. to 9:00 a.m. on weekends and holidays.

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TABLE I-6
ESTIMATED DAYTIME CONSTRUCTION NOISE LEVELS

| Receptor Location | Activity | Principal Noise Sources | Reference Noise Level, L _{max} in dBA at 50 feet ^a | Minimum Distance Between Project and Closest Sensitive Receptor ^b | Noise Level Adjustment Factor for Distance | Assumed Usage Factor ^c | Noise Level Adjusted for Distance and Usage | Impact 3.11-1 | | Impact 3.11-2 | | Noise Reduction From Mitigation Measure NOI-1 and NOI-2b ^e | Mitigated L _{eq} With Mitigation Measure NOI-1 and NOI-2b ^e | | | | | | | |
|---|------------------|-------------------------|--|--|--|-----------------------------------|---|---|--|---|--|---|---|--|--|--|--|--|--|--|
| | | | | | | | | L _{eq} Exceeds 75-dBA Speech Interference Threshold? | Impact 3.11-1 Daytime Significance Determination | L _{eq} Exceeds 70-dBA Speech Interference Threshold? | Impact 3.11-2 Daytime Significance Determination | | | | | | | | | |
| Open Trench Pipeline Construction | | | | | | | | | | | | | | | | | | | | |
| <i>Wildcat Pipeline (Berkeley)</i> | | | | | | | | | | | | | | | | | | | | |
| Closet residential receptors on Parkside, The Uplands, Hillegass or Benvenue, Stuart, Telegraph, Ward, Dana | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 30 30 | 4 4 | 10% 10% | -10 -10 | 84 83 | Yes Yes | SU SU | Yes Yes | 1 Day 1 Day | LS LS | | | | | | | |
| <i>Wildcat Pipeline (El Cerrito)</i> | | | | | | | | | | | | | | | | | | | | |
| Closet residential receptors on Lynn, C Street, Behrens, Fairmount, Norvell Lincoln, Richmond, Hill | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 25 25 | 6 6 | 10% 10% | -10 -10 | 86 85 | - | - | Yes Yes | 1 Day 1 Day | LS LS | | | | | | | |
| <i>Central Pressure Zone Pipeline (El Cerrito/Richmond)</i> | | | | | | | | | | | | | | | | | | | | |
| Closet residential receptors on San Pablo Avenue (Highway 123) | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 30 30 | 4 4 | 10% 10% | -10 -10 | 84 83 | - | - | Yes Yes | 1 Day 1 Day | LS LS | | | | | | | |
| <i>Central Pressure Zone Pipeline (Richmond/San Pablo)</i> | | | | | | | | | | | | | | | | | | | | |
| Closet school receptor (Richmond High School) on 23rd Street | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 55 55 | -1 -1 | 10% 10% | -10 -10 | 79 78 | Yes Yes | SU SM | Yes Yes | 1 Day 1 Day | LS LS | | | | | | | |
| <i>Richmond Ordinance Noise Limit for Short-term Construction Activities:</i> | | | | | | | | | | | | | | | | | | | | |
| Closet school receptor (Richmond High School) on 23rd Street | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 55 55 | -1 -1 | 10% 10% | -10 -10 | 79 78 | Yes Yes | SU SM | Yes Yes | 1 Day 1 Day | LS LS | | | | | | | |
| <i>Total Construction Days at One Receptor:</i> | | | | | | | | | | | | | | | | | | | | |
| <i>6 Days</i> | | | | | | | | | | | | | | | | | | | | |

TABLE I-6 (Continued)
ESTIMATED DAYTIME CONSTRUCTION NOISE LEVELS

| Pipeline and Closest Noise-Sensitive Receptor Location | Construction Activity | Principal Noise Sources | Minimum Noise Level, Sensitive Receptor ^b | | | | | | Impact 1 | | | | | | Impact 2 | | | | | | Noise Reduction From Mitigation Measure NOI-1 ^e | Mitigated L_{eq} With Controls |
|---|---|--|--|----------------------------|----------------------------|---------------------------------|-----------------------------------|--|--|---|--|--------------------------------|--|----------------------------|---|---|--------------------------|---------------|--|---|--|---|
| | | | L_{max} in dBA at 50 feet ^a | Receptor ^b | Distance | Noise Level | Adjustment Factor for Usage | Assumed Usage Factor ^c for Usage | Noise Level Adjusted for Distance | Leq Noise Level Adjusted for Usage | Leq Noise Level Ordinance Daytime | Impact 1 Significance | Leq Exceeds 75-dBA Ordinance Daytime | Duration of Impact 2 | Leq Exceeds 70-dBA Speech Interference Threshold? | Construction ^d (Workdays) | Impact 2 Significance | Determination | | | | |
| Open Trench Pipeline Construction | | | | | | | | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (Richmond/San Pablo) | | | Richmond Ordinance Noise Limit for Short-term Construction Activities: | | | | | | 75 dBA | Impact 1 | | | | | | Leq Exceeds 70-dBA Ordinance Daytime | Impact 2 | | Noise Reduction From Mitigation Measure NOI-1 ^e | Mitigated L_{eq} With Controls | | |
| Closet residential receptor at 404 23rd Street | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 20 20 | 8 8 | 10% 10% | -10 -10 | 88 87 | Yes Yes | SU SU | Yes Yes | 1 Day 1 Day | LS LS | 0 0 | 88 82 | 5 | | | | | | |
| Excavation and Pipe Installation | Excavator | Various Trucks (dump, flatbed, water) | 81 76 | 20 20 | 8 8 | 40% 40% | 4 4 | 85 80 | Yes Yes | SU SU | Yes Yes | 3 Days 3 Days | LS LS | 0 0 | 85 80 | | | | | | | |
| Repaving | Paving Equipment (roller) Compactor | Backhoe, Loader, Forklift Mobile Batch Plant ^f | 79 76 | 20 20 | 8 8 | 40% 15% | 4 8 | 83 76 | Yes Yes | SU SU | Yes Yes | 3 Days 2 Days | LS LS | 0 0 | 83 76 | | | | | | | |
| Highest Combined Leq at Closest Receptor: | | | | | | 93 | | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (Richmond/San Pablo) | | | | | | | | | | | | | | | | | | | | | | |
| Closet residential receptors on: 23rd Street, Brookside, EB/MUD ROW across San Pablo Creek to Road 20 | Pavement Cutting | Pavement Saw Jackhammer | 90 89 | 10 10 | 14 14 | 10% 10% | -10 | 94 93 | - | - | - | Yes Yes | 1 Day 1 Day | LS LS | 0 0 | 94 88 | | | | | | |
| Excavation and Pipe Installation | Excavator | Various Trucks (dump, flatbed, water) | 81 76 | 10 10 | 14 14 | 40% 40% | 4 4 | 91 86 | - | - | - | Yes Yes | 3 Days 3 Days | LS LS | 0 0 | 91 86 | | | | | | |
| Repaving | Mobile Batch Plant ^f | Mobile Batch Plant ^f | 76 | 10 | 14 | 15% | 8 | 82 | - | - | - | Yes Yes | 2 Days 2 Days | LS LS | 0 0 | 82 82 | | | | | | |
| Highest Combined Leq at Closest Receptor: | | | | | | 99 | | | | | | | | | | | | | | | | |
| Jack-and-Bore Construction | | | | | | | | | | | | | | | | | | | | | | |
| Wildcat Creek Crossing (San Pablo) | Pit Excavation | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator | 101 75 81 | 70 70 70 | -3 -3 -3 | 20% 20% 40% | -7 -7 4 | 91 65 74 | - | - | - | Yes No Yes | 10 Days 10 Days 10 Days | SM LS SM | 0 0 0 | 91 65 74 | | | | | | |
| Various Trucks (dump, flatbed, water) | Backhoe, Loader, Forklift | Backhoe, Loader, Forklift | 76 79 | 70 70 | -3 -3 | 40% 40% | 4 | 69 72 | - | - | - | Yes Yes Yes | 10 Days 10 Days 10 Days | LS SM SM | 0 0 0 | 69 72 72 | | | | | | |
| Repaving | Boring Machine or Auger ^h | Boring Machine or Auger ^h | 84 83 | 70 70 | -3 -3 | 40% 40% | 4 4 | 77 76 | - | - | - | Yes Yes | 20 Days 20 Days | SM SM | -5 -3 | 72 73 | | | | | | |
| Highest Combined Leq at Closest Receptor: | | | | | | 92 | | | | | | | | | | | | | | | | |
| Pipe Bridge Construction | | | | | | | | | | | | | | | | | | | | | | |
| San Pablo Creek Crossing (San Pablo) | San Pablo Ordinance Noise Limit for Short-term Construction Activities: | | | | | | None | | | | | | | | | | | | | | | |
| Closet residential receptors at 2215 Road 20 to the west and 41 Campo Verde Circle to the east | Excavation and Backhoe, Loader, Forklift | Excavator Various Trucks (dump, flatbed, water) Drill Rig Crane | 81 76 84 81 79 | 70 70 70 70 70 | -3 -3 -3 -3 -3 | 40% 40% 20% 20% 40% | 4 4 -7 -7 4 | 74 69 74 71 72 | - | - | - | Yes No Yes Yes Yes | 5 Days 5 Days 5 Days 5 Days 5 Days | LS LS LS LS LS | 0 0 0 0 0 | 74 69 74 71 72 | | | | | | |
| Repaving | Paving Equipment (roller) | Compactor | 80 83 | 70 70 | -3 -3 | 10% 10% | -10 -10 | 67 70 | - | - | - | No Yes | 5 Days 5 Days | LS LS | 0 0 | 67 70 | | | | | | |
| Highest Combined Leq at Closest Receptor: | | | | | | 92 | | | | | | | | | | | | | | | | |
| Pipe Installation | | | | | | | | | | | | | | | | | | | | | | |
| San Pablo Ordinance Noise Limit for Short-term Construction Activities: | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | |

TABLE I-6 (Continued)
ESTIMATED DAYTIME CONSTRUCTION NOISE LEVELS

| Pipeline and Closest Noise-Sensitive Receptor Location | Construction Activity | Principal Noise Sources | Impact 3.11-1 | | | | Impact 3.11-2 | | | | Noise Reduction From Mitigation Measure NOI-1 and NOI-2b ^e | Mitigated L_{eq} Measure NOI-1 and NOI-2b ^e | | | |
|---|--|--|--|---|--|---|--|---|---|---|---|---|----------------------------|----------------------------|--|
| | | | Reference Noise Level, L _{max} in dBA at 50 feet ^a | Minimum Distance Between Project and Closest Sensitive Receptor ^b | Noise Level Adjustment Factor for Distance | Assumed Usage Factor ^c | Noise Level Adjusted Factor for Usage and Usage | Leq Noise Level Adjusted for Distance and Usage | Leq Exceeds 75-dBA Speech Interference Threshold? | Impact 3.11-1 Daytime Significance Determination | Impact 3.11-2 Daytime Significance Determination | | | | |
| Tie-in Construction | | | | | | | | | | | | | | | |
| <i>Wildcat Pipeline (Berkeley) Tie-ins</i> | | | | | | | | | | | | | | | |
| Closest residential receptors on: Dana/ Parker (north tie-in) and Parker/Nogales (south tie-in) | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | 30 30 30 30 30 | 4 4 4 4 4 | 20% 20% 40% 40% 40% | -7 -7 -4 -4 -4 | 98 72 81 76 79 | Yes No Yes Yes Yes | SM LS LS LS LS | Yes <10 Days <10 Days <10 Days <10 Days | LS 0 0 0 0 | 98 72 81 76 79 | | |
| <i>Pipe Connection</i> | | | | | | | | | | | | | | | |
| Wildcat Pipeline (Berkeley) Tie-ins | Hydraulic Compressor Hot Tapping Machine Hot Tapping Machine Motor/Generator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 81 76 79 | 20 20 20 20 20 | 8 8 8 8 8 | 100% 100% 100% 40% 40% | 0 0 0 -4 -4 | 88 86 89 92 95 | Yes Yes Yes Yes Yes | SU SU SU SU SU | Yes 1 Day 1 Day 1 Day 1 Day | LS LS LS LS LS | -5 -5 -5 -5 -5 | 83 81 84 87 90 | | |
| Testing | Dewatering Pump | 45 | 20 | 8 | 100% | 0 | 53 | No | LS | No | 25 Days | LS | -5 | 48 | |
| <i>Wildcat Pipeline (El Cerrito) Tie-ins</i> | | | | | | | | | | | | | | | |
| Closest residential receptors at Liberty/Hill (north tie-in) and Lynn/San Carlos (south tie-in) | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | 30 30 30 30 30 | 4 4 4 4 4 | 20% 20% 40% 40% 40% | -7 -7 -4 -4 -4 | 98 72 81 76 79 | - - - - - | Yes No Yes Yes Yes | <10 Days <10 Days <10 Days <10 Days <10 Days | LS LS LS LS LS | 0 0 0 0 0 | 98 72 81 76 79 | |
| <i>Pipe Connection</i> | | | | | | | | | | | | | | | |
| Wildcat Pipeline (El Cerrito) Tie-ins | Hydraulic Compressor Hot Tapping Machine Hot Tapping Machine Motor/Generator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 81 76 79 | 30 30 30 25 25 | 4 4 4 6 6 | 100% 100% 100% 40% 40% | 0 0 0 -4 -4 | 84 82 85 78 81 | - - - - - | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | LS LS LS LS LS | -5 -5 -5 -5 -5 | 79 77 80 73 76 | | |
| Testing | Dewatering Pump | 45 | 30 | 4 | 100% | 0 | 49 | - | - | No | 25 Days | LS | -5 | 44 | |
| <i>Central Pressure Zone Pipeline (El Cerrito/Richmond) Tie-in</i> | | | | | | | | | | | | | | | |
| Closest residential receptors at San Pablo/ Nevin (north tie-in) | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | 130 130 130 130 130 | -8 -8 -8 -8 -8 | 20% 20% 40% 40% 40% | -7 -7 -4 -4 -4 | 86 60 69 64 67 | Yes No No No Yes | SM LS LS LS LS | Yes <10 Days <10 Days <10 Days <10 Days | LS 0 0 0 0 | 86 60 69 64 67 | | |
| <i>Pipe Connection</i> | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (El Cerrito/Richmond) Tie-in | Hydraulic Compressor Hot Tapping Machine Hot Tapping Machine Motor/Generator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 81 76 79 | 130 130 130 130 130 | -8 -8 -8 -8 -8 | 100% 100% 100% 40% 40% | 0 0 0 -4 -4 | 72 70 73 64 67 | Yes Yes Yes Yes Yes | SU SU SU SU SU | 1 Day 1 Day 1 Day 1 Day 1 Day | LS LS LS LS LS | -5 -5 -5 -5 -5 | 67 65 68 59 62 | | |
| Testing | Dewatering Pump | 45 | 30 | 4 | 100% | 0 | 49 | No | LS | No | 25 Days | LS | -5 | 44 | |
| <i>Highest Combined Leq at One Receptor:</i> | | | | | | | | | | | | | | | |
| Wildcat Pipeline (Berkeley) Tie-ins | Total Construction Days at One Receptor: 25 Days | | | | | | | | | | | | | | |
| El Cerrito Ordinance Noise Limit for Short-term Construction Activities: | 75 dBA | | | | | | | | | | | | | | |
| Richmond Ordinance Noise Limit for Short-term Construction Activities: | 75 dBA | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (El Cerrito/Richmond) Tie-in | Total Construction Days at One Receptor: 25 Days | | | | | | | | | | | | | | |

TABLE I-6 (Continued)
ESTIMATED DAYTIME CONSTRUCTION NOISE LEVELS

| Pipeline and Closest Noise-Sensitive Receptor Location | Construction Activity | Principal Noise Sources | Minimum Reference Noise Level, L _{max} in dBA at 50 feet ^a | | | | | | Impact 3.11-1 | | | Impact 3.11-2 | | | Noise Reduction From Mitigation Measure NOI-1 and NOI-2b ^e | | | |
|---|--|--|---|---------------------------------------|---|--|------------------------------------|--|--|---|---|---|---------------------------------|---|---|-------------------------------|---|---|
| | | | Distance Between Project and Closest Sensitive Receptor ^b | Noise Level Factor ^c | Adjustment Factor for Usage Factor ^c for Usage | Assumed Usage Factor ^c for Usage | Adjusted Factor for Distance | Noise Level Level Adjusted Daytime Significance | Leg Noise Level Ordinance Daytime Significance | Impact 3.11-1 | Leg Exceeds 70-dBA Speech Interference Threshold? | Duration of Construction ^d (Workdays) | Impact 3.11-2 Significance | Leg Exceeds 70-dBA Speech Interference Threshold? | Duration of Construction ^d (Workdays) | Impact 3.11-2 Significance | Leg Exceeds 70-dBA Speech Interference Threshold? | Duration of Construction ^d (Workdays) |
| Tie-in Construction | | | | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (El Cerrito/Richmond) Tie-in | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | -3 -3 -3 -3 -3 | 20% 20% 40% 40% 40% | 0 0 0 0 4 | -7 -7 4 4 4 | 91 65 74 69 72 | - - - - - | None | Yes No Yes Yes Yes | <10 Days <10 Days <10 Days <10 Days <10 Days | LS | 0 | 91 | 91 | 91 | |
| Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping Machine Motor/Generator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 81 76 79 | 30 30 30 10 10 | 4 4 4 14 14 | 100% 100% 100% 40% 40% | 0 0 0 4 4 | 84 82 85 86 89 | - - - - - | None | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | LS | -5 | 77 | 77 | 77 | | |
| Testing | Dewatering Pump | 45 | 30 | 4 | 100% | 0 | 49 | - | None | No | 25 Days | LS | -5 | 44 | 44 | 44 | 44 | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (Richmond/San Pablo) Tie-in | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | -3 -3 -3 -3 -3 | 20% 20% 40% 40% 40% | 0 0 4 4 4 | -7 -7 4 4 4 | 91 65 74 69 72 | - - - - - | None | Yes No Yes No Yes | <10 Days <10 Days <10 Days <10 Days <10 Days | LS | 0 | 91 | 91 | 91 | |
| Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping Machine Motor/Generator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 81 76 79 | 20 20 20 12 12 | 8 100% 100% 40% 40% | 0 0 0 4 4 | 0 0 0 84 87 | 88 86 89 84 87 | - - - - - | None | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | LS | -5 | 83 | 83 | 83 | | |
| Testing | Dewatering Pump | 45 | 20 | 8 | 100% | 0 | 53 | - | None | No | 25 Days | LS | -5 | 82 | 82 | 82 | 82 | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (Richmond/San Pablo) Tie-in | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | -3 -3 -3 -3 -3 | 20% 20% 40% 40% 40% | 0 0 0 0 4 | -7 -7 4 4 4 | 91 65 74 69 72 | - - - - - | 75 dBA | Yes No Yes No Yes | SM LS SU LS LS | Yes No Yes Yes Yes | <10 Days <10 Days <10 Days <10 Days <10 Days | LS | 0 | 91 | 91 |
| Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping Machine Motor/Generator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 81 76 79 | 40 40 40 40 40 | 100% 100% 100% 100% 100% | 0 0 0 0 0 | 82 80 83 80 83 | Yes Yes Yes Yes Yes | SM SU SU SM SU | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | LS | -5 | 75 | 75 | 75 | | | |
| Testing | Dewatering Pump | 45 | 40 | 2 | 100% | 0 | 47 | No | LS | No | 25 Days | LS | -5 | 42 | 42 | 42 | 42 | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Central Pressure Zone Pipeline (Richmond/San Pablo) Tie-in | Pit Excavation and Backfill | Impact/Vibratory Sheetpile Driver ^g – Upper Range Impact/Vibratory Sheetpile Driver – Lower Range Excavator Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 101 75 81 76 79 | -3 -3 -3 -3 -3 | 20% 20% 40% 40% 40% | 0 0 0 0 0 | -7 -7 4 4 4 | 91 65 74 69 72 | - - - - - | None | Yes Yes Yes Yes Yes | LS LS LS LS LS | Yes Yes Yes Yes Yes | <10 Days <10 Days <10 Days <10 Days <10 Days | LS | 0 | 72 | 72 |

TABLE I-6 (Continued)
ESTIMATED DAYTIME CONSTRUCTION NOISE LEVELS

NOTES: Noise Levels in **BOLD** indicate a significant impact because they exceed the ordinance noise limit and/or exceed the 70-dBA speech interference threshold for longer than two weeks (10 weekdays). "SU" indicates the impact would be significant and could not be reduced to a less-than-significant level with specified mitigation measures.

^a Reference noise levels are based on noise measurements collected during construction of the Central Artery/Tunnel Project (completed in 2007) and these measurements also serve as default values in the FHWA Roadway Construction Noise Model. Available online at: http://www.fhwa.dot.gov/environment/noise/construction_noise/handbook09.cfm

^b These distances represent the predominant setback distance from the closest receptors to the curb, which is the closest possible location where construction equipment could operate. For San Pablo Avenue, there are scattered residential uses along the alignment with setback distances ranging between 15 and 45 feet, and this distance represents the average setback distance. For the combined noise level, the minimum distance between source and receptor would vary because of the narrow work area. Also, as construction progresses approximately 200 feet along the pipeline alignment each day, the equipment operations is also conservatively estimated to move at least 100 feet along the alignment.

^c Equipment usage factors are estimated by the Federal Highway Administration based on a roadway tunnel project (FHWA, 2006), but adjusted based on noise monitoring experience of Wilson Ihrig Associates (WIA) on similar construction projects.

^d For daytime noise, significance is determined based on whether both the speech interference threshold and two-week construction duration threshold is exceeded at a given receptor.

^e Mitigation Measure NOI-1 includes EBMUD Best Practices mitigation measures to reduce noise levels using noise standards of the local jurisdictions and measures to reduce noise levels for activities that may generate noise levels greater than 90 dBA (if applicable).

^f A mobile batch plant is assumed to include a colloidal mixer, agitator, and hydraulic double-acting pump and operate without an enclosure (WIA, 2001).

^g Reference hourly noise level of 101 dBA (L_{max}) applied, but assumes maximum noise levels would occur 20% of every one-hour time period (12 minutes). Noise levels generated by a sheetpile driver can vary substantially if a vibratory impact pile driver can be used instead of an impact pile driver and if no substantial subsurface obstructions are encountered. The low to high range captures the potential variation in noise levels due to these factors (i.e. impact vs. vibratory and subsurface obstructions vs. no obstructions).

^h Since the boring machine only operates in the insertion pit, this is the distance to the closest residential receptor at the insertion pit. Since the boring machine/jigger would be located at the bottom of the insertion pit, an 5 dBA reduction is applied to account for noise attenuation benefits by pit walls (see Noise Reduction from Mitigation column). Since the boring jack power unit would be located at ground surface (above the pit), no additional attenuation benefit from the pit walls is applied. However, implementation of Mitigation Measure NOI-1b is conservatively estimated provide a minimum 3-dB noise reduction during operation of the boring jack power unit.

Source: Orion Environmental Associates.

TABLE I-7
ESTIMATED NIGHTTIME CONSTRUCTION NOISE LEVELS

| Pipeline and Closest Noise-Sensitive Receptor Location | Construction Activity | Principal Noise Source | Reference Noise Level, L _{max} in dBA at 50 feet ^a | Residential Receptors ^b | Noise Level Factor for Usage Factor ^c for Usage | Noise Level Factor for Usage Factor ^c for Usage | L _{eq} Noise Level Factor for Usage Factor ^c for Usage | Impact 3.11-1 | | Impact 3.11-2 | | | | | | | | |
|--|--------------------------|--|--|---------------------------------------|---|---|---|---------------------------------|--|---|--|----|--|--|--|--|--|--|
| | | | | | | | | Exceeds 54-dBA Ordinance | Nighttime Significance Determination | Exceeds 60-dBA Impact 3.11-1 | Sleep Duration of Disturbance | | | | | | | |
| Tie-in Construction | | | | | | | | | | | | | | | | | | |
| Wildcat Pipeline Tie-ins (Berkeley) | | | | | | | | | | | | | | | | | | |
| Closest residential receptors on: Parkside and Dana | Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping & Lighting Generators Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 84 76 79 | 8 8 8 5 5 | 100% 100% 100% 40% 40% | 0 0 0 4 4 | 88 86 92 92 95 | Yes Yes Yes Yes Yes | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | SU SU SU SU SU | | | | | | | |
| Testing | Dewatering Pump | | 45 | 20 | 8 | 100% | 0 | No | LS | No | 20 Days | LS | | | | | | |
| Wildcat Pipeline Tie-ins (El Cerrito) | | | | | | | | | | | | | | | | | | |
| Closest residential receptors at Liberty/Hill (north tie-in) and Lynn/San Carlos (south tie-in) | Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping & Lighting Generators Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 84 76 79 | 30 30 30 25 25 | 100% 100% 100% 40% 40% | 0 0 0 4 4 | 84 82 88 78 81 | Yes Yes Yes Yes Yes | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | SU SU SU SU SU | | | | | | | |
| Testing | Dewatering Pump | | 45 | 30 | 4 | 100% | 0 | No | LS | No | 20 Days | LS | | | | | | |
| Central Pressure Zone Pipeline Tie-ins (El Cerrito) | | | | | | | | | | | | | | | | | | |
| Closest residential receptors at San Pablo/Nevin (north tie-in) and San Pablo/Central (south tie-in) | Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping & Lighting Generators Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 84 76 79 | 30 30 30 10 10 | 100% 100% 100% 40% 40% | 0 0 0 4 4 | 84 82 88 86 89 | Yes Yes Yes Yes Yes | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | SU SU SU SM SU | | | | | | | |
| Testing | Dewatering Pump | | 45 | 30 | 4 | 100% | 0 | No | LS | No | 20 Days | LS | | | | | | |
| Central Pressure Zone Pipeline Tie-in (Richmond) | | | | | | | | | | | | | | | | | | |
| Closest residential receptor at Road 20th/21st (north tie-in) | Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping & Lighting Generators Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 84 76 79 | 20 20 20 12 12 | 100% 100% 100% 40% 40% | 0 0 0 4 4 | 88 86 92 84 87 | Yes Yes Yes Yes Yes | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | SU SU SU SU SU | | | | | | | |
| Testing | Dewatering Pump | | 45 | 20 | 8 | 100% | 0 | No | LS | No | 20 Days | LS | | | | | | |
| Central Pressure Zone Pipeline Tie-in (San Pablo) | | | | | | | | | | | | | | | | | | |
| Closest residential receptors at 23rd/Nevin (south tie-in) | Pipe Connection | Hydraulic Compressor Hot Tapping Machine Hot Tapping & Lighting Generators Various Trucks (dump, flatbed, water) Backhoe, Loader, Forklift | 80 78 84 76 79 | 40 40 40 20 20 | 100% 100% 100% 40% 40% | 0 0 0 4 4 | 82 80 86 80 83 | Yes Yes Yes Yes Yes | Yes Yes Yes Yes Yes | 1 Day 1 Day 1 Day 1 Day 1 Day | SU SU SU SU SU | | | | | | | |
| Testing | Dewatering Pump | | 45 | 40 | 2 | 100% | 0 | No | LS | No | 20 Days | LS | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| San Pablo Ordinance Noise Limit for Nighttime Construction Activities: | | | | | | | | | | | | | | | | | | |
| Total Construction Days at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |
| Highest Combined Leg at One Receptor: | | | | | | | | | | | | | | | | | | |

TABLE I-7 (Continued)
ESTIMATED NIGHTTIME CONSTRUCTION NOISE LEVELS

| 3.11-2 | | | | | | | | | |
|---|----------------------------------|---------------------------------------|---|-------------|--------------------------|-------------|-----------------------------|---------------|---|
| Pipeline and Closest Noise-Sensitive Receptor Location | Construction Activity | Principal Noise Source | Distance Between Project and Closest Residential Receptors ^a | Noise Level | Assumed Factor for Usage | Noise Level | L _{eq} Noise Level | Impact 3.11-1 | Exceeds 60-dB(A) Sleep Impact 3.11-1 |
| 3.11-2 | | | | | | | | | |
| Open Trench Pipeline Construction at Some Major Intersections | | | | | | | | | |
| <i>Berkeley and Richmond Ordinance Noise Limit for Nighttime Construction Activities:</i> | | | | | | | | | |
| <i>Intersections (All Locations)</i> | | | | | | | | | |
| Minimum Distance from Residential Receptors | Pavement Cutting | Pavement Saw | 90 | 20 | 8 | 10% | -10 | 88 | SU |
| | | Jackhammer | 89 | 20 | 8 | 10% | -10 | 87 | SU |
| | Excavation and Pipe Installation | Excavator | 81 | 20 | 3 | 40% | -4 | 85 | SU |
| | | Various Trucks (dump, flatbed, water) | 76 | 20 | 3 | 40% | -4 | 80 | Yes |
| | | Backhoe, Loader, Forklift | 79 | 20 | 8 | 40% | -4 | 83 | Yes |
| | | Mobile Batch Plant | 76 | 20 | 8 | 15% | -8 | 76 | Yes |
| | Repaving | Paving Equipment (roller) | 80 | 20 | 8 | 10% | -10 | 78 | Yes |
| | | Compactor | 83 | 20 | 8 | 10% | -10 | 81 | Yes |
| | | | | | | | | | Total Construction Days at One Receptor: 6 Days |
| | | | | | | | | | |
| | | | | | | | | | |

NOTES: Noise Levels in **BOLD** indicate a significant impact because they exceed the ordinance noise limit and/or exceed the 60-dB(A) sleep interference threshold. "SU" indicates the impact would be significant and could not be reduced to a less-than-significant level with specified mitigation measures.

^a Reference noise levels are based on noise measurements collected during construction of the Central Artery/Tunnel Project (completed in 2007) and these measurements also serve as default values in the FHWA Roadway Construction Noise Model. Available online at: http://www.fhwa.dot.gov/environment/noise/construction_noise/handbook09.htm

^b These distances represent the predominant setback distance from the closest sensitive receptors with a direct line-of-sight to the closest possible location where construction equipment could operate. For the combined noise level, the minimum distance between source and receptor would vary because all equipment could not operate at the same minimum distance simultaneously because of the limited work area at tie-ins.

^c Equipment usage factors are estimated by the Federal Highway Administration based on a roadway tunnel project (FHWA, 2006), but adjusted based on noise monitoring experience of Wilson Ihrig Associates (WIA) on similar construction projects.

^d For nighttime noise, significance is based solely on whether the estimated noise level exceeds the sleep interference threshold (i.e. construction duration is not a factor) since even one night of sleep disruption is considered significant.

Source: Orion Environmental Associates.

TABLE I-8
ESTIMATED CONSTRUCTION VIBRATION LEVELS

| Pipeline and Closest Structure | Construction Activity | Construction Equipment with Potential to Generate Vibration that Could Cause Cosmetic or Structural Damage | Reference Vibration Level, in/sec PPV at 25 feet ^a | Distance Between Project and Closest Structure ^b | Vibration Level Adjusted for Distance | Impact 3.11-3 | | |
|--|----------------------------------|--|---|---|---------------------------------------|--|--|--|
| | | | | | | Exceeds 0.5 in/sec PPV Cosmetic Damage Threshold for Impact? | Exceeds 0.4 in/sec PPV Cosmetic Damage Threshold for Continuous Vibration? | Impact 3.11-3 Significance Determination |
| Open Trench Pipeline Construction | | | | | | | | |
| All Pipelines | | | | | | | | |
| Closet structures to Pipeline | Excavation and Pipe Installation | Earthmoving Equipment | 0.089 | 15 | 0.191 | - | Yes | SM |
| Alignments | | Backfill and Repaving | 0.076 | 10 | 0.300 | - | No | LS |
| Jack-and-Bore and Tie-in Construction | | | | | | | | |
| Willcat Creek Crossing (San Pablo) and All Pipeline Tie-ins | Pit Excavation | Impact Sheetpile Driver-Upper Range OR | 1.518 | 15 | 3.266 | Yes | - | SM |
| Closet structure to Southerly Receiving Pit (15 feet) and closest structure to Creek | | Impact Sheetpile Driver-Low Range | 0.644 | 15 | 1.386 | Yes | - | SM |
| Crossing Tie-in Pits (18 feet) | | Vibratory Sheetpile Driver-Upper Range OR | 0.734 | 15 | 1.579 | - | Yes | SM |
| | | Vibratory Sheetpile Driver-Lower Range | 0.170 | 15 | 0.366 | - | No | LS |
| | | Earthmoving Equipment | 0.089 | 15 | 0.191 | - | No | LS |
| | | Loaded Trucks | 0.076 | 15 | 0.164 | - | No | LS |
| | Repaving | Vibratory Compactor | 0.210 | 15 | 0.452 | - | Yes | SM |
| | | Jumping Jack/Vibratory Compactor | 0.035 | 15 | 0.075 | - | No | LS |
| Pipe Bridge Construction | | | | | | | | |
| San Pablo Creek Crossing (San Pablo) | | | | | | | | |
| Closet structure to either pipe bridge | Excavation | Caisson Drilling | 0.089 | 70 | 0.019 | - | No | LS |
| Tie-in Construction | | | | | | | | |
| Willcat Pipeline Tie-ins (Berkeley) | | | | | | | | |
| Closet residential receptors on: Parkside and Dana | Pipe Connection | Earthmoving Equipment | 0.089 | 20 | 0.124 | - | No | LS |
| | | Loaded Trucks | 0.076 | 20 | 0.106 | - | No | LS |
| Willcat Pipeline Tie-ins (El Cerrito) | | | | | | | | |
| Closet residential receptors 40 feet from north tie-in and 30 feet from south tie-in | Pipe Connection | Earthmoving Equipment | 0.089 | 30 | 0.068 | - | No | LS |
| | | Loaded Trucks | 0.076 | 30 | 0.058 | - | No | LS |
| Tie-in Construction | | | | | | | | |
| Central Pressure Zone Pipeline Tie-ins (El Cerrito) | | | | | | | | |
| Closet residential receptors with direct line-of-sight located 125 feet from north tie-in and 250 feet from south tie-in | Pipe Connection | Earthmoving Equipment | 0.089 | 30 | 0.068 | - | No | LS |
| | | Loaded Trucks | 0.076 | 30 | 0.058 | - | No | LS |
| Central Pressure Zone Pipeline Tie-in (Richmond) | | | | | | | | |
| Closet residential receptor at 404 23rd Street | Pipe Connection | Earthmoving Equipment | 0.089 | 20 | 0.124 | - | No | LS |
| | | Loaded Trucks | 0.076 | 20 | 0.106 | - | No | LS |
| Central Pressure Zone Pipeline Tie-in (San Pablo) | | | | | | | | |
| Closet residential receptors at 2028, 2029, 2100, and 2101 Road 20 | Pipe Connection | Earthmoving Equipment | 0.089 | 40 | 0.044 | - | No | LS |
| | | Loaded Trucks | 0.076 | 40 | 0.038 | - | No | LS |

NOTES: Vibration levels in **BOLD** indicate a significant impact because they exceed the threshold for either impact or continuous vibration for cosmetic damage. "SW" indicates the impact would be significant but mitigated to a less-than-significant level with specified mitigation measures.

^a Reference vibration levels are based on vibration data provided by the Federal Transit Administration (FTA, 2006).

^b These distances represent the predominant minimum setback distance from the closest receptors to the curb, which is the closest possible location where construction equipment could operate.

Source: Orion Environmental Associates.

APPENDIX J

Wildcat Pipeline (Berkeley) Level of Service Calculations

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2016 Wildcat Pipeline (Berkeley) No Project AM Peak

1: Derby St & Telegraph Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 7 | 30 | 27 | 67 | 34 | 19 | 17 | 641 | 43 | 34 | 454 | 3 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | | | | | | | | 1.00 | 1.00 | | 0.95 | 1.00 |
| Fr _t | | | | | | | | 0.94 | 0.98 | | 1.00 | 0.85 |
| Flt Protected | | | | | | | | 0.99 | 0.97 | | 1.00 | 1.00 |
| Satd. Flow (prot) | | | | | | | | 1749 | 1773 | | 3535 | 1583 |
| Flt Permitted | | | | | | | | 0.94 | 0.79 | | 0.94 | 1.00 |
| Satd. Flow (perm) | | | | | | | | 1649 | 1437 | | 3322 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 8 | 33 | 29 | 73 | 37 | 21 | 18 | 697 | 47 | 37 | 493 | 3 |
| RTOR Reduction (vph) | 0 | 24 | 0 | 0 | 18 | 0 | 0 | 0 | 23 | 0 | 0 | 1 |
| Lane Group Flow (vph) | 0 | 46 | 0 | 0 | 113 | 0 | 0 | 715 | 24 | 0 | 530 | 2 |
| Turn Type | Perm | | | Perm | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 4.0 | | | 4.0 | | | 12.6 | 12.6 | | 12.6 | 12.6 |
| Effective Green, g (s) | | 4.0 | | | 4.0 | | | 12.6 | 12.6 | | 12.6 | 12.6 |
| Actuated g/C Ratio | | 0.16 | | | 0.16 | | | 0.51 | 0.51 | | 0.51 | 0.51 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 268 | | | 234 | | | 1702 | 811 | | 1613 | 811 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.03 | | | c0.08 | | | c0.22 | 0.02 | | 0.17 | 0.00 | |
| v/c Ratio | 0.17 | | | 0.48 | | | 0.42 | 0.03 | | 0.33 | 0.00 | |
| Uniform Delay, d1 | 8.9 | | | 9.4 | | | 3.7 | 3.0 | | 3.5 | 2.9 | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | | | 1.6 | | | 0.2 | 0.0 | | 0.1 | 0.0 | |
| Delay (s) | 9.2 | | | 10.9 | | | 3.9 | 3.0 | | 3.6 | 2.9 | |
| Level of Service | A | | | B | | | A | A | | A | A | |
| Approach Delay (s) | 9.2 | | | 10.9 | | | 3.8 | | | 3.6 | | |
| Approach LOS | A | | | B | | | A | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 4.6 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.44 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 24.6 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 55.1% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) No Project AM Peak

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 5 | 70 | 26 | 77 | 68 | 55 | 47 | 681 | 17 | 12 | 531 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | 0.99 | | | | 0.99 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 0.97 | | | | 0.96 | | | 1.00 | | | 0.99 | |
| Fl _t Protected | 1.00 | | | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1778 | | | | 1730 | | | 3502 | | | 3499 | |
| Fl _t Permitted | 0.98 | | | | 0.83 | | | 0.89 | | | 0.94 | |
| Satd. Flow (perm) | 1742 | | | | 1457 | | | 3144 | | | 3278 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 5 | 76 | 28 | 84 | 74 | 60 | 51 | 740 | 18 | 13 | 577 | 29 |
| RTOR Reduction (vph) | 0 | 21 | 0 | 0 | 37 | 0 | 0 | 4 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 0 | 88 | 0 | 0 | 182 | 0 | 0 | 805 | 0 | 0 | 611 | 0 |
| Confl. Peds. (#/hr) | 62 | | 22 | 22 | | 62 | 40 | | 94 | 94 | | 40 |
| Confl. Bikes (#/hr) | | | 8 | | | 3 | | | 44 | | | 5 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 6.9 | | | 6.9 | | | 13.9 | | | 13.9 | | |
| Effective Green, g (s) | 6.9 | | | 6.9 | | | 13.9 | | | 13.9 | | |
| Actuated g/C Ratio | 0.24 | | | 0.24 | | | 0.48 | | | 0.48 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 417 | | | 349 | | | 1517 | | | 1582 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.05 | | | c0.12 | | | c0.26 | | | 0.19 | | |
| v/c Ratio | 0.21 | | | 0.52 | | | 0.53 | | | 0.39 | | |
| Uniform Delay, d1 | 8.8 | | | 9.5 | | | 5.2 | | | 4.7 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 0.3 | | | 1.4 | | | 0.4 | | | 0.2 | | |
| Delay (s) | 9.0 | | | 10.9 | | | 5.5 | | | 4.9 | | |
| Level of Service | A | | | B | | | A | | | A | | |
| Approach Delay (s) | 9.0 | | | 10.9 | | | 5.5 | | | 4.9 | | |
| Approach LOS | A | | | B | | | A | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 6.2 | | | HCM Level of Service | | | A | | | | | |
| HCM Volume to Capacity ratio | 0.53 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 28.8 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 66.0% | | | ICU Level of Service | | | C | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Sign Control | Stop | | | Stop | Stop | |
| Volume (vph) | 21 | 75 | 93 | 359 | 232 | 33 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 23 | 82 | 101 | 390 | 252 | 36 |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total (vph) | 104 | 491 | 288 | | | |
| Volume Left (vph) | 23 | 101 | 0 | | | |
| Volume Right (vph) | 82 | 0 | 36 | | | |
| Hadj (s) | -0.39 | 0.08 | -0.04 | | | |
| Departure Headway (s) | 5.3 | 4.6 | 4.7 | | | |
| Degree Utilization, x | 0.15 | 0.63 | 0.38 | | | |
| Capacity (veh/h) | 600 | 767 | 734 | | | |
| Control Delay (s) | 9.2 | 15.1 | 10.5 | | | |
| Approach Delay (s) | 9.2 | 15.1 | 10.5 | | | |
| Approach LOS | A | C | B | | | |
| Intersection Summary | | | | | | |
| Delay | | | | 12.9 | | |
| HCM Level of Service | | | | B | | |
| Intersection Capacity Utilization | | 60.7% | | ICU Level of Service | | B |
| Analysis Period (min) | | | 15 | | | |

2016 Wildcat Pipeline (Berkeley) No Project AM Peak

4: Ashby Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|------|------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 6 | 415 | 70 | 6 | 625 | 156 | 76 | 316 | 22 | 69 | 173 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | | | | | | | | | | | | |
| Flt Protected | | | | | | | | | | | | |
| Satd. Flow (prot) | | | | | | | | | | | | |
| Flt Permitted | | | | | | | | | | | | |
| Satd. Flow (perm) | | | | | | | | | | | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 7 | 451 | 76 | 7 | 679 | 170 | 83 | 343 | 24 | 75 | 188 | 62 |
| RTOR Reduction (vph) | 0 | 15 | 0 | 0 | 55 | 0 | 0 | 5 | 0 | 0 | 22 | 0 |
| Lane Group Flow (vph) | 0 | 519 | 0 | 0 | 801 | 0 | 0 | 445 | 0 | 0 | 303 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | | 14.0 | | | 14.0 | | | 13.5 | | | 13.5 | |
| Effective Green, g (s) | | 14.0 | | | 14.0 | | | 13.5 | | | 13.5 | |
| Actuated g/C Ratio | | 0.39 | | | 0.39 | | | 0.38 | | | 0.38 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | | 711 | | | 1287 | | | 630 | | | 591 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | c0.29 | | | 0.25 | | | c0.27 | | | 0.20 | |
| v/c Ratio | | 0.73 | | | 0.62 | | | 0.71 | | | 0.51 | |
| Uniform Delay, d1 | | 9.1 | | | 8.6 | | | 9.3 | | | 8.5 | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | 3.8 | | | 0.9 | | | 3.6 | | | 0.8 | |
| Delay (s) | | 12.9 | | | 9.6 | | | 12.9 | | | 9.2 | |
| Level of Service | | B | | | A | | | B | | | A | |
| Approach Delay (s) | | 12.9 | | | 9.6 | | | 12.9 | | | 9.2 | |
| Approach LOS | | B | | | A | | | B | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.0 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.72 | | |
| Actuated Cycle Length (s) | 35.5 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 65.3% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat Pipeline (Berkeley) No Project AM Peak

5: Alcatraz Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 43 | 136 | 140 | 12 | 125 | 10 | 131 | 310 | 18 | 7 | 213 | 51 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Flt Protected | 0.94 | | | | 0.99 | | | | 0.99 | | | 0.97 |
| Flt Permitted | 0.99 | | | | 1.00 | | | | 0.99 | | | 1.00 |
| Satd. Flow (prot) | 1741 | | | | 1838 | | | | 1827 | | | 1813 |
| Flt Permitted | 0.94 | | | | 0.96 | | | | 0.83 | | | 0.99 |
| Satd. Flow (perm) | 1646 | | | | 1767 | | | | 1533 | | | 1790 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 47 | 148 | 152 | 13 | 136 | 11 | 142 | 337 | 20 | 8 | 232 | 55 |
| RTOR Reduction (vph) | 0 | 67 | 0 | 0 | 6 | 0 | 0 | 3 | 0 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 0 | 280 | 0 | 0 | 154 | 0 | 0 | 496 | 0 | 0 | 276 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 10.8 | | | 10.8 | | | 15.7 | | | 15.7 | | |
| Effective Green, g (s) | 10.8 | | | 10.8 | | | 15.7 | | | 15.7 | | |
| Actuated g/C Ratio | 0.31 | | | 0.31 | | | 0.46 | | | 0.46 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 515 | | | 553 | | | 698 | | | 815 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.17 | | | 0.09 | | | c0.32 | | | 0.15 | | |
| v/c Ratio | 0.54 | | | 0.28 | | | 0.71 | | | 0.34 | | |
| Uniform Delay, d1 | 9.8 | | | 8.9 | | | 7.6 | | | 6.1 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 1.2 | | | 0.3 | | | 3.4 | | | 0.2 | | |
| Delay (s) | 11.0 | | | 9.2 | | | 11.0 | | | 6.3 | | |
| Level of Service | B | | | A | | | B | | | A | | |
| Approach Delay (s) | 11.0 | | | 9.2 | | | 11.0 | | | 6.3 | | |
| Approach LOS | B | | | A | | | B | | | A | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 9.7 | HCM Level of Service | A |
| HCM Volume to Capacity ratio | 0.64 | | |
| Actuated Cycle Length (s) | 34.5 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 77.3% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat Pipeline (Berkeley) No Project AM Peak

6: The Uplands & Claremont Ave

6/7/2012



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 86 | 77 | 411 | 54 | 31 | 370 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | | | 4.0 |
| Lane Util. Factor | 1.00 | | 0.95 | | | 0.95 |
| Frpb, ped/bikes | 0.99 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.94 | | 0.98 | | | 1.00 |
| Fl _t Protected | 0.97 | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 1676 | | 3463 | | | 3524 |
| Fl _t Permitted | 0.97 | | 1.00 | | | 0.89 |
| Satd. Flow (perm) | 1676 | | 3463 | | | 3156 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 93 | 84 | 447 | 59 | 34 | 402 |
| RTOR Reduction (vph) | 68 | 0 | 26 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 109 | 0 | 480 | 0 | 0 | 436 |
| Confl. Peds. (#/hr) | 52 | 46 | | 19 | 19 | |
| Confl. Bikes (#/hr) | | | | | | 5 |
| Turn Type | | | | | | Perm |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | | | 6 | |
| Actuated Green, G (s) | 3.8 | | 7.8 | | | 7.8 |
| Effective Green, g (s) | 3.8 | | 7.8 | | | 7.8 |
| Actuated g/C Ratio | 0.19 | | 0.40 | | | 0.40 |
| Clearance Time (s) | 4.0 | | 4.0 | | | 4.0 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 325 | | 1378 | | | 1256 |
| v/s Ratio Prot | c0.07 | | c0.14 | | | |
| v/s Ratio Perm | | | | | 0.14 | |
| v/c Ratio | 0.34 | | 0.35 | | | 0.35 |
| Uniform Delay, d1 | 6.8 | | 4.1 | | | 4.1 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.6 | | 0.2 | | | 0.2 |
| Delay (s) | 7.4 | | 4.3 | | | 4.3 |
| Level of Service | A | | A | | | A |
| Approach Delay (s) | 7.4 | | 4.3 | | | 4.3 |
| Approach LOS | A | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 4.8 | | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | 0.34 | | | | |
| Actuated Cycle Length (s) | | 19.6 | | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | 47.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

2016 Wildcat Pipeline (Berkeley) No Project AM Peak

7: Brookside Dr & Claremont Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 1 | 0 | 0 | 17 | 0 | 15 | 1 | 463 | 10 | 6 | 436 | 1 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 1 | 0 | 0 | 18 | 0 | 16 | 1 | 503 | 11 | 7 | 474 | 1 |
| Pedestrians | | 27 | | | 16 | | | 2 | | | 1 | |
| Lane Width (ft) | | 12.0 | | | 12.0 | | | 12.0 | | | 12.0 | |
| Walking Speed (ft/s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Percent Blockage | | 2 | | | 1 | | | 0 | | | 0 | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | 460 | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 786 | 1047 | 266 | 779 | 1042 | 274 | 502 | | | 530 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 786 | 1047 | 266 | 779 | 1042 | 274 | 502 | | | 530 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 100 | 100 | 100 | 93 | 100 | 98 | 100 | | | 99 | | |
| cM capacity (veh/h) | 261 | 217 | 714 | 272 | 219 | 713 | 1035 | | | 1020 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total | 1 | 35 | 253 | 262 | 243 | 238 | | | | | | |
| Volume Left | 1 | 18 | 1 | 0 | 7 | 0 | | | | | | |
| Volume Right | 0 | 16 | 0 | 11 | 0 | 1 | | | | | | |
| cSH | 261 | 384 | 1035 | 1700 | 1020 | 1700 | | | | | | |
| Volume to Capacity | 0.00 | 0.09 | 0.00 | 0.15 | 0.01 | 0.14 | | | | | | |
| Queue Length 95th (ft) | 0 | 7 | 0 | 0 | 0 | 0 | | | | | | |
| Control Delay (s) | 18.9 | 15.3 | 0.0 | 0.0 | 0.3 | 0.0 | | | | | | |
| Lane LOS | C | C | A | | A | | | | | | | |
| Approach Delay (s) | 18.9 | 15.3 | 0.0 | | 0.1 | | | | | | | |
| Approach LOS | C | C | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 0.6 | | | | | | | | | |
| Intersection Capacity Utilization | | 27.0% | | ICU Level of Service | | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) No Project PM Peak

1: Derby St & Telegraph Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|-------|------|------|------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 16 | 61 | 29 | 110 | 74 | 20 | 29 | 531 | 62 | 56 | 791 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | | | | | | | | 1.00 | 1.00 | | 0.95 | 1.00 |
| Fr _t | | | | | | | | 0.96 | 0.99 | | 1.00 | 0.85 |
| Flt Protected | | | | | | | | 0.99 | 0.97 | | 1.00 | 1.00 |
| Satd. Flow (prot) | | | | | | | | 1780 | 1789 | | 3530 | 1583 |
| Flt Permitted | | | | | | | | 0.93 | 0.77 | | 0.89 | 1.00 |
| Satd. Flow (perm) | | | | | | | | 1662 | 1414 | | 3153 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 17 | 66 | 32 | 120 | 80 | 22 | 32 | 577 | 67 | 61 | 860 | 18 |
| RTOR Reduction (vph) | 0 | 24 | 0 | 0 | 12 | 0 | 0 | 0 | 34 | 0 | 0 | 9 |
| Lane Group Flow (vph) | 0 | 91 | 0 | 0 | 210 | 0 | 0 | 609 | 33 | 0 | 921 | 9 |
| Turn Type | Perm | | | Perm | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 7.7 | | | 7.7 | | | 14.8 | 14.8 | | 14.8 | 14.8 |
| Effective Green, g (s) | | 7.7 | | | 7.7 | | | 14.8 | 14.8 | | 14.8 | 14.8 |
| Actuated g/C Ratio | | 0.25 | | | 0.25 | | | 0.49 | 0.49 | | 0.49 | 0.49 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 420 | | | 357 | | | 1530 | 768 | | 1527 | 768 |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | 0.05 | | | c0.15 | | | 0.19 | 0.02 | | c0.29 | 0.01 |
| v/c Ratio | | 0.22 | | | 0.59 | | | 0.40 | 0.04 | | 0.60 | 0.01 |
| Uniform Delay, d1 | | 9.0 | | | 10.0 | | | 5.0 | 4.1 | | 5.7 | 4.1 |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.3 | | | 2.5 | | | 0.2 | 0.0 | | 0.7 | 0.0 |
| Delay (s) | | 9.3 | | | 12.5 | | | 5.2 | 4.1 | | 6.4 | 4.1 |
| Level of Service | | A | | | B | | | A | A | | A | A |
| Approach Delay (s) | | 9.3 | | | 12.5 | | | 5.1 | | | 6.3 | |
| Approach LOS | | A | | | B | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 6.8 | HCM Level of Service | A |
| HCM Volume to Capacity ratio | 0.60 | | |
| Actuated Cycle Length (s) | 30.5 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 66.9% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat Pipeline (Berkeley) No Project PM Peak

2: Stuart St & Telegraph Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 2 | 57 | 41 | 46 | 45 | 24 | 15 | 664 | 40 | 12 | 863 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | | | 1.00 | | | 0.95 | | | 0.95 | | |
| Frpb, ped/bikes | 0.99 | | | | 0.99 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 0.94 | | | | 0.97 | | | 0.99 | | | 1.00 | |
| Fl _t Protected | 1.00 | | | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1737 | | | | 1759 | | | 3492 | | | 3514 | |
| Fl _t Permitted | 0.99 | | | | 0.82 | | | 0.93 | | | 0.94 | |
| Satd. Flow (perm) | 1721 | | | | 1473 | | | 3255 | | | 3318 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 62 | 45 | 50 | 49 | 26 | 16 | 722 | 43 | 13 | 938 | 27 |
| RTOR Reduction (vph) | 0 | 25 | 0 | 0 | 22 | 0 | 0 | 8 | 0 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 0 | 84 | 0 | 0 | 103 | 0 | 0 | 773 | 0 | 0 | 974 | 0 |
| Confl. Peds. (#/hr) | 26 | | 14 | 14 | | 26 | 64 | | 48 | 48 | | 64 |
| Confl. Bikes (#/hr) | | | 6 | | | 5 | | | 15 | | | 5 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 4.0 | | | | 4.0 | | | 14.4 | | | 14.4 | |
| Effective Green, g (s) | 4.0 | | | | 4.0 | | | 14.4 | | | 14.4 | |
| Actuated g/C Ratio | 0.15 | | | | 0.15 | | | 0.55 | | | 0.55 | |
| Clearance Time (s) | 4.0 | | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 261 | | | 223 | | | 1775 | | | 1810 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.05 | | | c0.07 | | | 0.24 | | | c0.29 | | |
| v/c Ratio | 0.32 | | | 0.46 | | | 0.44 | | | 0.54 | | |
| Uniform Delay, d1 | 10.0 | | | 10.2 | | | 3.6 | | | 3.9 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 0.7 | | | 1.5 | | | 0.2 | | | 0.3 | | |
| Delay (s) | 10.7 | | | 11.7 | | | 3.7 | | | 4.2 | | |
| Level of Service | B | | | B | | | A | | | A | | |
| Approach Delay (s) | 10.7 | | | 11.7 | | | 3.7 | | | 4.2 | | |
| Approach LOS | B | | | B | | | A | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 4.8 | | HCM Level of Service | | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.52 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 26.4 | | Sum of lost time (s) | | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 53.5% | | ICU Level of Service | | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Sign Control | Stop | | | Stop | Stop | |
| Volume (vph) | 36 | 103 | 86 | 271 | 394 | 55 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 39 | 112 | 93 | 295 | 428 | 60 |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total (vph) | 151 | 388 | 488 | | | |
| Volume Left (vph) | 39 | 93 | 0 | | | |
| Volume Right (vph) | 112 | 0 | 60 | | | |
| Hadj (s) | -0.36 | 0.08 | -0.04 | | | |
| Departure Headway (s) | 5.6 | 5.0 | 4.8 | | | |
| Degree Utilization, x | 0.24 | 0.54 | 0.65 | | | |
| Capacity (veh/h) | 570 | 693 | 728 | | | |
| Control Delay (s) | 10.3 | 13.9 | 16.5 | | | |
| Approach Delay (s) | 10.3 | 13.9 | 16.5 | | | |
| Approach LOS | B | B | C | | | |
| Intersection Summary | | | | | | |
| Delay | | | | 14.6 | | |
| HCM Level of Service | | | | B | | |
| Intersection Capacity Utilization | | 66.8% | | ICU Level of Service | | C |
| Analysis Period (min) | | | | 15 | | |

2016 Wildcat Pipeline (Berkeley) No Project PM Peak

4: Ashby Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|------|------|------|------|------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 14 | 739 | 81 | 8 | 463 | 105 | 45 | 230 | 44 | 108 | 240 | 60 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | | 0.99 | | | | 0.97 | | | 0.98 | | | 0.98 |
| Flt Protected | | 1.00 | | | | 1.00 | | | 0.99 | | | 0.99 |
| Satd. Flow (prot) | | 1837 | | | | 3440 | | | 1815 | | | 1802 |
| Flt Permitted | | 0.99 | | | | 0.94 | | | 0.90 | | | 0.77 |
| Satd. Flow (perm) | | 1817 | | | | 3249 | | | 1642 | | | 1402 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 15 | 803 | 88 | 9 | 503 | 114 | 49 | 250 | 48 | 117 | 261 | 65 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 30 | 0 | 0 | 9 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 900 | 0 | 0 | 596 | 0 | 0 | 338 | 0 | 0 | 434 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | | 33.2 | | | 33.2 | | | 21.2 | | | 21.2 | |
| Effective Green, g (s) | | 33.2 | | | 33.2 | | | 21.2 | | | 21.2 | |
| Actuated g/C Ratio | | 0.53 | | | 0.53 | | | 0.34 | | | 0.34 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | | 967 | | | 1729 | | | 558 | | | 476 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | c0.50 | | | 0.18 | | | 0.21 | | | c0.31 | |
| v/c Ratio | | 0.93 | | | 0.34 | | | 0.61 | | | 0.91 | |
| Uniform Delay, d1 | | 13.5 | | | 8.4 | | | 17.1 | | | 19.7 | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | 15.0 | | | 0.1 | | | 1.9 | | | 21.6 | |
| Delay (s) | | 28.5 | | | 8.5 | | | 19.0 | | | 41.3 | |
| Level of Service | | C | | | A | | | B | | | D | |
| Approach Delay (s) | | 28.5 | | | 8.5 | | | 19.0 | | | 41.3 | |
| Approach LOS | | C | | | A | | | B | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 24.1 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.92 | | |
| Actuated Cycle Length (s) | 62.4 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 100.4% | ICU Level of Service | G |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat Pipeline (Berkeley) No Project PM Peak

5: Alcatraz Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 45 | 193 | 156 | 18 | 93 | 15 | 128 | 256 | 25 | 14 | 331 | 67 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Flt Protected | 0.95 | | | | 0.98 | | | 0.99 | | | 0.98 | |
| Flt Permitted | 0.99 | | | | 0.99 | | | 0.98 | | | 1.00 | |
| Satd. Flow (prot) | 1753 | | | | 1820 | | | 1819 | | | 1819 | |
| Flt Permitted | 1680 | | | | 1699 | | | 1441 | | | 1788 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 49 | 210 | 170 | 20 | 101 | 16 | 139 | 278 | 27 | 15 | 360 | 73 |
| RTOR Reduction (vph) | 0 | 53 | 0 | 0 | 11 | 0 | 0 | 6 | 0 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 0 | 376 | 0 | 0 | 126 | 0 | 0 | 438 | 0 | 0 | 432 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 12.3 | | | 12.3 | | | 15.5 | | | 15.5 | | |
| Effective Green, g (s) | 12.3 | | | 12.3 | | | 15.5 | | | 15.5 | | |
| Actuated g/C Ratio | 0.34 | | | 0.34 | | | 0.43 | | | 0.43 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 577 | | | 584 | | | 624 | | | 774 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.22 | | | 0.07 | | | c0.30 | | | 0.24 | | |
| v/c Ratio | 0.65 | | | 0.22 | | | 0.70 | | | 0.56 | | |
| Uniform Delay, d1 | 9.9 | | | 8.3 | | | 8.3 | | | 7.6 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 2.6 | | | 0.2 | | | 3.6 | | | 0.9 | | |
| Delay (s) | 12.6 | | | 8.5 | | | 11.9 | | | 8.5 | | |
| Level of Service | B | | | A | | | B | | | A | | |
| Approach Delay (s) | 12.6 | | | 8.5 | | | 11.9 | | | 8.5 | | |
| Approach LOS | B | | | A | | | B | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 10.7 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.68 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 35.8 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 82.2% | | | ICU Level of Service | | | E | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) No Project PM Peak

6: The Uplands & Claremont Ave

6/7/2012



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 61 | 69 | 680 | 142 | 36 | 375 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | | | 4.0 |
| Lane Util. Factor | 1.00 | | 0.95 | | | 0.95 |
| Frpb, ped/bikes | 0.98 | | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.93 | | 0.97 | | | 1.00 |
| Fl _t Protected | 0.98 | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 1652 | | 3429 | | | 3524 |
| Fl _t Permitted | 0.98 | | 1.00 | | | 0.86 |
| Satd. Flow (perm) | 1652 | | 3429 | | | 3047 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 66 | 75 | 739 | 154 | 39 | 408 |
| RTOR Reduction (vph) | 64 | 0 | 34 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 77 | 0 | 859 | 0 | 0 | 447 |
| Confl. Peds. (#/hr) | 23 | 64 | | 14 | | |
| Confl. Bikes (#/hr) | | | | 2 | | |
| Turn Type | | | | | Perm | |
| Protected Phases | 8 | | 2 | | 6 | |
| Permitted Phases | | | | | 6 | |
| Actuated Green, G (s) | 3.6 | | 13.4 | | 13.4 | |
| Effective Green, g (s) | 3.6 | | 13.4 | | 13.4 | |
| Actuated g/C Ratio | 0.14 | | 0.54 | | 0.54 | |
| Clearance Time (s) | 4.0 | | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 238 | | 1838 | | 1633 | |
| v/s Ratio Prot | c0.05 | | c0.25 | | | |
| v/s Ratio Perm | | | | | 0.15 | |
| v/c Ratio | 0.32 | | 0.47 | | 0.27 | |
| Uniform Delay, d1 | 9.6 | | 3.6 | | 3.2 | |
| Progression Factor | 1.00 | | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.8 | | 0.2 | | 0.1 | |
| Delay (s) | 10.4 | | 3.8 | | 3.2 | |
| Level of Service | B | | A | | A | |
| Approach Delay (s) | 10.4 | | 3.8 | | 3.2 | |
| Approach LOS | B | | A | | A | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 4.2 | | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | 0.44 | | | | |
| Actuated Cycle Length (s) | | 25.0 | | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | 57.8% | | ICU Level of Service | | B |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

2016 Wildcat Pipeline (Berkeley) No Project PM Peak

7: Brookside Dr & Claremont Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 0 | 0 | 0 | 12 | 0 | 8 | 3 | 764 | 21 | 12 | 399 | 1 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 0 | 0 | 13 | 0 | 9 | 3 | 830 | 23 | 13 | 434 | 1 |
| Pedestrians | | 54 | | | 23 | | | 4 | | | 1 | |
| Lane Width (ft) | | 12.0 | | | 12.0 | | | 12.0 | | | 12.0 | |
| Walking Speed (ft/s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Percent Blockage | | 4 | | | 2 | | | 0 | | | 0 | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | 460 | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 946 | 1397 | 275 | 1118 | 1386 | 451 | 489 | | | 876 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 946 | 1397 | 275 | 1118 | 1386 | 451 | 489 | | | 876 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 100 | 100 | 100 | 91 | 100 | 98 | 100 | | | 98 | | |
| cM capacity (veh/h) | 190 | 128 | 687 | 148 | 130 | 545 | 1022 | | | 752 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total | 0 | 22 | 418 | 438 | 230 | 218 | | | | | | |
| Volume Left | 0 | 13 | 3 | 0 | 13 | 0 | | | | | | |
| Volume Right | 0 | 9 | 0 | 23 | 0 | 1 | | | | | | |
| cSH | 1700 | 209 | 1022 | 1700 | 752 | 1700 | | | | | | |
| Volume to Capacity | 0.00 | 0.10 | 0.00 | 0.26 | 0.02 | 0.13 | | | | | | |
| Queue Length 95th (ft) | 0 | 9 | 0 | 0 | 1 | 0 | | | | | | |
| Control Delay (s) | 0.0 | 24.2 | 0.1 | 0.0 | 0.7 | 0.0 | | | | | | |
| Lane LOS | A | C | A | | A | | | | | | | |
| Approach Delay (s) | 0.0 | 24.2 | 0.0 | | 0.4 | | | | | | | |
| Approach LOS | A | C | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 0.6 | | | | | | | | | |
| Intersection Capacity Utilization | | 34.3% | | ICU Level of Service | | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

1: Derby St & Telegraph Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|-------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 7 | 30 | 27 | 220 | 34 | 19 | 17 | 641 | 140 | 34 | 454 | 3 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | | | | | | | | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |
| Fr _t | | | | | | | | 0.94 | 0.99 | 1.00 | 0.85 | 1.00 |
| Flt Protected | | | | | | | | 0.99 | 0.96 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | | | | | | | | 1749 | 1774 | 3535 | 1583 | 3527 |
| Flt Permitted | | | | | | | | 0.95 | 0.72 | 0.94 | 1.00 | 0.89 |
| Satd. Flow (perm) | | | | | | | | 1665 | 1329 | 3321 | 1583 | 3140 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 8 | 33 | 29 | 239 | 37 | 21 | 18 | 697 | 152 | 37 | 493 | 3 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 0 | 8 | 0 | 0 | 0 | 84 | 0 | 0 | 2 |
| Lane Group Flow (vph) | 0 | 50 | 0 | 0 | 289 | 0 | 0 | 715 | 68 | 0 | 530 | 1 |
| Turn Type | Perm | | | Perm | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 9.2 | | | 9.2 | | | 13.9 | 13.9 | | 13.9 | 13.9 |
| Effective Green, g (s) | | 9.2 | | | 9.2 | | | 13.9 | 13.9 | | 13.9 | 13.9 |
| Actuated g/C Ratio | | 0.30 | | | 0.30 | | | 0.45 | 0.45 | | 0.45 | 0.45 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 493 | | | 393 | | | 1484 | 708 | | 1403 | 708 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | 0.03 | | | c0.22 | | | c0.22 | 0.04 | | 0.17 | 0.00 |
| v/c Ratio | | 0.10 | | | 0.74 | | | 0.48 | 0.10 | | 0.38 | 0.00 |
| Uniform Delay, d1 | | 7.9 | | | 9.9 | | | 6.1 | 5.0 | | 5.7 | 4.8 |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | | | 7.0 | | | 0.2 | 0.1 | | 0.2 | 0.0 |
| Delay (s) | | 8.0 | | | 16.9 | | | 6.3 | 5.0 | | 5.9 | 4.8 |
| Level of Service | | A | | | B | | | A | A | | A | A |
| Approach Delay (s) | | 8.0 | | | 16.9 | | | 6.1 | | | 5.9 | |
| Approach LOS | | A | | | B | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 7.9 | HCM Level of Service | A |
| HCM Volume to Capacity ratio | 0.58 | | |
| Actuated Cycle Length (s) | 31.1 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 63.5% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|------|----------------------|-------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 0 | 101 | 0 | 0 | 200 | 0 | 728 | 17 | 0 | 543 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | | | 0.95 | | | 0.95 | | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr _t | | | 0.86 | | | 0.86 | | | 1.00 | | | 0.99 |
| Fl _t Protected | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | | | 1524 | | | 1528 | | | 1851 | | | 1846 |
| Fl _t Permitted | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Satd. Flow (perm) | | | 1524 | | | 1528 | | | 1851 | | | 1846 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 0 | 110 | 0 | 0 | 217 | 0 | 791 | 18 | 0 | 590 | 29 |
| RTOR Reduction (vph) | 0 | 84 | 0 | 0 | 31 | 0 | 0 | 1 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 0 | 26 | 0 | 0 | 186 | 0 | 0 | 808 | 0 | 0 | 616 | 0 |
| Confl. Peds. (#/hr) | 62 | | 22 | 22 | | 62 | 40 | | 94 | 94 | | 40 |
| Confl. Bikes (#/hr) | | | 8 | | | 3 | | | 44 | | | 5 |
| Turn Type | Perm | | Perm | | | | | | | | | |
| Protected Phases | | 4 | | | | 8 | | | 2 | | | 6 |
| Permitted Phases | 4 | | | | 8 | | | | | | | |
| Actuated Green, G (s) | | 7.5 | | | 7.5 | | | 16.8 | | | 16.8 | |
| Effective Green, g (s) | | 7.5 | | | 7.5 | | | 16.8 | | | 16.8 | |
| Actuated g/C Ratio | | 0.23 | | | 0.23 | | | 0.52 | | | 0.52 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 354 | | 355 | | | 963 | | | 960 | | | |
| v/s Ratio Prot | 0.02 | | c0.12 | | | c0.44 | | | 0.33 | | | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | | 0.07 | | | 0.52 | | | 0.84 | | | 0.64 | |
| Uniform Delay, d1 | | 9.7 | | | 10.8 | | | 6.6 | | | 5.6 | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | 0.1 | | | 1.4 | | | 6.5 | | | 1.5 | |
| Delay (s) | | 9.8 | | | 12.2 | | | 13.1 | | | 7.1 | |
| Level of Service | | A | | | B | | | B | | | A | |
| Approach Delay (s) | | 9.8 | | | 12.2 | | | 13.1 | | | 7.1 | |
| Approach LOS | | A | | | B | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 10.6 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.74 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 32.3 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 63.1% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak
 3: Derby St & College Ave

6/7/2012



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------|----------------------|-------|------|------|------|
| Lane Configurations | | | | | | |
| Sign Control | Stop | | | Stop | Stop | |
| Volume (vph) | 21 | 172 | 246 | 359 | 232 | 33 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 23 | 187 | 267 | 390 | 252 | 36 |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total (vph) | 210 | 658 | 288 | | | |
| Volume Left (vph) | 23 | 267 | 0 | | | |
| Volume Right (vph) | 187 | 0 | 36 | | | |
| Hadj (s) | -0.48 | 0.12 | -0.04 | | | |
| Departure Headway (s) | 5.8 | 5.1 | 5.4 | | | |
| Degree Utilization, x | 0.34 | 0.93 | 0.43 | | | |
| Capacity (veh/h) | 596 | 695 | 646 | | | |
| Control Delay (s) | 11.7 | 41.1 | 12.5 | | | |
| Approach Delay (s) | 11.7 | 41.1 | 12.5 | | | |
| Approach LOS | B | E | B | | | |
| Intersection Summary | | | | | | |
| Delay | 28.6 | | | | | |
| HCM Level of Service | D | | | | | |
| Intersection Capacity Utilization | 72.0% | ICU Level of Service | | | C | |
| Analysis Period (min) | 15 | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

4: Ashby Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 6 | 415 | 130 | 6 | 625 | 156 | 137 | 316 | 22 | 69 | 173 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 0.95 | | | | 1.00 | | | 1.00 |
| Flt Protected | 0.97 | | | | 0.97 | | | | 0.99 | | | 0.97 |
| Flt Permitted | 1.00 | | | | 1.00 | | | | 0.99 | | | 0.99 |
| Satd. Flow (prot) | 1802 | | | | 3432 | | | | 1825 | | | 1794 |
| Flt Permitted | 0.99 | | | | 0.95 | | | | 0.82 | | | 0.84 |
| Satd. Flow (perm) | 1783 | | | | 3263 | | | | 1527 | | | 1531 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 7 | 451 | 141 | 7 | 679 | 170 | 149 | 343 | 24 | 75 | 188 | 62 |
| RTOR Reduction (vph) | 0 | 28 | 0 | 0 | 55 | 0 | 0 | 4 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 0 | 571 | 0 | 0 | 801 | 0 | 0 | 512 | 0 | 0 | 304 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 14.8 | | | 14.8 | | | 15.0 | | | 15.0 | | |
| Effective Green, g (s) | 14.8 | | | 14.8 | | | 15.0 | | | 15.0 | | |
| Actuated g/C Ratio | 0.39 | | | 0.39 | | | 0.40 | | | 0.40 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 698 | | | 1278 | | | 606 | | | 608 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.32 | | | 0.25 | | | c0.34 | | | 0.20 | | |
| v/c Ratio | 0.82 | | | 0.63 | | | 0.84 | | | 0.50 | | |
| Uniform Delay, d1 | 10.3 | | | 9.3 | | | 10.3 | | | 8.6 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 7.4 | | | 1.0 | | | 10.4 | | | 0.6 | | |
| Delay (s) | 17.7 | | | 10.2 | | | 20.8 | | | 9.2 | | |
| Level of Service | B | | | B | | | C | | | A | | |
| Approach Delay (s) | 17.7 | | | 10.2 | | | 20.8 | | | 9.2 | | |
| Approach LOS | B | | | B | | | C | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 14.4 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.83 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 37.8 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 78.5% | | | ICU Level of Service | | | D | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

5: Alcatraz Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 43 | 136 | 140 | 12 | 125 | 71 | 131 | 310 | 18 | 67 | 213 | 51 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | | 0.94 | | | | 0.95 | | | 0.99 | | | 0.98 |
| Flt Protected | | 0.99 | | | | 1.00 | | | 0.99 | | | 0.99 |
| Satd. Flow (prot) | | 1741 | | | | 1772 | | | 1827 | | | 1806 |
| Flt Permitted | | 0.93 | | | | 0.97 | | | 0.83 | | | 0.86 |
| Satd. Flow (perm) | | 1629 | | | | 1723 | | | 1530 | | | 1566 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 47 | 148 | 152 | 13 | 136 | 77 | 142 | 337 | 20 | 73 | 232 | 55 |
| RTOR Reduction (vph) | 0 | 66 | 0 | 0 | 44 | 0 | 0 | 3 | 0 | 0 | 15 | 0 |
| Lane Group Flow (vph) | 0 | 281 | 0 | 0 | 182 | 0 | 0 | 496 | 0 | 0 | 345 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | | 11.0 | | | 11.0 | | | 15.9 | | | 15.9 | |
| Effective Green, g (s) | | 11.0 | | | 11.0 | | | 15.9 | | | 15.9 | |
| Actuated g/C Ratio | | 0.32 | | | 0.32 | | | 0.46 | | | 0.46 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | | 513 | | | 543 | | | 697 | | | 713 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | c0.17 | | | 0.11 | | | c0.32 | | | 0.22 | |
| v/c Ratio | | 0.55 | | | 0.34 | | | 0.71 | | | 0.48 | |
| Uniform Delay, d1 | | 9.9 | | | 9.2 | | | 7.7 | | | 6.6 | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | 1.2 | | | 0.4 | | | 3.4 | | | 0.5 | |
| Delay (s) | | 11.1 | | | 9.5 | | | 11.1 | | | 7.2 | |
| Level of Service | | B | | | A | | | B | | | A | |
| Approach Delay (s) | | 11.1 | | | 9.5 | | | 11.1 | | | 7.2 | |
| Approach LOS | | B | | | A | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 9.8 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.64 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 34.9 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 75.5% | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

6: The Uplands & Claremont Ave

6/7/2012



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 0 | 163 | 411 | 54 | 0 | 401 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | | | 4.0 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 0.95 |
| Frpb, ped/bikes | 0.95 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.86 | | 0.98 | | | 1.00 |
| Fl _t Protected | 1.00 | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 1532 | | 1826 | | | 3539 |
| Fl _t Permitted | 1.00 | | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 1532 | | 1826 | | | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 177 | 447 | 59 | 0 | 436 |
| RTOR Reduction (vph) | 151 | 0 | 11 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 26 | 0 | 495 | 0 | 0 | 436 |
| Confl. Peds. (#/hr) | 52 | 46 | | 19 | 19 | |
| Confl. Bikes (#/hr) | | | | | | 5 |
| Turn Type | | | | | Perm | |
| Protected Phases | 8 | | 2 | | 6 | |
| Permitted Phases | | | | | 6 | |
| Actuated Green, G (s) | 3.0 | | 9.8 | | 9.8 | |
| Effective Green, g (s) | 3.0 | | 9.8 | | 9.8 | |
| Actuated g/C Ratio | 0.14 | | 0.47 | | 0.47 | |
| Clearance Time (s) | 4.0 | | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 221 | | 860 | | 1667 | |
| v/s Ratio Prot | c0.02 | | c0.27 | | 0.12 | |
| v/s Ratio Perm | | | | | | |
| v/c Ratio | 0.12 | | 0.58 | | 0.26 | |
| Uniform Delay, d1 | 7.7 | | 4.0 | | 3.3 | |
| Progression Factor | 1.00 | | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.2 | | 0.9 | | 0.1 | |
| Delay (s) | 8.0 | | 4.9 | | 3.4 | |
| Level of Service | A | | A | | A | |
| Approach Delay (s) | 8.0 | | 4.9 | | 3.4 | |
| Approach LOS | A | | A | | A | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 4.8 | | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | 0.47 | | | | |
| Actuated Cycle Length (s) | | 20.8 | | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | 45.6% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

7: Brookside Dr & Claremont Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 1 | 0 | 0 | 42 | 0 | 40 | 1 | 463 | 77 | 73 | 436 | 1 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 1 | 0 | 0 | 46 | 0 | 43 | 1 | 503 | 84 | 79 | 474 | 1 |
| Pedestrians | | 27 | | | 16 | | | 2 | | | 1 | |
| Lane Width (ft) | | 12.0 | | | 12.0 | | | 12.0 | | | 12.0 | |
| Walking Speed (ft/s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Percent Blockage | | 2 | | | 1 | | | 0 | | | 0 | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | 460 | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 958 | 1265 | 266 | 961 | 1224 | 310 | 502 | | | 603 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 958 | 1265 | 266 | 961 | 1224 | 310 | 502 | | | 603 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 99 | 100 | 100 | 76 | 100 | 94 | 100 | | | 92 | | |
| cM capacity (veh/h) | 176 | 148 | 714 | 189 | 157 | 676 | 1035 | | | 958 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total | 1 | 89 | 253 | 335 | 316 | 238 | | | | | | |
| Volume Left | 1 | 46 | 1 | 0 | 79 | 0 | | | | | | |
| Volume Right | 0 | 43 | 0 | 84 | 0 | 1 | | | | | | |
| cSH | 176 | 292 | 1035 | 1700 | 958 | 1700 | | | | | | |
| Volume to Capacity | 0.01 | 0.31 | 0.00 | 0.20 | 0.08 | 0.14 | | | | | | |
| Queue Length 95th (ft) | 0 | 31 | 0 | 0 | 7 | 0 | | | | | | |
| Control Delay (s) | 25.6 | 22.7 | 0.0 | 0.0 | 2.9 | 0.0 | | | | | | |
| Lane LOS | D | C | A | | A | | | | | | | |
| Approach Delay (s) | 25.6 | 22.7 | 0.0 | | 1.7 | | | | | | | |
| Approach LOS | D | C | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 2.4 | | | | | | | | | |
| Intersection Capacity Utilization | | 44.3% | | ICU Level of Service | | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project AM Peak

7: Brookside Dr & Claremont Ave with Flagger

10/2/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 1 | 0 | 0 | 42 | 0 | 40 | 1 | 463 | 77 | 73 | 436 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | 1.00 | | | | | 0.99 | | 0.99 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | | | | | 0.93 | | 0.98 | | | 1.00 | |
| Fl _t Protected | 0.95 | | | | | 0.97 | | 1.00 | | | 0.99 | |
| Satd. Flow (prot) | 1768 | | | | | 1679 | | 3444 | | | 3509 | |
| Fl _t Permitted | 1.00 | | | | | 1.00 | | 0.95 | | | 0.84 | |
| Satd. Flow (perm) | 1861 | | | | | 1723 | | 3287 | | | 2964 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1 | 0 | 0 | 46 | 0 | 43 | 1 | 503 | 84 | 79 | 474 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 39 | 0 | 0 | 19 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1 | 0 | 0 | 50 | 0 | 0 | 569 | 0 | 0 | 554 | 0 |
| Confl. Peds. (#/hr) | 1 | | 2 | 2 | | 1 | 27 | | 16 | 16 | | 27 |
| Confl. Bikes (#/hr) | | | | | | | | | 6 | | | 14 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 2.8 | | | 2.8 | | | 21.3 | | | 21.3 | | |
| Effective Green, g (s) | 2.8 | | | 2.8 | | | 21.3 | | | 21.3 | | |
| Actuated g/C Ratio | 0.09 | | | 0.09 | | | 0.66 | | | 0.66 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 162 | | | 150 | | | 2181 | | | 1967 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.00 | | | c0.03 | | | 0.17 | | | c0.19 | | |
| v/c Ratio | 0.01 | | | 0.33 | | | 0.26 | | | 0.28 | | |
| Uniform Delay, d1 | 13.4 | | | 13.8 | | | 2.2 | | | 2.2 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 0.0 | | | 1.3 | | | 0.1 | | | 0.1 | | |
| Delay (s) | 13.4 | | | 15.1 | | | 2.3 | | | 2.3 | | |
| Level of Service | B | | | B | | | A | | | A | | |
| Approach Delay (s) | 13.4 | | | 15.1 | | | 2.3 | | | 2.3 | | |
| Approach LOS | B | | | B | | | A | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 3.2 | | | HCM Level of Service | | | A | | | | | |
| HCM Volume to Capacity ratio | 0.29 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 32.1 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 44.3% | | | ICU Level of Service | | | A | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak

1: Derby St & Telegraph Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|-------|------|------|------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 16 | 61 | 29 | 216 | 74 | 20 | 29 | 531 | 169 | 56 | 791 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | | | | | | | | 1.00 | 1.00 | | 0.95 | 1.00 |
| Fr _t | | | | | | | | 0.96 | 0.99 | | 1.00 | 0.85 |
| Flt Protected | | | | | | | | 0.99 | 0.97 | | 1.00 | 1.00 |
| Satd. Flow (prot) | | | | | | | | 1780 | 1784 | | 3530 | 1583 |
| Flt Permitted | | | | | | | | 0.93 | 0.72 | | 0.89 | 1.00 |
| Satd. Flow (perm) | | | | | | | | 1670 | 1332 | | 3139 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 17 | 66 | 32 | 235 | 80 | 22 | 32 | 577 | 184 | 61 | 860 | 18 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 0 | 6 | 0 | 0 | 0 | 108 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 0 | 95 | 0 | 0 | 331 | 0 | 0 | 609 | 76 | 0 | 921 | 8 |
| Turn Type | Perm | | | Perm | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 12.9 | | | 12.9 | | | 14.7 | 14.7 | | 14.7 | 14.7 |
| Effective Green, g (s) | | 12.9 | | | 12.9 | | | 14.7 | 14.7 | | 14.7 | 14.7 |
| Actuated g/C Ratio | | 0.36 | | | 0.36 | | | 0.41 | 0.41 | | 0.41 | 0.41 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 605 | | | 483 | | | 1296 | 654 | | 1293 | 654 |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | 0.06 | | | c0.25 | | | 0.19 | 0.05 | | c0.29 | 0.01 |
| v/c Ratio | | 0.16 | | | 0.68 | | | 0.47 | 0.12 | | 0.71 | 0.01 |
| Uniform Delay, d1 | | 7.7 | | | 9.6 | | | 7.6 | 6.4 | | 8.7 | 6.2 |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | | | 4.0 | | | 0.3 | 0.1 | | 1.9 | 0.0 |
| Delay (s) | | 7.8 | | | 13.6 | | | 7.9 | 6.5 | | 10.6 | 6.2 |
| Level of Service | | A | | | B | | | A | A | | B | A |
| Approach Delay (s) | | 7.8 | | | 13.6 | | | 7.6 | | | 10.5 | |
| Approach LOS | | A | | | B | | | A | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 9.8 | HCM Level of Service | A |
| HCM Volume to Capacity ratio | 0.70 | | |
| Actuated Cycle Length (s) | 35.6 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 72.7% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak

2: Stuart St & Telegraph Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 0 | 100 | 0 | 0 | 115 | 0 | 679 | 40 | 0 | 875 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | | | 0.95 | | | 0.97 | | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr | | | 0.86 | | | 0.86 | | | 0.99 | | | 1.00 |
| Flt Protected | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | | | 1534 | | | 1557 | | | 1842 | | | 1852 |
| Flt Permitted | | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 |
| Satd. Flow (perm) | | | 1534 | | | 1557 | | | 1842 | | | 1852 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 0 | 109 | 0 | 0 | 125 | 0 | 738 | 43 | 0 | 951 | 27 |
| RTOR Reduction (vph) | 0 | 24 | 0 | 0 | 57 | 0 | 0 | 4 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 85 | 0 | 0 | 68 | 0 | 0 | 777 | 0 | 0 | 976 | 0 |
| Confl. Peds. (#/hr) | 26 | | 14 | 14 | | 26 | 64 | | 48 | 48 | | 64 |
| Confl. Bikes (#/hr) | | | 6 | | | 5 | | | 15 | | | 5 |
| Turn Type | Perm | | | Perm | | | | | | | | |
| Protected Phases | | 4 | | | | 8 | | | 2 | | | 6 |
| Permitted Phases | 4 | | | | 8 | | | | | | | |
| Actuated Green, G (s) | | 4.2 | | | | 4.2 | | | 16.9 | | | 16.9 |
| Effective Green, g (s) | | 4.2 | | | | 4.2 | | | 16.9 | | | 16.9 |
| Actuated g/C Ratio | | 0.14 | | | | 0.14 | | | 0.58 | | | 0.58 |
| Clearance Time (s) | | 4.0 | | | | 4.0 | | | 4.0 | | | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | | 3.0 | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 221 | | | 225 | | | 1070 | | | 1076 | | |
| v/s Ratio Prot | c0.06 | | | 0.04 | | | 0.42 | | | c0.53 | | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | | 0.38 | | | | 0.30 | | | 0.73 | | | 0.91 |
| Uniform Delay, d1 | 11.3 | | | 11.1 | | | 4.4 | | | 5.4 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 1.1 | | | 0.8 | | | 2.5 | | | 10.9 | | |
| Delay (s) | 12.4 | | | 11.9 | | | 6.9 | | | 16.3 | | |
| Level of Service | B | | | B | | | A | | | B | | |
| Approach Delay (s) | 12.4 | | | 11.9 | | | 6.9 | | | 16.3 | | |
| Approach LOS | B | | | B | | | A | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 12.1 | | | HCM Level of Service | | | | | | B | | |
| HCM Volume to Capacity ratio | 0.80 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 29.1 | | | Sum of lost time (s) | | | | | | 8.0 | | |
| Intersection Capacity Utilization | 66.1% | | | ICU Level of Service | | | | | | C | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak
 3: Derby St & College Ave

6/7/2012



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------|----------------------|-------|------|------|------|
| Lane Configurations | | | | | | |
| Sign Control | Stop | | Stop | Stop | | |
| Volume (vph) | 36 | 210 | 192 | 271 | 394 | 55 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 39 | 228 | 209 | 295 | 428 | 60 |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total (vph) | 267 | 503 | 488 | | | |
| Volume Left (vph) | 39 | 209 | 0 | | | |
| Volume Right (vph) | 228 | 0 | 60 | | | |
| Hadj (s) | -0.45 | 0.12 | -0.04 | | | |
| Departure Headway (s) | 6.0 | 5.6 | 5.5 | | | |
| Degree Utilization, x | 0.45 | 0.79 | 0.75 | | | |
| Capacity (veh/h) | 541 | 624 | 630 | | | |
| Control Delay (s) | 13.7 | 26.4 | 23.1 | | | |
| Approach Delay (s) | 13.7 | 26.4 | 23.1 | | | |
| Approach LOS | B | D | C | | | |
| Intersection Summary | | | | | | |
| Delay | 22.4 | | | | | |
| HCM Level of Service | C | | | | | |
| Intersection Capacity Utilization | 78.2% | ICU Level of Service | | | D | |
| Analysis Period (min) | 15 | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak

4: Ashby Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 14 | 739 | 234 | 8 | 463 | 105 | 125 | 230 | 44 | 108 | 240 | 60 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | | | | | | | | | | | | |
| Flt Protected | | | | | | | | | | | | |
| Satd. Flow (prot) | | | | | | | | | | | | |
| Flt Permitted | | | | | | | | | | | | |
| Satd. Flow (perm) | | | | | | | | | | | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 15 | 803 | 254 | 9 | 503 | 114 | 136 | 250 | 48 | 117 | 261 | 65 |
| RTOR Reduction (vph) | 0 | 17 | 0 | 0 | 30 | 0 | 0 | 7 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 1055 | 0 | 0 | 596 | 0 | 0 | 427 | 0 | 0 | 434 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | | 35.0 | | | 35.0 | | | 22.0 | | | 22.0 | |
| Effective Green, g (s) | | 35.0 | | | 35.0 | | | 22.0 | | | 22.0 | |
| Actuated g/C Ratio | | 0.54 | | | 0.54 | | | 0.34 | | | 0.34 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | | 961 | | | 1745 | | | 423 | | | 464 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | c0.59 | | | 0.18 | | | c0.34 | | | 0.32 | |
| v/c Ratio | | 1.10 | | | 0.34 | | | 1.01 | | | 0.93 | |
| Uniform Delay, d1 | | 15.0 | | | 8.5 | | | 21.5 | | | 20.8 | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | 59.5 | | | 0.1 | | | 46.4 | | | 26.1 | |
| Delay (s) | | 74.5 | | | 8.6 | | | 67.9 | | | 46.9 | |
| Level of Service | | E | | | A | | | E | | | D | |
| Approach Delay (s) | | 74.5 | | | 8.6 | | | 67.9 | | | 46.9 | |
| Approach LOS | | E | | | A | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 52.6 | | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | 1.06 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 65.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 102.2% | | | ICU Level of Service | | | G | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak

5: Alcatraz Ave & College Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 45 | 193 | 156 | 18 | 93 | 95 | 128 | 256 | 25 | 167 | 331 | 67 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Flt Protected | 0.95 | | | | 0.94 | | | 0.99 | | | 0.98 | |
| Flt Permitted | 0.99 | | | | 1.00 | | | 0.98 | | | 0.99 | |
| Satd. Flow (prot) | 1753 | | | | 1739 | | | 1819 | | | 1806 | |
| Flt Permitted | 0.94 | | | | 0.96 | | | 0.74 | | | 0.78 | |
| Satd. Flow (perm) | 1659 | | | | 1675 | | | 1361 | | | 1428 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 49 | 210 | 170 | 20 | 101 | 103 | 139 | 278 | 27 | 182 | 360 | 73 |
| RTOR Reduction (vph) | 0 | 55 | 0 | 0 | 70 | 0 | 0 | 5 | 0 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 0 | 374 | 0 | 0 | 154 | 0 | 0 | 439 | 0 | 0 | 605 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 13.0 | | | 13.0 | | | 20.0 | | | 20.0 | | |
| Effective Green, g (s) | 13.0 | | | 13.0 | | | 20.0 | | | 20.0 | | |
| Actuated g/C Ratio | 0.32 | | | 0.32 | | | 0.49 | | | 0.49 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 526 | | | 531 | | | 664 | | | 697 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.23 | | | 0.09 | | | 0.32 | | | 0.42 | | |
| v/c Ratio | 0.71 | | | 0.29 | | | 0.66 | | | 0.87 | | |
| Uniform Delay, d1 | 12.3 | | | 10.5 | | | 7.9 | | | 9.3 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 4.5 | | | 0.3 | | | 2.5 | | | 11.1 | | |
| Delay (s) | 16.8 | | | 10.8 | | | 10.4 | | | 20.4 | | |
| Level of Service | B | | | B | | | B | | | C | | |
| Approach Delay (s) | 16.8 | | | 10.8 | | | 10.4 | | | 20.4 | | |
| Approach LOS | B | | | B | | | B | | | C | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 15.7 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.81 | | |
| Actuated Cycle Length (s) | 41.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 78.0% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 0 | 130 | 680 | 142 | 0 | 411 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | | | 4.0 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 0.95 |
| Frpb, ped/bikes | 0.92 | | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.86 | | 0.98 | | | 1.00 |
| Fl _t Protected | 1.00 | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 1487 | | 1809 | | | 3539 |
| Fl _t Permitted | 1.00 | | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 1487 | | 1809 | | | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 141 | 739 | 154 | 0 | 447 |
| RTOR Reduction (vph) | 73 | 0 | 13 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 68 | 0 | 880 | 0 | 0 | 447 |
| Confl. Peds. (#/hr) | 23 | 64 | | 14 | | |
| Confl. Bikes (#/hr) | | | | 2 | | |
| Turn Type | | | | | Perm | |
| Protected Phases | 8 | | 2 | | 6 | |
| Permitted Phases | | | | | 6 | |
| Actuated Green, G (s) | 4.1 | | 16.9 | | 16.9 | |
| Effective Green, g (s) | 4.1 | | 16.9 | | 16.9 | |
| Actuated g/C Ratio | 0.14 | | 0.58 | | 0.58 | |
| Clearance Time (s) | 4.0 | | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 210 | | 1054 | | 2062 | |
| v/s Ratio Prot | c0.05 | | c0.49 | | 0.13 | |
| v/s Ratio Perm | | | | | | |
| v/c Ratio | 0.32 | | 0.83 | | 0.22 | |
| Uniform Delay, d1 | 11.2 | | 4.9 | | 2.9 | |
| Progression Factor | 1.00 | | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 0.9 | | 5.8 | | 0.1 | |
| Delay (s) | 12.1 | | 10.7 | | 2.9 | |
| Level of Service | B | | B | | A | |
| Approach Delay (s) | 12.1 | | 10.7 | | 2.9 | |
| Approach LOS | B | | B | | A | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 8.5 | | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | 0.73 | | | | |
| Actuated Cycle Length (s) | | 29.0 | | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | 64.6% | | ICU Level of Service | | C |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak

7: Brookside Dr & Claremont Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 0 | 0 | 0 | 83 | 0 | 78 | 3 | 764 | 71 | 62 | 399 | 1 |
| Sign Control | | Stop | | | | Stop | | | Free | | | Free |
| Grade | | 0% | | | | 0% | | | 0% | | | 0% |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 0 | 0 | 90 | 0 | 85 | 3 | 830 | 77 | 67 | 434 | 1 |
| Pedestrians | | 54 | | | | 23 | | | 4 | | | 1 |
| Lane Width (ft) | | 12.0 | | | | 12.0 | | | 12.0 | | | 12.0 |
| Walking Speed (ft/s) | | 4.0 | | | | 4.0 | | | 4.0 | | | 4.0 |
| Percent Blockage | | 4 | | | | 2 | | | 0 | | | 0 |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | 460 | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 1131 | 1560 | 275 | 1254 | 1522 | 478 | 489 | | | | 931 | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 1131 | 1560 | 275 | 1254 | 1522 | 478 | 489 | | | | 931 | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | | 4.1 | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | | 2.2 | |
| p0 queue free % | 100 | 100 | 100 | 18 | 100 | 84 | 100 | | | | 91 | |
| cM capacity (veh/h) | 112 | 94 | 687 | 111 | 99 | 523 | 1022 | | | | 717 | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total | 0 | 175 | 418 | 492 | 284 | 218 | | | | | | |
| Volume Left | 0 | 90 | 3 | 0 | 67 | 0 | | | | | | |
| Volume Right | 0 | 85 | 0 | 77 | 0 | 1 | | | | | | |
| cSH | 1700 | 179 | 1022 | 1700 | 717 | 1700 | | | | | | |
| Volume to Capacity | 0.00 | 0.98 | 0.00 | 0.29 | 0.09 | 0.13 | | | | | | |
| Queue Length 95th (ft) | 0 | 196 | 0 | 0 | 8 | 0 | | | | | | |
| Control Delay (s) | 0.0 | 114.3 | 0.1 | 0.0 | 3.4 | 0.0 | | | | | | |
| Lane LOS | A | F | A | | A | | | | | | | |
| Approach Delay (s) | 0.0 | 114.3 | 0.0 | | 1.9 | | | | | | | |
| Approach LOS | A | F | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 13.2 | | | | | | | | | |
| Intersection Capacity Utilization | | 56.5% | | ICU Level of Service | | | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

2016 Wildcat Pipeline (Berkeley) with Project PM Peak

7: Brookside Dr & Claremont Ave with Flagger

10/2/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 0 | 0 | 83 | 0 | 78 | 3 | 764 | 71 | 62 | 399 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 1.00 | | | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | | 0.99 | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | | 1.00 | | 1.00 | | | 1.00 | |
| Fr _t | | | | | 0.93 | | | 0.99 | | | 1.00 | |
| Flt Protected | | | | | | 0.97 | | 1.00 | | | 0.99 | |
| Satd. Flow (prot) | | | | | | 1676 | | 3477 | | | 3511 | |
| Flt Permitted | | | | | | 0.84 | | 0.95 | | | 0.80 | |
| Satd. Flow (perm) | | | | | | 1440 | | 3317 | | | 2836 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 0 | 0 | 90 | 0 | 85 | 3 | 830 | 77 | 67 | 434 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 47 | 0 | 0 | 12 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 128 | 0 | 0 | 898 | 0 | 0 | 502 | 0 |
| Confl. Peds. (#/hr) | | | | | 4 | | 1 | 54 | | 23 | 23 | 54 |
| Confl. Bikes (#/hr) | | | | | | | 1 | | | 16 | | 16 |
| Turn Type | Perm | | Perm | | | Perm | | Perm | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 8 | | | 2 | | | 6 | | | |
| Actuated Green, G (s) | | | | | 6.9 | | | 20.2 | | | 20.2 | |
| Effective Green, g (s) | | | | | 6.9 | | | 20.2 | | | 20.2 | |
| Actuated g/C Ratio | | | | | 0.20 | | | 0.58 | | | 0.58 | |
| Clearance Time (s) | | | | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | | | | | 283 | | | 1909 | | | 1632 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | | | | | c0.09 | | | c0.27 | | | 0.18 | |
| v/c Ratio | | | | | 0.45 | | | 0.47 | | | 0.31 | |
| Uniform Delay, d1 | | | | | 12.4 | | | 4.3 | | | 3.8 | |
| Progression Factor | | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.2 | | | 0.2 | | | 0.1 | |
| Delay (s) | | | | | 13.6 | | | 4.5 | | | 3.9 | |
| Level of Service | | | | | B | | | A | | | A | |
| Approach Delay (s) | | 0.0 | | | 13.6 | | | 4.5 | | | 3.9 | |
| Approach LOS | | A | | | B | | | A | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 5.3 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.47 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 35.1 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 56.5% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

APPENDIX K

Wildcat Pipeline (El Cerrito) Level of Service Calculations

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2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 1: MacDonald Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|------|------|------|-------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | |
| Volume (vph) | 19 | 548 | 79 | 123 | 294 | 33 | 125 | 43 | 163 | 40 | 69 | 24 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3415 | 1863 | 1554 | 1767 | 1831 | | 1770 | 3539 | 1542 | 1764 | 4860 | |
| Flt Permitted | 0.55 | 1.00 | 1.00 | 0.33 | 1.00 | | 0.69 | 1.00 | 1.00 | 0.72 | 1.00 | |
| Satd. Flow (perm) | 1971 | 1863 | 1554 | 610 | 1831 | | 1277 | 3539 | 1542 | 1346 | 4860 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 21 | 596 | 86 | 134 | 320 | 36 | 136 | 47 | 177 | 43 | 75 | 26 |
| RTOR Reduction (vph) | 0 | 0 | 48 | 0 | 9 | 0 | 0 | 0 | 130 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 21 | 596 | 38 | 134 | 347 | 0 | 136 | 47 | 47 | 43 | 82 | 0 |
| Confl. Peds. (#/hr) | 10 | | 6 | 6 | | 10 | | | 4 | 4 | | |
| Confl. Bikes (#/hr) | | | 7 | | | 2 | | | 2 | | | 2 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 12.2 | 12.2 | 12.2 | 12.2 | 12.2 | | 7.4 | 7.4 | 7.4 | 7.4 | 7.4 | |
| Effective Green, g (s) | 12.2 | 12.2 | 12.2 | 12.2 | 12.2 | | 7.4 | 7.4 | 7.4 | 7.4 | 7.4 | |
| Actuated g/C Ratio | 0.44 | 0.44 | 0.44 | 0.44 | 0.44 | | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 871 | 824 | 687 | 270 | 809 | | 342 | 949 | 413 | 361 | 1303 | |
| v/s Ratio Prot | | c0.32 | | | 0.19 | | | 0.01 | | | 0.02 | |
| v/s Ratio Perm | 0.01 | | 0.02 | 0.22 | | | c0.11 | | 0.03 | 0.03 | | |
| v/c Ratio | 0.02 | 0.72 | 0.06 | 0.50 | 0.43 | | 0.40 | 0.05 | 0.11 | 0.12 | 0.06 | |
| Uniform Delay, d1 | 4.3 | 6.3 | 4.4 | 5.5 | 5.3 | | 8.3 | 7.5 | 7.6 | 7.6 | 7.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 3.2 | 0.0 | 1.4 | 0.4 | | 0.8 | 0.0 | 0.1 | 0.1 | 0.0 | |
| Delay (s) | 4.4 | 9.5 | 4.4 | 6.9 | 5.7 | | 9.0 | 7.5 | 7.8 | 7.8 | 7.5 | |
| Level of Service | A | A | A | A | A | | A | A | A | A | A | |
| Approach Delay (s) | | 8.7 | | | 6.0 | | | 8.2 | | | 7.6 | |
| Approach LOS | | A | | | A | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 7.7 | HCM Level of Service | A |
| HCM Volume to Capacity ratio | 0.60 | | |
| Actuated Cycle Length (s) | 27.6 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 59.2% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 2: Cutting Blvd & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|--------|------|--------|-------|------|------|--------|-------|------|------|-------|------|
| Lane Configurations | 1 | | 2,3 | 1,2 | 1,2 | 1 | 1,2 | 1,2 | | | 1,2 | 1 |
| Volume (vph) | 184 | 0 | 750 | 106 | 239 | 48 | 330 | 402 | 0 | 0 | 476 | 161 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | | | 0.95 | 1.00 |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | 3433 | 5085 | | | 3539 | 1583 |
| Flt Permitted | 0.59 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 1101 | | 2787 | 3433 | 3539 | 1583 | 3526 | 5085 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 200 | 0 | 815 | 115 | 260 | 52 | 359 | 437 | 0 | 0 | 517 | 175 |
| RTOR Reduction (vph) | 0 | 0 | 523 | 0 | 0 | 42 | 0 | 0 | 0 | 0 | 0 | 128 |
| Lane Group Flow (vph) | 200 | 0 | 292 | 115 | 260 | 10 | 359 | 437 | 0 | 0 | 517 | 47 |
| Turn Type | custom | | custom | Perm | | Perm | custom | | | | Perm | |
| Protected Phases | | | | | 3 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4,5 | 3 | | 3 | 5 | | | | 6 | |
| Actuated Green, G (s) | 12.2 | | 19.8 | 10.1 | 10.1 | 10.1 | 4.1 | 21.9 | | | 14.8 | 14.8 |
| Effective Green, g (s) | 12.2 | | 19.8 | 10.1 | 10.1 | 10.1 | 4.1 | 21.9 | | | 14.8 | 14.8 |
| Actuated g/C Ratio | 0.22 | | 0.36 | 0.18 | 0.18 | 0.18 | 0.07 | 0.40 | | | 0.27 | 0.27 |
| Clearance Time (s) | 3.5 | | | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 243 | | 1000 | 628 | 648 | 290 | 262 | 2017 | | | 949 | 424 |
| v/s Ratio Prot | | | | c0.07 | | | 0.09 | | | | c0.15 | |
| v/s Ratio Perm | c0.18 | | 0.10 | 0.03 | | 0.01 | c0.10 | | | | 0.03 | |
| v/c Ratio | 0.82 | | 0.29 | 0.18 | 0.40 | 0.03 | 1.37 | 0.22 | | | 0.54 | 0.11 |
| Uniform Delay, d1 | 20.5 | | 12.7 | 19.1 | 19.9 | 18.5 | 25.6 | 11.0 | | | 17.3 | 15.2 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 19.7 | | 0.2 | 0.1 | 0.4 | 0.0 | 189.0 | 0.1 | | | 0.6 | 0.1 |
| Delay (s) | 40.1 | | 12.8 | 19.2 | 20.3 | 18.6 | 214.6 | 11.0 | | | 18.0 | 15.4 |
| Level of Service | D | | B | B | C | B | F | B | | | B | B |
| Approach Delay (s) | | 18.2 | | | 19.8 | | | 102.8 | | | 17.3 | |
| Approach LOS | | B | | | B | | | F | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 41.2 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.67 | | |
| Actuated Cycle Length (s) | 55.2 | Sum of lost time (s) | 14.0 |
| Intersection Capacity Utilization | 54.4% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|-----------------------------------|-------|------|------|------|------|------|----------------------|------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 15 | 31 | 22 | 2 | 40 | 37 | 4 | 66 | 31 | 7 | 471 | 86 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.98 | 1.00 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1833 | 1583 | | | | | 1778 | 1583 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.24 | 1.00 | | | | | 0.70 | 1.00 | | 0.09 | 1.00 | 1.00 |
| Satd. Flow (perm) | 442 | 1583 | | | | | 1303 | 1583 | | 171 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 16 | 34 | 24 | 2 | 43 | 40 | 4 | 72 | 34 | 8 | 512 | 93 |
| RTOR Reduction (vph) | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 66 | 0 | 0 | 0 | 59 |
| Lane Group Flow (vph) | 0 | 50 | 24 | 0 | 0 | 0 | 87 | 6 | 0 | 42 | 512 | 34 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | pm+pt | pm+pt | | Perm |
| Protected Phases | | 3 | | | | | | 7 | | 5 | 5 | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | 2 |
| Actuated Green, G (s) | 12.3 | 12.3 | | | | | 10.3 | 10.3 | | 51.0 | 43.5 | 43.5 |
| Effective Green, g (s) | 12.3 | 12.3 | | | | | 10.3 | 10.3 | | 51.0 | 43.5 | 43.5 |
| Actuated g/C Ratio | 0.10 | 0.10 | | | | | 0.09 | 0.09 | | 0.43 | 0.37 | 0.37 |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 46 | 164 | | | | | 113 | 137 | | 174 | 1296 | 580 |
| v/s Ratio Prot | | | | | | | | | | 0.02 | 0.14 | |
| v/s Ratio Perm | c0.11 | 0.02 | | | | | c0.07 | 0.00 | | 0.09 | 0.02 | |
| v/c Ratio | 1.09 | 0.15 | | | | | 0.77 | 0.05 | | 0.24 | 0.40 | 0.06 |
| Uniform Delay, d1 | 53.2 | 48.5 | | | | | 53.1 | 49.7 | | 23.2 | 27.9 | 24.4 |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 159.3 | 0.4 | | | | | 26.5 | 0.1 | | 0.7 | 0.2 | 0.0 |
| Delay (s) | 212.5 | 48.9 | | | | | 79.6 | 49.9 | | 24.0 | 28.1 | 24.4 |
| Level of Service | F | D | | | | | E | D | | C | C | C |
| Approach Delay (s) | 156.6 | | | | | | 66.1 | | | | 27.3 | |
| Approach LOS | F | | | | | | E | | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 36.5 | | | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | 0.85 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 118.8 | | | | | | Sum of lost time (s) | | | 20.0 | | |
| Intersection Capacity Utilization | 76.3% | | | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | | | ↑↑ | | ↑ |
| Volume (vph) | 527 | 856 | 351 | 9 | 12 | 156 | 111 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | | | | 0.97 | | 1.00 |
| Fr _t | 1.00 | 0.96 | | | | 0.94 | | 0.85 |
| Flt Protected | 0.95 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | 3433 | 3382 | | | | 3299 | 1583 | |
| Flt Permitted | 0.33 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | 1207 | 3382 | | | | 3299 | 1583 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 573 | 930 | 382 | 10 | 13 | 170 | 121 | 16 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 14 |
| Lane Group Flow (vph) | 573 | 1321 | 0 | 0 | 0 | 304 | 0 | 2 |
| Turn Type | pm+pt | | | | Perm | | Perm | |
| Protected Phases | 1 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | 64.0 | 53.5 | | | | 16.2 | 16.2 | |
| Effective Green, g (s) | 64.0 | 53.5 | | | | 16.2 | 16.2 | |
| Actuated g/C Ratio | 0.54 | 0.45 | | | | 0.14 | 0.14 | |
| Clearance Time (s) | 4.0 | 4.0 | | | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 959 | 1523 | | | | 450 | 216 | |
| v/s Ratio Prot | c0.08 | c0.39 | | | | | | |
| v/s Ratio Perm | 0.24 | | | | | 0.09 | 0.00 | |
| v/c Ratio | 0.60 | 0.87 | | | | 0.68 | 0.01 | |
| Uniform Delay, d1 | 16.3 | 29.5 | | | | 48.8 | 44.4 | |
| Progression Factor | 1.00 | 1.00 | | | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.0 | 5.5 | | | | 4.0 | 0.0 | |
| Delay (s) | 17.3 | 35.0 | | | | 52.8 | 44.4 | |
| Level of Service | B | C | | | | D | D | |
| Approach Delay (s) | 29.6 | | | | | 52.4 | | |
| Approach LOS | | C | | | | D | | |

Intersection Summary

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 4: Potrero Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|-------|-------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ ↖ | ↑ ↗ ↖ | ↑ ↗ | ↑ ↗ ↖ | | ↑ ↗ | ↑ ↗ ↖ | ↑ ↗ |
| Volume (vph) | 47 | 266 | 178 | 100 | 373 | 97 | 122 | 404 | 14 | 107 | 794 | 32 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3430 | | 1770 | 3522 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.36 | 1.00 | 1.00 | 0.42 | 1.00 | | 0.25 | 1.00 | | 0.48 | 1.00 | 1.00 |
| Satd. Flow (perm) | 664 | 1863 | 1583 | 790 | 3430 | | 461 | 3522 | | 901 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 51 | 289 | 193 | 109 | 405 | 105 | 133 | 439 | 15 | 116 | 863 | 35 |
| RTOR Reduction (vph) | 0 | 0 | 138 | 0 | 42 | 0 | 0 | 3 | 0 | 0 | 0 | 20 |
| Lane Group Flow (vph) | 51 | 289 | 55 | 109 | 468 | 0 | 133 | 451 | 0 | 116 | 863 | 15 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | | 25.9 | 22.1 | | 25.9 | 22.1 | 22.1 |
| Effective Green, g (s) | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | | 25.9 | 22.1 | | 25.9 | 22.1 | 22.1 |
| Actuated g/C Ratio | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | | 0.52 | 0.44 | | 0.52 | 0.44 | 0.44 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 188 | 528 | 449 | 224 | 972 | | 338 | 1554 | | 532 | 1561 | 698 |
| v/s Ratio Prot | c0.16 | | | 0.14 | | | c0.03 | 0.13 | | 0.02 | c0.24 | |
| v/s Ratio Perm | 0.08 | | 0.03 | 0.14 | | | 0.17 | | | 0.10 | | 0.01 |
| v/c Ratio | 0.27 | 0.55 | 0.12 | 0.49 | 0.48 | | 0.39 | 0.29 | | 0.22 | 0.55 | 0.02 |
| Uniform Delay, d1 | 13.9 | 15.2 | 13.3 | 14.9 | 14.9 | | 6.7 | 9.0 | | 6.3 | 10.3 | 7.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.8 | 1.2 | 0.1 | 1.7 | 0.4 | | 0.8 | 0.1 | | 0.2 | 0.4 | 0.0 |
| Delay (s) | 14.7 | 16.4 | 13.4 | 16.6 | 15.3 | | 7.5 | 9.1 | | 6.5 | 10.8 | 7.9 |
| Level of Service | B | B | B | B | B | | A | A | | A | B | A |
| Approach Delay (s) | | 15.2 | | | 15.5 | | | 8.7 | | | 10.2 | |
| Approach LOS | | B | | | B | | | A | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 12.0 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.54 | | |
| Actuated Cycle Length (s) | 50.1 | Sum of lost time (s) | 10.0 |
| Intersection Capacity Utilization | 62.1% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 5: Moeser Ln & San Pablo Ave

6/7/2012



| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|-------|-------|-------|
| Lane Configurations | ↑ ↗ | ↑ ↗ | ↗ ↘ | ↑ ↗ ↘ | | ↗ ↘ | ↑ ↗ ↘ |
| Volume (vph) | 311 | 91 | 33 | 456 | 94 | 153 | 785 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 |
| Frpb, ped/bikes | 1.00 | 0.98 | 1.00 | 0.99 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1547 | 1770 | 3429 | | 1767 | 3539 |
| Flt Permitted | 0.95 | 1.00 | 0.29 | 1.00 | | 0.36 | 1.00 |
| Satd. Flow (perm) | 1770 | 1547 | 535 | 3429 | | 678 | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 338 | 99 | 36 | 496 | 102 | 166 | 853 |
| RTOR Reduction (vph) | 0 | 70 | 0 | 24 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 338 | 29 | 36 | 574 | 0 | 166 | 853 |
| Confl. Peds. (#/hr) | 1 | 20 | | | 10 | 10 | |
| Confl. Bikes (#/hr) | | | | | 2 | | |
| Turn Type | | Perm | pm+pt | | pm+pt | | |
| Protected Phases | 4 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | 4 | 2 | | | 6 | |
| Actuated Green, G (s) | 14.2 | 14.2 | 23.1 | 21.7 | | 26.3 | 23.3 |
| Effective Green, g (s) | 14.2 | 14.2 | 23.1 | 21.7 | | 26.3 | 23.3 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.47 | 0.44 | | 0.54 | 0.48 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 514 | 449 | 288 | 1522 | | 431 | 1686 |
| v/s Ratio Prot | c0.19 | | 0.00 | 0.17 | | c0.02 | c0.24 |
| v/s Ratio Perm | | 0.02 | 0.06 | | | 0.18 | |
| v/c Ratio | 0.66 | 0.06 | 0.12 | 0.38 | | 0.39 | 0.51 |
| Uniform Delay, d1 | 15.2 | 12.5 | 7.0 | 9.1 | | 5.9 | 8.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.0 | 0.1 | 0.2 | 0.2 | | 0.6 | 0.2 |
| Delay (s) | 18.3 | 12.6 | 7.2 | 9.2 | | 6.5 | 9.1 |
| Level of Service | B | B | A | A | | A | A |
| Approach Delay (s) | 17.0 | | | 9.1 | | | 8.6 |
| Approach LOS | B | | | A | | A | |
| Intersection Summary | | | | | | | |
| HCM Average Control Delay | | 10.5 | | HCM Level of Service | | B | |
| HCM Volume to Capacity ratio | | 0.56 | | | | | |
| Actuated Cycle Length (s) | | 48.9 | | Sum of lost time (s) | | 9.0 | |
| Intersection Capacity Utilization | | 54.5% | | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | | |
| c Critical Lane Group | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
6: Central Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---|------|-------|------|------|----------------------|------|-------|------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | |
| Volume (vph) | 134 | 252 | 94 | 101 | 283 | 35 | 18 | 458 | 69 | 35 | 601 | 183 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1681 | 1765 | 1583 | | 3453 | | 1770 | 3470 | | 1770 | 3415 | |
| Flt Permitted | 0.49 | 0.97 | 1.00 | | 0.55 | | 0.16 | 1.00 | | 0.30 | 1.00 | |
| Satd. Flow (perm) | 866 | 1712 | 1583 | | 1925 | | 290 | 3470 | | 553 | 3415 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 146 | 274 | 102 | 110 | 308 | 38 | 20 | 498 | 75 | 38 | 653 | 199 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 6 | 0 | 0 | 11 | 0 | 0 | 25 | 0 |
| Lane Group Flow (vph) | 131 | 289 | 24 | 0 | 450 | 0 | 20 | 562 | 0 | 38 | 827 | 0 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | |
| Protected Phases | | 4 | | | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 3 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 20.5 | 20.5 | 20.5 | | 24.3 | | 27.7 | 25.7 | | 27.9 | 25.8 | |
| Effective Green, g (s) | 20.5 | 20.5 | 20.5 | | 24.3 | | 27.7 | 25.7 | | 27.9 | 25.8 | |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | | 0.28 | | 0.32 | 0.30 | | 0.32 | 0.30 | |
| Clearance Time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 206 | 408 | 377 | | 543 | | 128 | 1036 | | 209 | 1023 | |
| v/s Ratio Prot | | | | | | | 0.00 | 0.16 | | c0.00 | c0.24 | |
| v/s Ratio Perm | 0.15 | c0.17 | 0.02 | | c0.23 | | 0.05 | | | 0.05 | | |
| v/c Ratio | 0.64 | 0.71 | 0.06 | | 1.17dl | | 0.16 | 0.54 | | 0.18 | 0.81 | |
| Uniform Delay, d1 | 29.4 | 30.1 | 25.4 | | 28.9 | | 21.5 | 25.3 | | 20.5 | 27.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 6.3 | 5.6 | 0.1 | | 10.0 | | 0.6 | 0.6 | | 0.4 | 4.8 | |
| Delay (s) | 35.7 | 35.6 | 25.5 | | 39.0 | | 22.1 | 25.9 | | 20.9 | 32.6 | |
| Level of Service | D | D | C | | D | | C | C | | C | C | |
| Approach Delay (s) | | 33.7 | | | 39.0 | | | 25.7 | | | 32.1 | |
| Approach LOS | | C | | | D | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 32.2 | | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.73 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 86.1 | | | Sum of lost time (s) | | | 9.5 | | | | |
| Intersection Capacity Utilization | | 64.2% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| dl Defacto Left Lane. Recode with 1 though lane as a left lane. | | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 7: Fairmont Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|-------|------|-------|------|------|-------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | | | ↔ | | ↑ | ↑ | | ↑ | ↑ | |
| Volume (vph) | 2 | 215 | 13 | 87 | 196 | 105 | 22 | 336 | 72 | 99 | 691 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 0.99 | 1.00 | |
| Fr _t | 1.00 | 0.99 | | | 0.96 | | 1.00 | 0.97 | | 1.00 | 1.00 | |
| Fl _t Protected | 0.95 | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1745 | 1844 | | | 3317 | | 1769 | 3407 | | 1754 | 3523 | |
| Fl _t Permitted | 0.45 | 1.00 | | | 0.77 | | 0.36 | 1.00 | | 0.44 | 1.00 | |
| Satd. Flow (perm) | 831 | 1844 | | | 2571 | | 669 | 3407 | | 807 | 3523 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 234 | 14 | 95 | 213 | 114 | 24 | 365 | 78 | 108 | 751 | 21 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 63 | 0 | 0 | 24 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 2 | 244 | 0 | 0 | 359 | 0 | 24 | 419 | 0 | 108 | 770 | 0 |
| Confl. Peds. (#/hr) | 43 | | 22 | 22 | | 43 | 10 | | 37 | 37 | | 10 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | | | pm+pt | | | pm+pt | | | |
| Protected Phases | | 4 | | | 8 | | 1 | 6 | | 5 | | 2 |
| Permitted Phases | 4 | | | 8 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 12.5 | 12.5 | | | 12.5 | | 23.6 | 22.9 | | 29.7 | 26.0 | |
| Effective Green, g (s) | 12.5 | 12.5 | | | 12.5 | | 23.6 | 22.9 | | 29.7 | 26.0 | |
| Actuated g/C Ratio | 0.25 | 0.25 | | | 0.25 | | 0.47 | 0.46 | | 0.59 | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 207 | 459 | | | 640 | | 330 | 1554 | | 549 | 1825 | |
| v/s Ratio Prot | | 0.13 | | | | | 0.00 | 0.12 | | c0.01 | c0.22 | |
| v/s Ratio Perm | 0.00 | | | c0.14 | | | 0.03 | | | 0.10 | | |
| v/c Ratio | 0.01 | 0.53 | | | 0.56 | | 0.07 | 0.27 | | 0.20 | 0.42 | |
| Uniform Delay, d1 | 14.2 | 16.3 | | | 16.5 | | 7.1 | 8.5 | | 4.6 | 7.5 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 1.2 | | | 1.1 | | 0.1 | 0.1 | | 0.2 | 0.2 | |
| Delay (s) | 14.2 | 17.5 | | | 17.6 | | 7.2 | 8.6 | | 4.7 | 7.6 | |
| Level of Service | B | B | | | B | | A | A | | A | A | |
| Approach Delay (s) | | 17.5 | | | 17.6 | | | 8.5 | | | 7.3 | |
| Approach LOS | | B | | | B | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.0 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.43 | | |
| Actuated Cycle Length (s) | 50.2 | Sum of lost time (s) | 7.0 |
| Intersection Capacity Utilization | 72.9% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
8: Key Blvd & Elm St

6/7/2012



| Movement | EBL | EBR | NBL | NBT | SBT | SBR | SBR2 | NEL | NER |
|-----------------------------------|-------|------|-------|-------|-------|----------------------|------|-------|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 2 | 179 | 179 | 48 | 188 | 0 | 4 | 115 | 101 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.5 | | | 5.5 | 5.5 | | | 5.5 | 5.5 |
| Lane Util. Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 0.87 | | | | 1.00 | 1.00 | | 1.00 | 0.85 |
| Flt Protected | 1.00 | | | | 0.96 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1613 | | | | 1784 | 1857 | | 1770 | 1583 |
| Flt Permitted | 1.00 | | | | 0.57 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | 1613 | | | | 1054 | 1857 | | 1770 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 195 | 195 | 52 | 204 | 0 | 4 | 125 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 96 |
| Lane Group Flow (vph) | 197 | 0 | 0 | 247 | 207 | 0 | 0 | 125 | 14 |
| Confl. Peds. (#/hr) | | | | 3 | | | 3 | | |
| Confl. Bikes (#/hr) | | | | | | | 2 | | |
| Turn Type | | | | Perm | | | | Perm | |
| Protected Phases | 3 | | | 4 2 | 7 2 | | | 8 | |
| Permitted Phases | | | | 4 2 | | | | 8 | |
| Actuated Green, G (s) | 15.2 | | | | 30.6 | 27.0 | | 11.9 | 11.9 |
| Effective Green, g (s) | 15.2 | | | | 30.6 | 27.0 | | 11.9 | 11.9 |
| Actuated g/C Ratio | 0.16 | | | | 0.32 | 0.28 | | 0.12 | 0.12 |
| Clearance Time (s) | 5.5 | | | | | | 5.5 | 5.5 | |
| Vehicle Extension (s) | 3.0 | | | | | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 258 | | | 339 | 527 | | | 221 | 198 |
| v/s Ratio Prot | c0.12 | | | | c0.11 | | | c0.07 | |
| v/s Ratio Perm | | | | c0.23 | | | | 0.01 | |
| v/c Ratio | 0.76 | | | 0.73 | 0.39 | | | 0.57 | 0.07 |
| Uniform Delay, d1 | 38.3 | | | 28.6 | 27.5 | | | 39.2 | 36.8 |
| Progression Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 12.6 | | | 7.6 | 0.5 | | | 3.3 | 0.1 |
| Delay (s) | 50.9 | | | 36.2 | 28.0 | | | 42.5 | 36.9 |
| Level of Service | D | | | D | C | | | D | D |
| Approach Delay (s) | 50.9 | | | 36.2 | 28.0 | | | 39.9 | |
| Approach LOS | D | | | D | C | | | D | |
| Intersection Summary | | | | | | | | | |
| HCM Average Control Delay | | | 38.5 | | | HCM Level of Service | | D | |
| HCM Volume to Capacity ratio | | | 0.67 | | | | | | |
| Actuated Cycle Length (s) | | | 95.2 | | | Sum of lost time (s) | | 27.5 | |
| Intersection Capacity Utilization | | | 58.8% | | | ICU Level of Service | | B | |
| Analysis Period (min) | | | 15 | | | | | | |
| c Critical Lane Group | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
9: Potrero Ave & Richmond St

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 32 | 107 | 76 | 22 | 145 | 24 | 59 | 254 | 13 | 12 | 335 | 45 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Flt Protected | 0.95 | | | | 0.98 | | | 0.99 | | | 0.98 | |
| Flt Permitted | 0.99 | | | | 0.99 | | | 0.99 | | | 1.00 | |
| Satd. Flow (prot) | 1760 | | | | 1821 | | | 1836 | | | 1831 | |
| Flt Permitted | 1760 | | | | 1821 | | | 1836 | | | 1831 | |
| Satd. Flow (perm) | 0.91 | | | | 0.93 | | | 0.89 | | | 0.98 | |
| | 1620 | | | | 1706 | | | 1647 | | | 1800 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 35 | 116 | 83 | 24 | 158 | 26 | 64 | 276 | 14 | 13 | 364 | 49 |
| RTOR Reduction (vph) | 0 | 59 | 0 | 0 | 15 | 0 | 0 | 4 | 0 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 175 | 0 | 0 | 193 | 0 | 0 | 350 | 0 | 0 | 414 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 6.5 | | | 6.5 | | | 8.7 | | | 8.7 | | |
| Effective Green, g (s) | 6.5 | | | 6.5 | | | 8.7 | | | 8.7 | | |
| Actuated g/C Ratio | 0.28 | | | 0.28 | | | 0.37 | | | 0.37 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 454 | | | 478 | | | 618 | | | 675 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.11 | | | c0.11 | | | 0.21 | | | c0.23 | | |
| v/c Ratio | 0.39 | | | 0.40 | | | 0.57 | | | 0.61 | | |
| Uniform Delay, d1 | 6.7 | | | 6.8 | | | 5.8 | | | 5.9 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 0.5 | | | 0.6 | | | 1.2 | | | 1.7 | | |
| Delay (s) | 7.3 | | | 7.3 | | | 7.0 | | | 7.5 | | |
| Level of Service | A | | | A | | | A | | | A | | |
| Approach Delay (s) | 7.3 | | | 7.3 | | | 7.0 | | | 7.5 | | |
| Approach LOS | A | | | A | | | A | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 7.3 | | | HCM Level of Service | | | A | | | | | |
| HCM Volume to Capacity ratio | 0.52 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 23.2 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 65.8% | | | ICU Level of Service | | | C | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
10: Moeser Ln & Richmond St

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 2 | 217 | 15 | 65 | 274 | 76 | 20 | 164 | 11 | 81 | 351 | 44 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | | | | 0.99 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Fr | 0.99 | | | | 0.98 | | | 0.99 | | | 0.99 | |
| Flt Protected | 1.00 | | | | 0.99 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1842 | | | | 1783 | | | 1836 | | | 1818 | |
| Flt Permitted | 1.00 | | | | 0.91 | | | 0.93 | | | 0.91 | |
| Satd. Flow (perm) | 1837 | | | | 1638 | | | 1723 | | | 1672 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 236 | 16 | 71 | 298 | 83 | 22 | 178 | 12 | 88 | 382 | 48 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 18 | 0 | 0 | 5 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 248 | 0 | 0 | 434 | 0 | 0 | 207 | 0 | 0 | 509 | 0 |
| Confl. Peds. (#/hr) | 28 | | 11 | 11 | | 28 | 4 | | 5 | 5 | | 4 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 14.1 | | | 14.1 | | | 15.9 | | | 15.9 | | |
| Effective Green, g (s) | 14.1 | | | 14.1 | | | 15.9 | | | 15.9 | | |
| Actuated g/C Ratio | 0.37 | | | 0.37 | | | 0.42 | | | 0.42 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 682 | | | 608 | | | 721 | | | 700 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.14 | | | c0.26 | | | 0.12 | | | c0.30 | | |
| v/c Ratio | 0.36 | | | 0.71 | | | 0.29 | | | 0.73 | | |
| Uniform Delay, d1 | 8.7 | | | 10.2 | | | 7.3 | | | 9.2 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 0.3 | | | 4.0 | | | 0.2 | | | 3.8 | | |
| Delay (s) | 9.0 | | | 14.2 | | | 7.5 | | | 13.0 | | |
| Level of Service | A | | | B | | | A | | | B | | |
| Approach Delay (s) | 9.0 | | | 14.2 | | | 7.5 | | | 13.0 | | |
| Approach LOS | A | | | B | | | A | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 11.9 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.72 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 38.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 85.7% | | | ICU Level of Service | | | E | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 11: Central Ave & Richmond St

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|-------|------|----------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 56 | 171 | 32 | 11 | 282 | 77 | 33 | 67 | 4 | 36 | 193 | 124 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 61 | 186 | 35 | 12 | 307 | 84 | 36 | 73 | 4 | 39 | 210 | 135 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 282 | 402 | 113 | 384 | | | | | | | | |
| Volume Left (vph) | 61 | 12 | 36 | 39 | | | | | | | | |
| Volume Right (vph) | 35 | 84 | 4 | 135 | | | | | | | | |
| Hadj (s) | 0.00 | -0.08 | 0.07 | -0.16 | | | | | | | | |
| Departure Headway (s) | 6.4 | 6.1 | 7.1 | 6.2 | | | | | | | | |
| Degree Utilization, x | 0.50 | 0.68 | 0.22 | 0.66 | | | | | | | | |
| Capacity (veh/h) | 507 | 552 | 408 | 549 | | | | | | | | |
| Control Delay (s) | 15.7 | 21.0 | 12.2 | 20.2 | | | | | | | | |
| Approach Delay (s) | 15.7 | 21.0 | 12.2 | 20.2 | | | | | | | | |
| Approach LOS | C | C | B | C | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | | | 18.6 | | | | | | | |
| HCM Level of Service | | | | | C | | | | | | | |
| Intersection Capacity Utilization | | | 67.2% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | | 15 | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 12: Fairmont Ave & Richmond St

6/7/2012



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|-------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Sign Control | | Stop | Stop | | Stop | |
| Volume (vph) | 27 | 291 | 300 | 77 | 139 | 65 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 29 | 316 | 326 | 84 | 151 | 71 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total (vph) | 346 | 410 | 222 | | | |
| Volume Left (vph) | 29 | 0 | 151 | | | |
| Volume Right (vph) | 0 | 84 | 71 | | | |
| Hadj (s) | 0.05 | -0.09 | -0.02 | | | |
| Departure Headway (s) | 5.2 | 5.0 | 5.7 | | | |
| Degree Utilization, x | 0.50 | 0.57 | 0.35 | | | |
| Capacity (veh/h) | 662 | 697 | 568 | | | |
| Control Delay (s) | 13.3 | 14.3 | 11.9 | | | |
| Approach Delay (s) | 13.3 | 14.3 | 11.9 | | | |
| Approach LOS | B | B | B | | | |
| Intersection Summary | | | | | | |
| Delay | | 13.4 | | | | |
| HCM Level of Service | | B | | | | |
| Intersection Capacity Utilization | | 58.2% | | ICU Level of Service | | B |
| Analysis Period (min) | | 15 | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 13: Fairmont Ave & Colusa Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBT | NBL2 | NBL | NBR2 | SEL | SET | SER | SER2 |
|-----------------------------------|-------|------|------|------|----------------------|------|------|------|------|------|------|--------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 62 | 8 | 198 | 3 | 2 | 9 | 22 | 1 | 4 | 253 | 29 | 93 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | 1.00 | | | 0.95 | | 0.95 |
| Fr _t | 0.90 | | | | 1.00 | | 1.00 | | | 0.98 | | 0.85 |
| Flt Protected | 0.99 | | | | 1.00 | | 0.95 | | | 1.00 | | 1.00 |
| Satd. Flow (prot) | 1657 | | | | 1863 | | 1770 | | | 1734 | | 1504 |
| Flt Permitted | 0.93 | | | | 1.00 | | 0.95 | | | 1.00 | | 1.00 |
| Satd. Flow (perm) | 1560 | | | | 1863 | | 1770 | | | 1730 | | 1504 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 67 | 9 | 215 | 3 | 2 | 10 | 24 | 1 | 4 | 275 | 32 | 101 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 73 |
| Lane Group Flow (vph) | 0 | 293 | 0 | 0 | 2 | 0 | 34 | 0 | 0 | 320 | 0 | 18 |
| Turn Type | Perm | | | | | Perm | | | Perm | | | custom |
| Protected Phases | | 6 | | | | 2 | | 4 | | | 8 | |
| Permitted Phases | 6 | | | | | | 4 | | | 8 | | 4 |
| Actuated Green, G (s) | 14.9 | | | | 14.9 | | 5.2 | | | 18.6 | | 5.2 |
| Effective Green, g (s) | 14.9 | | | | 14.9 | | 5.2 | | | 18.6 | | 5.2 |
| Actuated g/C Ratio | 0.29 | | | | 0.29 | | 0.10 | | | 0.36 | | 0.10 |
| Clearance Time (s) | 4.5 | | | | 4.5 | | 4.5 | | | 4.5 | | 4.5 |
| Vehicle Extension (s) | 3.0 | | | | 3.0 | | 3.0 | | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 445 | | | | 532 | | 176 | | | 616 | | 150 |
| v/s Ratio Prot | | | | | 0.00 | | | | | | | |
| v/s Ratio Perm | c0.19 | | | | | | 0.02 | | | 0.18 | | 0.01 |
| v/c Ratio | 0.66 | | | | 0.00 | | 0.19 | | | 0.52 | | 0.12 |
| Uniform Delay, d1 | 16.4 | | | | 13.3 | | 21.6 | | | 13.3 | | 21.4 |
| Progression Factor | 1.00 | | | | 1.00 | | 1.00 | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 3.5 | | | | 0.0 | | 0.5 | | | 0.7 | | 0.4 |
| Delay (s) | 19.9 | | | | 13.3 | | 22.1 | | | 14.0 | | 21.8 |
| Level of Service | B | | | | B | | C | | | B | | C |
| Approach Delay (s) | 19.9 | | | | 13.3 | | 22.1 | | | 15.7 | | |
| Approach LOS | B | | | | B | | C | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 16.7 | | | | HCM Level of Service | | | | | B | | |
| HCM Volume to Capacity ratio | 0.56 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 52.2 | | | | Sum of lost time (s) | | | | | 13.5 | | |
| Intersection Capacity Utilization | 67.6% | | | | ICU Level of Service | | | | | C | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak
 13: Fairmont Ave & Colusa Ave

6/7/2012



| Movement | NWL2 | NWL | NWT |
|------------------------|-------|------|------|
| Lane Configurations | | | |
| Volume (vph) | 1 | 165 | 157 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.5 | 4.5 |
| Lane Util. Factor | | 1.00 | 1.00 |
| Fr _t | | 1.00 | 1.00 |
| Flt Protected | | 0.95 | 1.00 |
| Satd. Flow (prot) | | 1770 | 1863 |
| Flt Permitted | | 0.46 | 1.00 |
| Satd. Flow (perm) | | 856 | 1863 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1 | 179 | 171 |
| RTOR Reduction (vph) | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 180 | 171 |
| Turn Type | Perm | Perm | |
| Protected Phases | | | 8 |
| Permitted Phases | 8 | 8 | |
| Actuated Green, G (s) | 18.6 | 18.6 | |
| Effective Green, g (s) | 18.6 | 18.6 | |
| Actuated g/C Ratio | 0.36 | 0.36 | |
| Clearance Time (s) | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 305 | 664 | |
| v/s Ratio Prot | | 0.09 | |
| v/s Ratio Perm | c0.21 | | |
| v/c Ratio | 0.59 | 0.26 | |
| Uniform Delay, d1 | 13.7 | 11.9 | |
| Progression Factor | 1.00 | 1.00 | |
| Incremental Delay, d2 | 3.0 | 0.2 | |
| Delay (s) | 16.7 | 12.1 | |
| Level of Service | B | B | |
| Approach Delay (s) | | 14.5 | |
| Approach LOS | | B | |
| Intersection Summary | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 1: MacDonald Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|-------|------|------|-------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↓ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑↓ | |
| Volume (vph) | 31 | 403 | 108 | 212 | 775 | 90 | 297 | 97 | 263 | 28 | 55 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.96 | 1.00 | 0.98 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | | 0.97 | 1.00 | 1.00 | 0.99 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3433 | 1863 | 1520 | 1747 | 1828 | | 1713 | 3539 | 1521 | 1743 | 4764 | |
| Flt Permitted | 0.12 | 1.00 | 1.00 | 0.44 | 1.00 | | 0.70 | 1.00 | 1.00 | 0.69 | 1.00 | |
| Satd. Flow (perm) | 428 | 1863 | 1520 | 805 | 1828 | | 1253 | 3539 | 1521 | 1259 | 4764 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 34 | 438 | 117 | 230 | 842 | 98 | 323 | 105 | 286 | 30 | 60 | 27 |
| RTOR Reduction (vph) | 0 | 0 | 52 | 0 | 6 | 0 | 0 | 0 | 197 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 34 | 438 | 65 | 230 | 934 | 0 | 323 | 105 | 89 | 30 | 68 | 0 |
| Confl. Peds. (#/hr) | 12 | | 24 | 24 | | 12 | 19 | | 9 | 9 | | 19 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 2 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 33.8 | 33.8 | 33.8 | 33.8 | 33.8 | | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | |
| Effective Green, g (s) | 33.8 | 33.8 | 33.8 | 33.8 | 33.8 | | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | |
| Actuated g/C Ratio | 0.56 | 0.56 | 0.56 | 0.56 | 0.56 | | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 238 | 1036 | 845 | 448 | 1016 | | 392 | 1106 | 475 | 393 | 1489 | |
| v/s Ratio Prot | | 0.24 | | c0.51 | | | 0.03 | | | | 0.01 | |
| v/s Ratio Perm | 0.08 | | 0.04 | 0.29 | | | c0.26 | | 0.06 | 0.02 | | |
| v/c Ratio | 0.14 | 0.42 | 0.08 | 0.51 | 0.92 | | 0.82 | 0.09 | 0.19 | 0.08 | 0.05 | |
| Uniform Delay, d1 | 6.5 | 7.8 | 6.3 | 8.4 | 12.3 | | 19.4 | 14.8 | 15.3 | 14.7 | 14.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 0.3 | 0.0 | 1.0 | 12.8 | | 13.1 | 0.0 | 0.2 | 0.1 | 0.0 | |
| Delay (s) | 6.8 | 8.1 | 6.3 | 9.4 | 25.0 | | 32.5 | 14.8 | 15.5 | 14.8 | 14.6 | |
| Level of Service | A | A | A | A | C | | C | B | B | B | B | |
| Approach Delay (s) | | | 7.7 | | 21.9 | | | 23.1 | | | 14.6 | |
| Approach LOS | | | A | | C | | | C | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 18.7 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.89 | | |
| Actuated Cycle Length (s) | 60.8 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 82.8% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 2: Cutting Blvd & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|----------------------|-------|------|------|--------|-------|------|------|-------|------|
| Lane Configurations | ↑ | | ↑↑ | ↑↑ | ↑↑ | ↑ | ↑↑ | ↑↑↑ | | | ↑↑ | ↑ |
| Volume (vph) | 194 | 0 | 574 | 100 | 504 | 88 | 475 | 880 | 0 | 0 | 578 | 197 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | | | 0.95 | 1.00 |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | 3433 | 5085 | | | 3539 | 1583 |
| Flt Permitted | 0.45 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 833 | | 2787 | 3433 | 3539 | 1583 | 3526 | 5085 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 211 | 0 | 624 | 109 | 548 | 96 | 516 | 957 | 0 | 0 | 628 | 214 |
| RTOR Reduction (vph) | 0 | 0 | 438 | 0 | 0 | 42 | 0 | 0 | 0 | 0 | 0 | 141 |
| Lane Group Flow (vph) | 211 | 0 | 186 | 109 | 548 | 54 | 516 | 957 | 0 | 0 | 628 | 73 |
| Turn Type | custom | | custom | Perm | | Perm | custom | | | | Perm | |
| Protected Phases | | | | | 3 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 5 | 3 | | 3 | 5 | | | | 6 | |
| Actuated Green, G (s) | 12.2 | | 19.8 | 17.7 | 17.7 | 17.7 | 4.1 | 25.7 | | | 18.6 | 18.6 |
| Effective Green, g (s) | 12.2 | | 19.8 | 17.7 | 17.7 | 17.7 | 4.1 | 25.7 | | | 18.6 | 18.6 |
| Actuated g/C Ratio | 0.18 | | 0.30 | 0.27 | 0.27 | 0.27 | 0.06 | 0.39 | | | 0.28 | 0.28 |
| Clearance Time (s) | 3.5 | | | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 153 | | 829 | 912 | 941 | 421 | 217 | 1962 | | | 988 | 442 |
| v/s Ratio Prot | | | | c0.15 | | | 0.19 | | | | c0.18 | |
| v/s Ratio Perm | c0.25 | | 0.07 | 0.03 | | 0.03 | c0.15 | | | | 0.05 | |
| v/c Ratio | 1.38 | | 0.22 | 0.12 | 0.58 | 0.13 | 2.38 | 0.49 | | | 0.64 | 0.16 |
| Uniform Delay, d1 | 27.2 | | 17.6 | 18.5 | 21.2 | 18.6 | 31.2 | 15.5 | | | 21.0 | 18.1 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 206.0 | | 0.1 | 0.1 | 0.9 | 0.1 | 634.0 | 0.2 | | | 1.3 | 0.2 |
| Delay (s) | 233.2 | | 17.8 | 18.6 | 22.2 | 18.7 | 665.3 | 15.7 | | | 22.4 | 18.3 |
| Level of Service | F | | B | B | C | B | F | B | | | C | B |
| Approach Delay (s) | 72.2 | | | | 21.2 | | | 243.2 | | | 21.3 | |
| Approach LOS | E | | | | C | | | F | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 115.9 | | HCM Level of Service | | | | | F | | | | |
| HCM Volume to Capacity ratio | 0.93 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 66.6 | | Sum of lost time (s) | | | | | 14.0 | | | | |
| Intersection Capacity Utilization | 67.5% | | ICU Level of Service | | | | | C | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|-----------------------------------|-------|------|------|------|------|------|----------------------|------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 46 | 33 | 35 | 2 | 29 | 32 | 15 | 239 | 61 | 24 | 940 | 115 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.97 | 1.00 | | | | | 0.96 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1810 | 1583 | | | | | 1790 | 1583 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.16 | 1.00 | | | | | 0.71 | 1.00 | | 0.10 | 1.00 | 1.00 |
| Satd. Flow (perm) | 306 | 1583 | | | | | 1322 | 1583 | | 177 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 50 | 36 | 38 | 2 | 32 | 35 | 16 | 260 | 66 | 26 | 1022 | 125 |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 244 | 0 | 0 | 0 | 87 |
| Lane Group Flow (vph) | 0 | 86 | 39 | 0 | 0 | 0 | 83 | 16 | 0 | 92 | 1022 | 38 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | pm+pt | pm+pt | | Perm |
| Protected Phases | | 3 | | | | | | 7 | | 5 | 5 | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | 2 |
| Actuated Green, G (s) | 41.0 | 41.0 | | | | | 9.0 | 9.0 | | 52.0 | 42.0 | 42.0 |
| Effective Green, g (s) | 41.0 | 41.0 | | | | | 9.0 | 9.0 | | 52.0 | 42.0 | 42.0 |
| Actuated g/C Ratio | 0.28 | 0.28 | | | | | 0.06 | 0.06 | | 0.36 | 0.29 | 0.29 |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 86 | 446 | | | | | 82 | 98 | | 173 | 1021 | 457 |
| v/s Ratio Prot | | | | | | | | | | 0.04 | 0.29 | |
| v/s Ratio Perm | c0.28 | 0.02 | | | | | c0.06 | 0.01 | | 0.15 | | 0.02 |
| v/c Ratio | 1.00 | 0.09 | | | | | 1.01 | 0.16 | | 0.53 | 1.00 | 0.08 |
| Uniform Delay, d1 | 52.3 | 38.5 | | | | | 68.3 | 64.7 | | 36.9 | 51.8 | 37.8 |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 97.0 | 0.1 | | | | | 102.8 | 0.8 | | 3.1 | 28.4 | 0.1 |
| Delay (s) | 149.3 | 38.6 | | | | | 171.1 | 65.5 | | 40.0 | 80.2 | 37.8 |
| Level of Service | F | D | | | | | F | E | | D | F | D |
| Approach Delay (s) | 114.2 | | | | | | 91.1 | | | | 72.9 | |
| Approach LOS | F | | | | | | F | | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 79.6 | | | | | | HCM Level of Service | | | E | | |
| HCM Volume to Capacity ratio | 0.96 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 145.6 | | | | | | Sum of lost time (s) | | | 16.0 | | |
| Intersection Capacity Utilization | 71.3% | | | | | | ICU Level of Service | | | C | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | | | ↑↑ | | ↑ |
| Volume (vph) | 324 | 677 | 236 | 8 | 14 | 274 | 113 | 46 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | | | | 0.97 | | 1.00 |
| Fr _t | 1.00 | 0.96 | | | | 0.96 | | 0.85 |
| Flt Protected | 0.95 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | 3433 | 3398 | | | | 3341 | | 1583 |
| Flt Permitted | 0.09 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | 336 | 3398 | | | | 3341 | | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 352 | 736 | 257 | 9 | 15 | 298 | 123 | 50 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 42 |
| Lane Group Flow (vph) | 352 | 1001 | 0 | 0 | 0 | 436 | 0 | 8 |
| Turn Type | pm+pt | | | Perm | | | Perm | |
| Protected Phases | 1 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | 53.0 | 43.0 | | | | 23.6 | | 23.6 |
| Effective Green, g (s) | 53.0 | 43.0 | | | | 23.6 | | 23.6 |
| Actuated g/C Ratio | 0.36 | 0.30 | | | | 0.16 | | 0.16 |
| Clearance Time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 335 | 1004 | | | | 542 | | 257 |
| v/s Ratio Prot | c0.07 | 0.29 | | | | | | |
| v/s Ratio Perm | c0.31 | | | | | 0.13 | | 0.01 |
| v/c Ratio | 1.05 | 1.00 | | | | 0.80 | | 0.03 |
| Uniform Delay, d1 | 38.4 | 51.2 | | | | 58.8 | | 51.4 |
| Progression Factor | 1.00 | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 63.1 | 27.5 | | | | 8.5 | | 0.1 |
| Delay (s) | 101.5 | 78.8 | | | | 67.2 | | 51.4 |
| Level of Service | F | E | | | | E | | D |
| Approach Delay (s) | | 84.7 | | | | 65.6 | | |
| Approach LOS | | F | | | | E | | |

Intersection Summary

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 4: Potrero Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|-------|-------|------|------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 105 | 191 | 155 | 69 | 185 | 62 | 138 | 959 | 26 | 81 | 612 | 95 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3406 | | 1770 | 3525 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.58 | 1.00 | 1.00 | 0.53 | 1.00 | | 0.34 | 1.00 | | 0.20 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1081 | 1863 | 1583 | 996 | 3406 | | 626 | 3525 | | 379 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 114 | 208 | 168 | 75 | 201 | 67 | 150 | 1042 | 28 | 88 | 665 | 103 |
| RTOR Reduction (vph) | 0 | 0 | 126 | 0 | 50 | 0 | 0 | 2 | 0 | 0 | 0 | 55 |
| Lane Group Flow (vph) | 114 | 208 | 42 | 75 | 218 | 0 | 150 | 1068 | 0 | 88 | 665 | 48 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | 12.2 | 12.2 | 12.2 | 12.2 | 12.2 | | 28.4 | 24.6 | | 25.2 | 23.0 | 23.0 |
| Effective Green, g (s) | 12.2 | 12.2 | 12.2 | 12.2 | 12.2 | | 28.4 | 24.6 | | 25.2 | 23.0 | 23.0 |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | | 0.58 | 0.50 | | 0.51 | 0.47 | 0.47 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 269 | 464 | 394 | 248 | 848 | | 452 | 1770 | | 257 | 1661 | 743 |
| v/s Ratio Prot | c0.11 | | | 0.06 | | c0.03 | c0.30 | | 0.02 | 0.19 | | |
| v/s Ratio Perm | 0.11 | | 0.03 | 0.08 | | | 0.17 | | | 0.16 | | 0.03 |
| v/c Ratio | 0.42 | 0.45 | 0.11 | 0.30 | 0.26 | | 0.33 | 0.60 | | 0.34 | 0.40 | 0.07 |
| Uniform Delay, d1 | 15.4 | 15.6 | 14.2 | 14.9 | 14.8 | | 4.9 | 8.7 | | 6.5 | 8.5 | 7.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.1 | 0.7 | 0.1 | 0.7 | 0.2 | | 0.4 | 0.6 | | 0.8 | 0.2 | 0.0 |
| Delay (s) | 16.5 | 16.2 | 14.3 | 15.6 | 14.9 | | 5.4 | 9.3 | | 7.3 | 8.7 | 7.2 |
| Level of Service | B | B | B | B | B | | A | A | | A | A | A |
| Approach Delay (s) | | 15.6 | | | 15.1 | | | 8.8 | | | 8.3 | |
| Approach LOS | | B | | | B | | | A | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 10.6 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.54 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 49.0 | | | Sum of lost time (s) | | | 9.0 | | | | |
| Intersection Capacity Utilization | | 59.0% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 5: Moeser Ln & San Pablo Ave

6/7/2012



| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|-------|------|-------|
| Lane Configurations | ↑ ↗ | ↑ ↗ | ↗ ↘ | ↑ ↗ ↘ | | ↑ ↗ | ↑ ↗ ↘ |
| Volume (vph) | 210 | 66 | 60 | 1086 | 136 | 143 | 631 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 |
| Frpb, ped/bikes | 1.00 | 0.96 | 1.00 | 0.99 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1520 | 1770 | 3459 | | 1769 | 3539 |
| Flt Permitted | 0.95 | 1.00 | 0.27 | 1.00 | | 0.20 | 1.00 |
| Satd. Flow (perm) | 1770 | 1520 | 508 | 3459 | | 372 | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 228 | 72 | 65 | 1180 | 148 | 155 | 686 |
| RTOR Reduction (vph) | 0 | 41 | 0 | 16 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 228 | 31 | 65 | 1312 | 0 | 155 | 686 |
| Confl. Peds. (#/hr) | | 41 | | | 18 | 18 | |
| Confl. Bikes (#/hr) | | | | | 8 | | |
| Turn Type | | Perm | pm+pt | | pm+pt | | |
| Protected Phases | 4 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | | 4 | 2 | | 6 | | |
| Actuated Green, G (s) | 26.0 | 26.0 | 24.0 | 20.0 | 24.0 | 20.0 | |
| Effective Green, g (s) | 26.0 | 26.0 | 24.0 | 20.0 | 24.0 | 20.0 | |
| Actuated g/C Ratio | 0.43 | 0.43 | 0.40 | 0.33 | 0.40 | 0.33 | |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 4.0 | 3.0 | 4.0 | |
| Lane Grp Cap (vph) | 767 | 659 | 287 | 1153 | 242 | 1180 | |
| v/s Ratio Prot | c0.13 | | 0.02 | c0.38 | c0.04 | 0.19 | |
| v/s Ratio Perm | | 0.02 | 0.08 | | 0.21 | | |
| v/c Ratio | 0.30 | 0.05 | 0.23 | 1.14 | 0.64 | 0.58 | |
| Uniform Delay, d1 | 11.1 | 9.8 | 11.5 | 20.0 | 14.2 | 16.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.0 | 0.1 | 1.8 | 73.0 | 12.3 | 2.1 | |
| Delay (s) | 12.0 | 10.0 | 13.4 | 93.0 | 26.5 | 18.6 | |
| Level of Service | B | A | B | F | C | B | |
| Approach Delay (s) | 11.5 | | | 89.3 | | 20.1 | |
| Approach LOS | B | | | F | | C | |
| Intersection Summary | | | | | | | |
| HCM Average Control Delay | | 57.1 | | HCM Level of Service | | E | |
| HCM Volume to Capacity ratio | | 0.66 | | | | | |
| Actuated Cycle Length (s) | | 60.0 | | Sum of lost time (s) | | 10.0 | |
| Intersection Capacity Utilization | | 74.1% | | ICU Level of Service | | D | |
| Analysis Period (min) | | 15 | | | | | |

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
6: Central Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Volume (vph) | 382 | 229 | 153 | 52 | 210 | 76 | 159 | 866 | 57 | 44 | 576 | 210 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.97 | | 1.00 | 0.99 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 0.98 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1681 | 1741 | 1583 | | 3393 | | 1770 | 3506 | | 1770 | 3397 | |
| Flt Permitted | 0.53 | 0.76 | 1.00 | | 0.55 | | 0.18 | 1.00 | | 0.20 | 1.00 | |
| Satd. Flow (perm) | 943 | 1338 | 1583 | | 1884 | | 339 | 3506 | | 373 | 3397 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 415 | 249 | 166 | 57 | 228 | 83 | 173 | 941 | 62 | 48 | 626 | 228 |
| RTOR Reduction (vph) | 0 | 0 | 115 | 0 | 27 | 0 | 0 | 5 | 0 | 0 | 37 | 0 |
| Lane Group Flow (vph) | 295 | 369 | 51 | 0 | 341 | 0 | 173 | 998 | 0 | 48 | 817 | 0 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | |
| Protected Phases | | 4 | | | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 3 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 31.0 | 31.0 | 31.0 | | 30.0 | | 28.0 | 22.0 | | 24.0 | 20.0 | |
| Effective Green, g (s) | 31.0 | 31.0 | 31.0 | | 30.0 | | 28.0 | 22.0 | | 24.0 | 20.0 | |
| Actuated g/C Ratio | 0.31 | 0.31 | 0.31 | | 0.30 | | 0.28 | 0.22 | | 0.24 | 0.20 | |
| Clearance Time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Grp Cap (vph) | 291 | 413 | 488 | | 562 | | 180 | 767 | | 145 | 676 | |
| v/s Ratio Prot | | | | | | | c0.06 | c0.28 | | 0.01 | 0.24 | |
| v/s Ratio Perm | c0.31 | 0.28 | 0.03 | | c0.18 | | 0.21 | | | 0.07 | | |
| v/c Ratio | 1.01 | 0.89 | 0.10 | | 0.61 | | 0.96 | 1.30 | | 0.33 | 1.21 | |
| Uniform Delay, d1 | 34.8 | 33.2 | 24.8 | | 30.2 | | 34.1 | 39.2 | | 31.2 | 40.2 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 56.3 | 24.3 | 0.4 | | 4.8 | | 57.6 | 145.2 | | 6.0 | 107.4 | |
| Delay (s) | 91.1 | 57.4 | 25.3 | | 35.0 | | 91.7 | 184.4 | | 37.3 | 147.7 | |
| Level of Service | F | E | C | | D | | F | F | | D | F | |
| Approach Delay (s) | | 63.0 | | | 35.0 | | | 170.8 | | | 141.8 | |
| Approach LOS | | E | | | D | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 120.2 | | | HCM Level of Service | | | F | | | | |
| HCM Volume to Capacity ratio | | 0.95 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 100.5 | | | Sum of lost time (s) | | | 12.5 | | | | |
| Intersection Capacity Utilization | | 71.1% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 7: Fairmont Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|-------|------|-------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 11 | 170 | 16 | 110 | 171 | 56 | 72 | 1024 | 121 | 88 | 801 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | | 0.99 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.99 | | | 0.98 | | 1.00 | 0.98 | | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | | 0.98 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1752 | 1833 | | | 3359 | | 1768 | 3469 | | 1769 | 3530 | |
| Flt Permitted | 0.51 | 1.00 | | | 0.79 | | 0.21 | 1.00 | | 0.14 | 1.00 | |
| Satd. Flow (perm) | 937 | 1833 | | | 2682 | | 387 | 3469 | | 266 | 3530 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 185 | 17 | 120 | 186 | 61 | 78 | 1113 | 132 | 96 | 871 | 12 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 25 | 0 | 0 | 14 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 12 | 197 | 0 | 0 | 342 | 0 | 78 | 1231 | 0 | 96 | 882 | 0 |
| Confl. Peds. (#/hr) | 21 | | 30 | 30 | | 21 | 30 | | 10 | 10 | | 30 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | 4 | | | | 1 |
| Turn Type | Perm | | Perm | | | pm+pt | | | pm+pt | | | |
| Protected Phases | | 4 | | | 8 | | 1 | 6 | | 5 | | 2 |
| Permitted Phases | 4 | | | 8 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 25.0 | 25.0 | | | 25.0 | | 32.0 | 28.0 | | 32.0 | 28.0 | |
| Effective Green, g (s) | 25.0 | 25.0 | | | 25.0 | | 32.0 | 28.0 | | 32.0 | 28.0 | |
| Actuated g/C Ratio | 0.37 | 0.37 | | | 0.37 | | 0.47 | 0.41 | | 0.47 | 0.41 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Grp Cap (vph) | 344 | 674 | | | 986 | | 263 | 1428 | | 214 | 1454 | |
| v/s Ratio Prot | | 0.11 | | | | | 0.02 | c0.36 | | c0.03 | 0.25 | |
| v/s Ratio Perm | 0.01 | | | c0.13 | | | 0.12 | | | 0.19 | | |
| v/c Ratio | 0.03 | 0.29 | | | 0.35 | | 0.30 | 0.86 | | 0.45 | 0.61 | |
| Uniform Delay, d1 | 13.8 | 15.2 | | | 15.6 | | 10.8 | 18.2 | | 13.1 | 15.7 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.2 | 1.1 | | | 1.0 | | 2.9 | 7.1 | | 6.7 | 1.9 | |
| Delay (s) | 14.0 | 16.3 | | | 16.6 | | 13.7 | 25.3 | | 19.7 | 17.6 | |
| Level of Service | B | B | | | B | | B | C | | B | B | |
| Approach Delay (s) | | 16.2 | | | 16.6 | | | 24.6 | | | 17.8 | |
| Approach LOS | | B | | | B | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 20.7 | | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.61 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 68.0 | | | Sum of lost time (s) | | | 11.0 | | | | |
| Intersection Capacity Utilization | | 92.1% | | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
8: Key Blvd & Elm St

6/7/2012

| Movement | EBL | EBR | NBL | NBT | SBT | SBR | SBR2 | NEL | NER |
|-----------------------------------|-------|-------|------|----------------------|-------|------|------|-------|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 0 | 118 | 291 | 112 | 133 | 0 | 4 | 176 | 101 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | | 4.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | | | 0.99 | 1.00 | | | 1.00 | 1.00 |
| Fr _t | 0.86 | | | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Fl _t Protected | 1.00 | | | 0.97 | 1.00 | | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1611 | | | 1783 | 1856 | | | 1770 | 1583 |
| Fl _t Permitted | 1.00 | | | 0.65 | 1.00 | | | 0.95 | 1.00 |
| Satd. Flow (perm) | 1611 | | | 1196 | 1856 | | | 1770 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 128 | 316 | 122 | 145 | 0 | 4 | 191 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 92 |
| Lane Group Flow (vph) | 128 | 0 | 0 | 438 | 148 | 0 | 0 | 191 | 18 |
| Confl. Peds. (#/hr) | | | | 5 | | | | 2 | |
| Turn Type | | | | Perm | | | | Perm | |
| Protected Phases | 3 | | | 4 2 | 7 2 | | | 8 | |
| Permitted Phases | | | | 4 2 | | | | 8 | |
| Actuated Green, G (s) | 16.0 | | | 32.0 | 32.0 | | | 16.0 | 16.0 |
| Effective Green, g (s) | 16.0 | | | 32.0 | 32.0 | | | 16.0 | 16.0 |
| Actuated g/C Ratio | 0.16 | | | 0.32 | 0.32 | | | 0.16 | 0.16 |
| Clearance Time (s) | 4.0 | | | | | | 4.0 | 4.0 | |
| Lane Grp Cap (vph) | 258 | | | 383 | 594 | | | 283 | 253 |
| v/s Ratio Prot | c0.08 | | | | c0.08 | | | c0.11 | |
| v/s Ratio Perm | | | | c0.37 | | | | 0.01 | |
| v/c Ratio | 0.50 | | | 1.14 | 0.25 | | | 0.67 | 0.07 |
| Uniform Delay, d1 | 38.3 | | | 34.0 | 25.1 | | | 39.6 | 35.7 |
| Progression Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 6.7 | | | 91.2 | 1.0 | | | 12.2 | 0.5 |
| Delay (s) | 45.0 | | | 125.2 | 26.1 | | | 51.7 | 36.2 |
| Level of Service | D | | | F | C | | | D | D |
| Approach Delay (s) | 45.0 | | | 125.2 | 26.1 | | | 46.1 | |
| Approach LOS | D | | | F | C | | | D | |
| Intersection Summary | | | | | | | | | |
| HCM Average Control Delay | | 77.1 | | HCM Level of Service | | | | E | |
| HCM Volume to Capacity ratio | | 0.74 | | | | | | | |
| Actuated Cycle Length (s) | | 100.0 | | Sum of lost time (s) | | | | 20.0 | |
| Intersection Capacity Utilization | | 59.6% | | ICU Level of Service | | | | B | |
| Analysis Period (min) | | 15 | | | | | | | |
| c Critical Lane Group | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
9: Potrero Ave & Richmond St

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 51 | 142 | 60 | 31 | 82 | 18 | 39 | 337 | 23 | 16 | 197 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Flt Protected | 0.97 | | | | 0.98 | | | 0.99 | | | 0.98 | |
| Flt Permitted | 0.99 | | | | 0.99 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1785 | | | | 1806 | | | 1839 | | | 1829 | |
| Flt Permitted | 0.99 | | | | 0.99 | | | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | 1759 | | | | 1759 | | | 1759 | | | 1769 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 55 | 154 | 65 | 34 | 89 | 20 | 42 | 366 | 25 | 17 | 214 | 29 |
| RTOR Reduction (vph) | 0 | 28 | 0 | 0 | 12 | 0 | 0 | 5 | 0 | 0 | 11 | 0 |
| Lane Group Flow (vph) | 0 | 246 | 0 | 0 | 131 | 0 | 0 | 428 | 0 | 0 | 249 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 16.0 | | | 16.0 | | | 16.0 | | | 16.0 | | |
| Effective Green, g (s) | 16.0 | | | 16.0 | | | 16.0 | | | 16.0 | | |
| Actuated g/C Ratio | 0.40 | | | 0.40 | | | 0.40 | | | 0.40 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Lane Grp Cap (vph) | 666 | | | 656 | | | 704 | | | 708 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.15 | | | 0.08 | | | c0.24 | | | 0.14 | | |
| v/c Ratio | 0.37 | | | 0.20 | | | 0.61 | | | 0.35 | | |
| Uniform Delay, d1 | 8.4 | | | 7.8 | | | 9.5 | | | 8.4 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.49 | | | 1.00 | | |
| Incremental Delay, d2 | 1.6 | | | 0.7 | | | 3.3 | | | 1.4 | | |
| Delay (s) | 10.0 | | | 8.5 | | | 17.5 | | | 9.7 | | |
| Level of Service | B | | | A | | | B | | | A | | |
| Approach Delay (s) | 10.0 | | | 8.5 | | | 17.5 | | | 9.7 | | |
| Approach LOS | B | | | A | | | B | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 12.7 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.49 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 40.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 55.2% | | | ICU Level of Service | | | B | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
10: Moeser Ln & Richmond St

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 27 | 198 | 11 | 26 | 182 | 116 | 26 | 322 | 26 | 79 | 241 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Frpb, ped/bikes | 1.00 | | | | | 0.99 | | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr | 0.99 | | | | | 0.95 | | | 0.99 | | | 0.99 |
| Flt Protected | 0.99 | | | | | 1.00 | | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | | 1836 | | | | 1741 | | | 1836 | | | 1814 |
| Flt Permitted | | 0.94 | | | | 0.96 | | | 0.96 | | | 0.86 |
| Satd. Flow (perm) | | 1736 | | | | 1686 | | | 1769 | | | 1585 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 29 | 215 | 12 | 28 | 198 | 126 | 28 | 350 | 28 | 86 | 262 | 37 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 50 | 0 | 0 | 7 | 0 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 0 | 252 | 0 | 0 | 302 | 0 | 0 | 399 | 0 | 0 | 375 | 0 |
| Confl. Peds. (#/hr) | 15 | | 7 | 7 | | 15 | 2 | | 2 | 2 | | 2 |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | | 16.0 | | | 16.0 | | | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | 16.0 | | | 16.0 | | | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | 0.40 | | | 0.40 | | | 0.40 | | | 0.40 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 694 | | | 674 | | | 708 | | | 634 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.15 | | | c0.18 | | | 0.23 | | | c0.24 | | |
| v/c Ratio | 0.36 | | | 0.45 | | | 0.56 | | | 0.59 | | |
| Uniform Delay, d1 | 8.4 | | | 8.8 | | | 9.3 | | | 9.4 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 0.76 | | |
| Incremental Delay, d2 | 1.5 | | | 2.1 | | | 3.2 | | | 3.9 | | |
| Delay (s) | 9.9 | | | 10.9 | | | 12.5 | | | 11.1 | | |
| Level of Service | A | | | B | | | B | | | B | | |
| Approach Delay (s) | 9.9 | | | 10.9 | | | 12.5 | | | 11.1 | | |
| Approach LOS | A | | | B | | | B | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 11.2 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.52 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 40.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 69.8% | | | ICU Level of Service | | | C | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 11: Central Ave & Richmond St 6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|------|----------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 94 | 191 | 40 | 3 | 95 | 38 | 35 | 206 | 8 | 36 | 172 | 85 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 102 | 208 | 43 | 3 | 103 | 41 | 38 | 224 | 9 | 39 | 187 | 92 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total (vph) | 353 | 148 | 271 | 318 | | | | | | | | |
| Volume Left (vph) | 102 | 3 | 38 | 39 | | | | | | | | |
| Volume Right (vph) | 43 | 41 | 9 | 92 | | | | | | | | |
| Hadj (s) | 0.02 | -0.13 | 0.04 | -0.12 | | | | | | | | |
| Departure Headway (s) | 6.1 | 6.4 | 6.2 | 6.0 | | | | | | | | |
| Degree Utilization, x | 0.60 | 0.26 | 0.47 | 0.53 | | | | | | | | |
| Capacity (veh/h) | 548 | 473 | 529 | 560 | | | | | | | | |
| Control Delay (s) | 17.6 | 11.7 | 14.5 | 15.4 | | | | | | | | |
| Approach Delay (s) | 17.6 | 11.7 | 14.5 | 15.4 | | | | | | | | |
| Approach LOS | C | B | B | C | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | | | 15.4 | | | | | | | |
| HCM Level of Service | | | | | C | | | | | | | |
| Intersection Capacity Utilization | | | | 60.9% | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | | 15 | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 12: Fairmont Ave & Richmond St

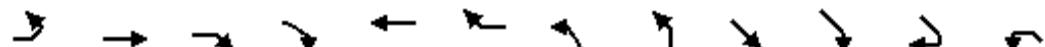
6/7/2012



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|-------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | |
| Sign Control | | Stop | Stop | | Stop | |
| Volume (vph) | 122 | 331 | 283 | 96 | 102 | 96 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 133 | 360 | 308 | 104 | 111 | 104 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total (vph) | 492 | 412 | 215 | | | |
| Volume Left (vph) | 133 | 0 | 111 | | | |
| Volume Right (vph) | 0 | 104 | 104 | | | |
| Hadj (s) | 0.09 | -0.12 | -0.15 | | | |
| Departure Headway (s) | 5.3 | 5.2 | 6.0 | | | |
| Degree Utilization, x | 0.72 | 0.59 | 0.36 | | | |
| Capacity (veh/h) | 665 | 672 | 541 | | | |
| Control Delay (s) | 20.6 | 15.4 | 12.3 | | | |
| Approach Delay (s) | 20.6 | 15.4 | 12.3 | | | |
| Approach LOS | C | C | B | | | |
| Intersection Summary | | | | | | |
| Delay | | 17.1 | | | | |
| HCM Level of Service | | C | | | | |
| Intersection Capacity Utilization | 70.4% | | ICU Level of Service | | C | |
| Analysis Period (min) | | 15 | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 13: Fairmont Ave & Colusa Ave

6/7/2012



| Movement | EBL | EBT | EBR | EBR2 | WBT | WBR | NBL2 | NBL | SET | SER | SER2 | NWL2 |
|------------------------|-------|------|------|------|------|------|------|------|------|------|--------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 138 | 5 | 176 | 4 | 11 | 1 | 7 | 19 | 117 | 16 | 77 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | 1.00 | 0.95 | | 0.95 | |
| Fr _t | 0.92 | | | | 0.99 | | | 1.00 | 0.98 | | 0.85 | |
| Flt Protected | 0.98 | | | | 1.00 | | | 0.95 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | 1687 | | | | 1843 | | | 1770 | 1726 | | 1504 | |
| Flt Permitted | 0.86 | | | | 1.00 | | | 0.95 | 1.00 | | 1.00 | |
| Satd. Flow (perm) | 1474 | | | | 1843 | | | 1770 | 1726 | | 1504 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 150 | 5 | 191 | 4 | 12 | 1 | 8 | 21 | 127 | 17 | 84 | 1 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 49 | 0 |
| Lane Group Flow (vph) | 0 | 349 | 0 | 0 | 12 | 0 | 0 | 29 | 149 | 0 | 27 | 0 |
| Turn Type | Perm | | | | | | | Perm | | | custom | Perm |
| Protected Phases | | 6! | | | | 2! | | | 4 | 8 | | |
| Permitted Phases | | 6! | | | | | | 4 | | 8 | | 6 8 |
| Actuated Green, G (s) | 15.2 | | | | 15.2 | | | 1.1 | 13.2 | | 15.2 | |
| Effective Green, g (s) | 15.2 | | | | 15.2 | | | 1.1 | 13.2 | | 15.2 | |
| Actuated g/C Ratio | 0.35 | | | | 0.35 | | | 0.03 | 0.31 | | 0.35 | |
| Clearance Time (s) | 4.5 | | | | 4.5 | | | 4.5 | 4.5 | | 4.5 | |
| Vehicle Extension (s) | 3.0 | | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 521 | | | | 651 | | | 45 | 530 | | 532 | |
| v/s Ratio Prot | | | | | 0.01 | | | | 0.09 | | | |
| v/s Ratio Perm | c0.24 | | | | | | | 0.02 | | | 0.02 | |
| v/c Ratio | 0.67 | | | | 0.02 | | | 0.64 | 0.28 | | 0.05 | |
| Uniform Delay, d1 | 11.8 | | | | 9.0 | | | 20.8 | 11.3 | | 9.1 | |
| Progression Factor | 1.00 | | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 3.4 | | | | 0.0 | | | 27.5 | 0.3 | | 0.0 | |
| Delay (s) | 15.2 | | | | 9.1 | | | 48.2 | 11.6 | | 9.2 | |
| Level of Service | B | | | | A | | | D | B | | A | |
| Approach Delay (s) | 15.2 | | | | 9.1 | | | 48.2 | 10.8 | | | |
| Approach LOS | B | | | | A | | | D | B | | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 14.4 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.63 | | |
| Actuated Cycle Length (s) | 43.0 | Sum of lost time (s) | 13.5 |
| Intersection Capacity Utilization | 65.0% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |

! Phase conflict between lane groups.

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak
 13: Fairmont Ave & Colusa Ave

6/7/2012



| Movement | NWL | NWT |
|------------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | 201 | 235 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Total Lost time (s) | 4.5 | 4.5 |
| Lane Util. Factor | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 |
| Flt Permitted | 0.66 | 1.00 |
| Satd. Flow (perm) | 1221 | 1863 |
| Peak-hour factor, PHF | 0.92 | 0.92 |
| Adj. Flow (vph) | 218 | 255 |
| RTOR Reduction (vph) | 0 | 0 |
| Lane Group Flow (vph) | 219 | 255 |
| Turn Type | Perm | |
| Protected Phases | 8 | |
| Permitted Phases | 8 | |
| Actuated Green, G (s) | 13.2 | 13.2 |
| Effective Green, g (s) | 13.2 | 13.2 |
| Actuated g/C Ratio | 0.31 | 0.31 |
| Clearance Time (s) | 4.5 | 4.5 |
| Vehicle Extension (s) | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 375 | 572 |
| v/s Ratio Prot | 0.14 | |
| v/s Ratio Perm | 0.18 | |
| v/c Ratio | 0.58 | 0.45 |
| Uniform Delay, d1 | 12.6 | 12.0 |
| Progression Factor | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.3 | 0.6 |
| Delay (s) | 14.9 | 12.5 |
| Level of Service | B | B |
| Approach Delay (s) | 13.6 | |
| Approach LOS | B | |

Intersection Summary

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 1: MacDonald Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|------|----------------------|-------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑↑ | |
| Volume (vph) | 19 | 548 | 79 | 123 | 294 | 33 | 125 | 43 | 163 | 40 | 69 | 24 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3415 | 1863 | 1554 | 1767 | 1831 | | 1770 | 3539 | 1542 | 1764 | 4860 | |
| Flt Permitted | 0.55 | 1.00 | 1.00 | 0.33 | 1.00 | | 0.69 | 1.00 | 1.00 | 0.72 | 1.00 | |
| Satd. Flow (perm) | 1971 | 1863 | 1554 | 610 | 1831 | | 1277 | 3539 | 1542 | 1346 | 4860 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 21 | 596 | 86 | 134 | 320 | 36 | 136 | 47 | 177 | 43 | 75 | 26 |
| RTOR Reduction (vph) | 0 | 0 | 48 | 0 | 9 | 0 | 0 | 0 | 130 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 21 | 596 | 38 | 134 | 347 | 0 | 136 | 47 | 47 | 43 | 82 | 0 |
| Confl. Peds. (#/hr) | 10 | | 6 | 6 | | 10 | | | 4 | 4 | | |
| Confl. Bikes (#/hr) | | | 7 | | | 2 | | | 2 | | | 2 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 12.2 | 12.2 | 12.2 | 12.2 | 12.2 | | 7.4 | 7.4 | 7.4 | 7.4 | 7.4 | |
| Effective Green, g (s) | 12.2 | 12.2 | 12.2 | 12.2 | 12.2 | | 7.4 | 7.4 | 7.4 | 7.4 | 7.4 | |
| Actuated g/C Ratio | 0.44 | 0.44 | 0.44 | 0.44 | 0.44 | | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 871 | 824 | 687 | 270 | 809 | | 342 | 949 | 413 | 361 | 1303 | |
| v/s Ratio Prot | | c0.32 | | | 0.19 | | | 0.01 | | | 0.02 | |
| v/s Ratio Perm | 0.01 | | 0.02 | 0.22 | | | c0.11 | | 0.03 | 0.03 | | |
| v/c Ratio | 0.02 | 0.72 | 0.06 | 0.50 | 0.43 | | 0.40 | 0.05 | 0.11 | 0.12 | 0.06 | |
| Uniform Delay, d1 | 4.3 | 6.3 | 4.4 | 5.5 | 5.3 | | 8.3 | 7.5 | 7.6 | 7.6 | 7.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 3.2 | 0.0 | 1.4 | 0.4 | | 0.8 | 0.0 | 0.1 | 0.1 | 0.0 | |
| Delay (s) | 4.4 | 9.5 | 4.4 | 6.9 | 5.7 | | 9.0 | 7.5 | 7.8 | 7.8 | 7.5 | |
| Level of Service | A | A | A | A | A | | A | A | A | A | A | |
| Approach Delay (s) | | 8.7 | | | 6.0 | | | 8.2 | | | 7.6 | |
| Approach LOS | | A | | | A | | | A | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 7.7 | | | | HCM Level of Service | | | A | | | |
| HCM Volume to Capacity ratio | | 0.60 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 27.6 | | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | 59.2% | | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
2: Cutting Blvd & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|--------|-------|----------------------|------|--------|-------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 184 | 0 | 750 | 561 | 239 | 48 | 330 | 645 | 0 | 0 | 476 | 161 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | | | 0.95 | 1.00 |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | 3433 | 5085 | | | 3539 | 1583 |
| Flt Permitted | 0.59 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 1101 | | 2787 | 3433 | 3539 | 1583 | 3526 | 5085 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 200 | 0 | 815 | 610 | 260 | 52 | 359 | 701 | 0 | 0 | 517 | 175 |
| RTOR Reduction (vph) | 0 | 0 | 154 | 0 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 132 |
| Lane Group Flow (vph) | 200 | 0 | 661 | 610 | 260 | 16 | 359 | 701 | 0 | 0 | 517 | 43 |
| Turn Type | custom | | custom | Perm | | Perm | custom | | | | Perm | |
| Protected Phases | | | | | 3 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 5 | 3 | | 3 | 5 | | | | 6 | |
| Actuated Green, G (s) | 12.3 | | 19.9 | 20.6 | 20.6 | 20.6 | 4.1 | 23.6 | | | 16.5 | 16.5 |
| Effective Green, g (s) | 12.3 | | 19.9 | 20.6 | 20.6 | 20.6 | 4.1 | 23.6 | | | 16.5 | 16.5 |
| Actuated g/C Ratio | 0.18 | | 0.29 | 0.31 | 0.31 | 0.31 | 0.06 | 0.35 | | | 0.24 | 0.24 |
| Clearance Time (s) | 3.5 | | | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 201 | | 822 | 1048 | 1080 | 483 | 214 | 1778 | | | 865 | 387 |
| v/s Ratio Prot | | | | | 0.07 | | | 0.14 | | | c0.15 | |
| v/s Ratio Perm | c0.18 | | 0.24 | c0.18 | | 0.01 | c0.10 | | | | 0.03 | |
| v/c Ratio | 1.00 | | 0.80 | 0.58 | 0.24 | 0.03 | 1.68 | 0.39 | | | 0.60 | 0.11 |
| Uniform Delay, d1 | 27.6 | | 22.0 | 19.8 | 17.6 | 16.5 | 31.7 | 16.6 | | | 22.6 | 19.8 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 61.7 | | 5.8 | 0.8 | 0.1 | 0.0 | 324.5 | 0.1 | | | 1.1 | 0.1 |
| Delay (s) | 89.3 | | 27.8 | 20.6 | 17.7 | 16.5 | 356.2 | 16.7 | | | 23.7 | 19.9 |
| Level of Service | F | | C | C | B | B | F | B | | | C | B |
| Approach Delay (s) | 39.9 | | | | 19.6 | | | 131.7 | | | 22.7 | |
| Approach LOS | D | | | | B | | | F | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 58.0 | | | | HCM Level of Service | | | E | | | | |
| HCM Volume to Capacity ratio | 0.77 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 67.5 | | | | Sum of lost time (s) | | | 14.0 | | | | |
| Intersection Capacity Utilization | 65.4% | | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|-----------------------------------|-------|------|----------------------|------|------|------|-------|------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 15 | 31 | 22 | 2 | 40 | 37 | 4 | 66 | 31 | 7 | 714 | 86 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.98 | 1.00 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1833 | 1583 | | | | | 1778 | 1583 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.24 | 1.00 | | | | | 0.70 | 1.00 | | 0.10 | 1.00 | 1.00 |
| Satd. Flow (perm) | 442 | 1583 | | | | | 1303 | 1583 | | 177 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 16 | 34 | 24 | 2 | 43 | 40 | 4 | 72 | 34 | 8 | 776 | 93 |
| RTOR Reduction (vph) | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 66 | 0 | 0 | 0 | 60 |
| Lane Group Flow (vph) | 0 | 50 | 24 | 0 | 0 | 0 | 87 | 6 | 0 | 42 | 776 | 33 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | pm+pt | pm+pt | | Perm |
| Protected Phases | | 3 | | | | | | 7 | | 5 | 5 | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | 2 |
| Actuated Green, G (s) | 12.3 | 12.3 | | | | | 10.3 | 10.3 | | 49.5 | 42.0 | 42.0 |
| Effective Green, g (s) | 12.3 | 12.3 | | | | | 10.3 | 10.3 | | 49.5 | 42.0 | 42.0 |
| Actuated g/C Ratio | 0.10 | 0.10 | | | | | 0.09 | 0.09 | | 0.42 | 0.35 | 0.35 |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 46 | 164 | | | | | 113 | 137 | | 174 | 1251 | 560 |
| v/s Ratio Prot | | | | | | | | | | 0.02 | 0.22 | |
| v/s Ratio Perm | c0.11 | 0.02 | | | | | c0.07 | 0.00 | | 0.08 | 0.02 | |
| v/c Ratio | 1.09 | 0.15 | | | | | 0.77 | 0.05 | | 0.24 | 0.62 | 0.06 |
| Uniform Delay, d1 | 53.2 | 48.5 | | | | | 53.1 | 49.7 | | 26.9 | 31.8 | 25.4 |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 159.3 | 0.4 | | | | | 26.5 | 0.1 | | 0.7 | 1.0 | 0.0 |
| Delay (s) | 212.5 | 48.9 | | | | | 79.6 | 49.9 | | 27.6 | 32.8 | 25.4 |
| Level of Service | F | D | | | | | E | D | | C | C | C |
| Approach Delay (s) | 156.6 | | | | | | 66.1 | | | | 31.8 | |
| Approach LOS | F | | | | | | E | | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 77.6 | | HCM Level of Service | | | | | | | E | | |
| HCM Volume to Capacity ratio | 1.02 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 118.8 | | Sum of lost time (s) | | | | | | 20.0 | | | |
| Intersection Capacity Utilization | 88.8% | | ICU Level of Service | | | | | | E | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | | | ↑↑ | | ↑ |
| Volume (vph) | 527 | 1311 | 351 | 9 | 12 | 156 | 111 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | | | | 0.97 | | 1.00 |
| Fr _t | 1.00 | 0.97 | | | | 0.94 | | 0.85 |
| Flt Protected | 0.95 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | 3433 | 3425 | | | | 3299 | | 1583 |
| Flt Permitted | 0.18 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | 659 | 3425 | | | | 3299 | | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 573 | 1425 | 382 | 10 | 13 | 170 | 121 | 16 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Lane Group Flow (vph) | 573 | 1817 | 0 | 0 | 0 | 304 | 0 | 2 |
| Turn Type | pm+pt | | | | Perm | | Perm | |
| Protected Phases | 1 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | 64.0 | 53.5 | | | | 16.2 | | 16.2 |
| Effective Green, g (s) | 64.0 | 53.5 | | | | 16.2 | | 16.2 |
| Actuated g/C Ratio | 0.54 | 0.45 | | | | 0.14 | | 0.14 |
| Clearance Time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 775 | 1542 | | | | 450 | | 216 |
| v/s Ratio Prot | c0.11 | c0.53 | | | | | | |
| v/s Ratio Perm | 0.29 | | | | | 0.09 | | 0.00 |
| v/c Ratio | 0.74 | 1.18 | | | | 0.68 | | 0.01 |
| Uniform Delay, d1 | 19.0 | 32.6 | | | | 48.8 | | 44.4 |
| Progression Factor | 1.00 | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 3.7 | 87.3 | | | | 4.0 | | 0.0 |
| Delay (s) | 22.7 | 120.0 | | | | 52.8 | | 44.4 |
| Level of Service | C | F | | | | D | | D |
| Approach Delay (s) | | 96.7 | | | | 52.4 | | |
| Approach LOS | | F | | | | D | | |

Intersection Summary

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
4: Potrero Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|-------|------|------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 47 | 266 | 178 | 100 | 373 | 340 | 122 | 404 | 14 | 562 | 794 | 32 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3286 | | 1770 | 3522 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.26 | 1.00 | 1.00 | 0.42 | 1.00 | | 0.26 | 1.00 | | 0.45 | 1.00 | 1.00 |
| Satd. Flow (perm) | 481 | 1863 | 1583 | 791 | 3286 | | 484 | 3522 | | 841 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 51 | 289 | 193 | 109 | 405 | 370 | 133 | 439 | 15 | 611 | 863 | 35 |
| RTOR Reduction (vph) | 0 | 0 | 137 | 0 | 262 | 0 | 0 | 3 | 0 | 0 | 0 | 19 |
| Lane Group Flow (vph) | 51 | 289 | 56 | 109 | 513 | 0 | 133 | 451 | 0 | 611 | 863 | 16 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | | 26.5 | 22.6 | | 28.9 | 23.8 | 23.8 |
| Effective Green, g (s) | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 | | 26.5 | 22.6 | | 28.9 | 23.8 | 23.8 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | | 0.50 | 0.42 | | 0.54 | 0.45 | 0.45 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 140 | 543 | 461 | 230 | 957 | | 335 | 1496 | | 546 | 1583 | 708 |
| v/s Ratio Prot | | 0.16 | | c0.16 | | | 0.03 | 0.13 | | c0.11 | 0.24 | |
| v/s Ratio Perm | 0.11 | | 0.04 | 0.14 | | | 0.17 | | | c0.50 | | 0.01 |
| v/c Ratio | 0.36 | 0.53 | 0.12 | 0.47 | 0.54 | | 0.40 | 0.30 | | 1.12 | 0.55 | 0.02 |
| Uniform Delay, d1 | 14.9 | 15.8 | 13.9 | 15.5 | 15.8 | | 7.5 | 10.1 | | 10.9 | 10.7 | 8.2 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.6 | 1.0 | 0.1 | 1.5 | 0.6 | | 0.8 | 0.1 | | 75.5 | 0.4 | 0.0 |
| Delay (s) | 16.6 | 16.8 | 14.0 | 17.0 | 16.4 | | 8.3 | 10.2 | | 86.4 | 11.1 | 8.2 |
| Level of Service | B | B | B | B | B | | A | B | | F | B | A |
| Approach Delay (s) | | 15.8 | | | 16.5 | | | 9.8 | | | 41.5 | |
| Approach LOS | | B | | | B | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 26.0 | | HCM Level of Service | | | C | | | | | |
| HCM Volume to Capacity ratio | | 0.92 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 53.2 | | Sum of lost time (s) | | | 9.0 | | | | | |
| Intersection Capacity Utilization | | 89.0% | | ICU Level of Service | | | E | | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
5: Moeser Ln & San Pablo Ave

6/7/2012



| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|-------|----------------------|-------|-------|-------|
| Lane Configurations | ↑ ↗ | ↑ ↗ | ↗ ↘ | ↑ ↗ ↘ | | ↑ ↗ | ↑ ↗ ↘ |
| Volume (vph) | 311 | 333 | 33 | 456 | 94 | 629 | 785 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 |
| Frpb, ped/bikes | 1.00 | 0.98 | 1.00 | 0.99 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1546 | 1770 | 3429 | | 1767 | 3539 |
| Fl _t Permitted | 0.95 | 1.00 | 0.30 | 1.00 | | 0.35 | 1.00 |
| Satd. Flow (perm) | 1770 | 1546 | 556 | 3429 | | 645 | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 338 | 362 | 36 | 496 | 102 | 684 | 853 |
| RTOR Reduction (vph) | 0 | 213 | 0 | 24 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 338 | 149 | 36 | 574 | 0 | 684 | 853 |
| Confl. Peds. (#/hr) | 1 | 20 | | | 10 | 10 | |
| Confl. Bikes (#/hr) | | | | | 2 | | |
| Turn Type | | Perm | pm+pt | | pm+pt | | |
| Protected Phases | 4 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | 4 | 2 | | | 6 | |
| Actuated Green, G (s) | 14.7 | 14.7 | 23.7 | 22.2 | | 28.7 | 24.7 |
| Effective Green, g (s) | 14.7 | 14.7 | 23.7 | 22.2 | | 28.7 | 24.7 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.47 | 0.44 | | 0.56 | 0.49 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 511 | 446 | 295 | 1496 | | 452 | 1717 |
| v/s Ratio Prot | c0.19 | | 0.00 | 0.17 | | c0.12 | 0.24 |
| v/s Ratio Perm | | 0.10 | 0.05 | | | c0.73 | |
| v/c Ratio | 0.66 | 0.33 | 0.12 | 0.38 | | 1.51 | 0.50 |
| Uniform Delay, d1 | 15.9 | 14.2 | 7.5 | 9.7 | | 10.3 | 8.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.2 | 0.4 | 0.2 | 0.2 | | 242.2 | 0.2 |
| Delay (s) | 19.1 | 14.7 | 7.7 | 9.9 | | 252.5 | 9.1 |
| Level of Service | B | B | A | A | | F | A |
| Approach Delay (s) | 16.8 | | | 9.8 | | | 117.4 |
| Approach LOS | B | | | A | | F | |
| Intersection Summary | | | | | | | |
| HCM Average Control Delay | | 69.1 | | HCM Level of Service | | E | |
| HCM Volume to Capacity ratio | | 1.27 | | | | | |
| Actuated Cycle Length (s) | | 50.9 | | Sum of lost time (s) | | 9.0 | |
| Intersection Capacity Utilization | | 80.9% | | ICU Level of Service | | D | |
| Analysis Period (min) | | 15 | | | | | |
| c Critical Lane Group | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
6: Central Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---|------|-------|------|------|----------------------|------|-------|------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | |
| Volume (vph) | 134 | 252 | 94 | 101 | 283 | 35 | 18 | 458 | 69 | 35 | 601 | 183 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1681 | 1765 | 1583 | | 3453 | | 1770 | 3470 | | 1770 | 3415 | |
| Flt Permitted | 0.49 | 0.97 | 1.00 | | 0.55 | | 0.16 | 1.00 | | 0.30 | 1.00 | |
| Satd. Flow (perm) | 866 | 1712 | 1583 | | 1925 | | 290 | 3470 | | 553 | 3415 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 146 | 274 | 102 | 110 | 308 | 38 | 20 | 498 | 75 | 38 | 653 | 199 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 6 | 0 | 0 | 11 | 0 | 0 | 25 | 0 |
| Lane Group Flow (vph) | 131 | 289 | 24 | 0 | 450 | 0 | 20 | 562 | 0 | 38 | 827 | 0 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | |
| Protected Phases | | 4 | | | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 3 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 20.5 | 20.5 | 20.5 | | 24.3 | | 27.7 | 25.7 | | 27.9 | 25.8 | |
| Effective Green, g (s) | 20.5 | 20.5 | 20.5 | | 24.3 | | 27.7 | 25.7 | | 27.9 | 25.8 | |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | | 0.28 | | 0.32 | 0.30 | | 0.32 | 0.30 | |
| Clearance Time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 206 | 408 | 377 | | 543 | | 128 | 1036 | | 209 | 1023 | |
| v/s Ratio Prot | | | | | | | 0.00 | 0.16 | | c0.00 | c0.24 | |
| v/s Ratio Perm | 0.15 | c0.17 | 0.02 | | c0.23 | | 0.05 | | | 0.05 | | |
| v/c Ratio | 0.64 | 0.71 | 0.06 | | 1.17dl | | 0.16 | 0.54 | | 0.18 | 0.81 | |
| Uniform Delay, d1 | 29.4 | 30.1 | 25.4 | | 28.9 | | 21.5 | 25.3 | | 20.5 | 27.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 6.3 | 5.6 | 0.1 | | 10.0 | | 0.6 | 0.6 | | 0.4 | 4.8 | |
| Delay (s) | 35.7 | 35.6 | 25.5 | | 39.0 | | 22.1 | 25.9 | | 20.9 | 32.6 | |
| Level of Service | D | D | C | | D | | C | C | | C | C | |
| Approach Delay (s) | | 33.7 | | | 39.0 | | | 25.7 | | | 32.1 | |
| Approach LOS | | C | | | D | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 32.2 | | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.73 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 86.1 | | | Sum of lost time (s) | | | 9.5 | | | | |
| Intersection Capacity Utilization | | 64.2% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| dl Defacto Left Lane. Recode with 1 though lane as a left lane. | | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 7: Fairmont Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|-------|------|------|-------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 2 | 215 | 13 | 87 | 196 | 105 | 22 | 336 | 72 | 99 | 691 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 0.99 | 1.00 | |
| Fr _t | 1.00 | 0.99 | | | 0.96 | | 1.00 | 0.97 | | 1.00 | 1.00 | |
| Fl _t Protected | 0.95 | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1745 | 1844 | | | 3317 | | 1769 | 3407 | | 1754 | 3523 | |
| Fl _t Permitted | 0.45 | 1.00 | | | 0.77 | | 0.36 | 1.00 | | 0.44 | 1.00 | |
| Satd. Flow (perm) | 831 | 1844 | | | 2571 | | 669 | 3407 | | 807 | 3523 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 234 | 14 | 95 | 213 | 114 | 24 | 365 | 78 | 108 | 751 | 21 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 63 | 0 | 0 | 24 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 2 | 244 | 0 | 0 | 359 | 0 | 24 | 419 | 0 | 108 | 770 | 0 |
| Confl. Peds. (#/hr) | 43 | | 22 | 22 | | 43 | 10 | | 37 | 37 | | 10 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | | | pm+pt | | | pm+pt | | | |
| Protected Phases | | 4 | | | 8 | | 1 | 6 | | 5 | | 2 |
| Permitted Phases | 4 | | | 8 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 12.5 | 12.5 | | | 12.5 | | 23.6 | 22.9 | | 29.7 | 26.0 | |
| Effective Green, g (s) | 12.5 | 12.5 | | | 12.5 | | 23.6 | 22.9 | | 29.7 | 26.0 | |
| Actuated g/C Ratio | 0.25 | 0.25 | | | 0.25 | | 0.47 | 0.46 | | 0.59 | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 207 | 459 | | | 640 | | 330 | 1554 | | 549 | 1825 | |
| v/s Ratio Prot | | 0.13 | | | | | 0.00 | 0.12 | | c0.01 | c0.22 | |
| v/s Ratio Perm | 0.00 | | | c0.14 | | | 0.03 | | | 0.10 | | |
| v/c Ratio | 0.01 | 0.53 | | | 0.56 | | 0.07 | 0.27 | | 0.20 | 0.42 | |
| Uniform Delay, d1 | 14.2 | 16.3 | | | 16.5 | | 7.1 | 8.5 | | 4.6 | 7.5 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 1.2 | | | 1.1 | | 0.1 | 0.1 | | 0.2 | 0.2 | |
| Delay (s) | 14.2 | 17.5 | | | 17.6 | | 7.2 | 8.6 | | 4.7 | 7.6 | |
| Level of Service | B | B | | | B | | A | A | | A | A | |
| Approach Delay (s) | | 17.5 | | | 17.6 | | | 8.5 | | | 7.3 | |
| Approach LOS | | B | | | B | | | A | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 11.0 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.43 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 50.2 | | | Sum of lost time (s) | | | 7.0 | | | | |
| Intersection Capacity Utilization | | 72.9% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
8: Key Blvd & Elm St

6/7/2012



| Movement | EBL | EBR | NBL | NBT | SBT | SBR | SBR2 | NEL | NER |
|-----------------------------------|-------|------|-------|-------|----------------------|------|------|-------|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 2 | 179 | 179 | 48 | 188 | 0 | 4 | 115 | 101 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.5 | | | 5.5 | 5.5 | | | 5.5 | 5.5 |
| Lane Util. Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frt | 0.87 | | | | 1.00 | 1.00 | | 1.00 | 0.85 |
| Flt Protected | 1.00 | | | | 0.96 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1613 | | | | 1784 | 1857 | | 1770 | 1583 |
| Flt Permitted | 1.00 | | | | 0.57 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | 1613 | | | | 1054 | 1857 | | 1770 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 195 | 195 | 52 | 204 | 0 | 4 | 125 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 96 |
| Lane Group Flow (vph) | 197 | 0 | 0 | 247 | 207 | 0 | 0 | 125 | 14 |
| Confl. Peds. (#/hr) | | | | 3 | | | 3 | | |
| Confl. Bikes (#/hr) | | | | | | | 2 | | |
| Turn Type | | | | Perm | | | | Perm | |
| Protected Phases | 3 | | | 4 2 | 7 2 | | | 8 | |
| Permitted Phases | | | | 4 2 | | | | 8 | |
| Actuated Green, G (s) | 15.2 | | | | 30.6 | 27.0 | | 11.9 | 11.9 |
| Effective Green, g (s) | 15.2 | | | | 30.6 | 27.0 | | 11.9 | 11.9 |
| Actuated g/C Ratio | 0.16 | | | | 0.32 | 0.28 | | 0.12 | 0.12 |
| Clearance Time (s) | 5.5 | | | | | | 5.5 | 5.5 | |
| Vehicle Extension (s) | 3.0 | | | | | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 258 | | | 339 | 527 | | | 221 | 198 |
| v/s Ratio Prot | c0.12 | | | | c0.11 | | | c0.07 | |
| v/s Ratio Perm | | | | c0.23 | | | | 0.01 | |
| v/c Ratio | 0.76 | | | 0.73 | 0.39 | | | 0.57 | 0.07 |
| Uniform Delay, d1 | 38.3 | | | 28.6 | 27.5 | | | 39.2 | 36.8 |
| Progression Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 12.6 | | | 7.6 | 0.5 | | | 3.3 | 0.1 |
| Delay (s) | 50.9 | | | 36.2 | 28.0 | | | 42.5 | 36.9 |
| Level of Service | D | | | D | C | | | D | D |
| Approach Delay (s) | 50.9 | | | 36.2 | 28.0 | | | 39.9 | |
| Approach LOS | D | | | D | C | | | D | |
| Intersection Summary | | | | | | | | | |
| HCM Average Control Delay | | | 38.5 | | HCM Level of Service | | | D | |
| HCM Volume to Capacity ratio | | | 0.67 | | | | | | |
| Actuated Cycle Length (s) | | | 95.2 | | Sum of lost time (s) | | | 27.5 | |
| Intersection Capacity Utilization | | | 58.8% | | ICU Level of Service | | | B | |
| Analysis Period (min) | | | 15 | | | | | | |
| c Critical Lane Group | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
9: Potrero Ave & Richmond St

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 32 | 107 | 531 | 22 | 145 | 24 | 326 | 0 | 0 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | | 1.00 | | | |
| Fr _t | 0.89 | | | | 0.98 | | | | 1.00 | | | |
| Flt Protected | 1.00 | | | | 0.99 | | | | 0.95 | | | |
| Satd. Flow (prot) | 1659 | | | | 1821 | | | | 1770 | | | |
| Flt Permitted | 0.98 | | | | 0.92 | | | | 0.76 | | | |
| Satd. Flow (perm) | 1627 | | | | 1692 | | | | 1410 | | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 35 | 116 | 577 | 24 | 158 | 26 | 354 | 0 | 0 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 337 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 391 | 0 | 0 | 196 | 0 | 0 | 354 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 12.2 | | | 12.2 | | | 9.4 | | | | | |
| Effective Green, g (s) | 12.2 | | | 12.2 | | | 9.4 | | | | | |
| Actuated g/C Ratio | 0.41 | | | 0.41 | | | 0.32 | | | | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | | | |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | 3.0 | | | | | |
| Lane Grp Cap (vph) | 671 | | | 697 | | | 448 | | | | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.24 | | | 0.12 | | | c0.25 | | | | | |
| v/c Ratio | 0.58 | | | 0.28 | | | 0.79 | | | | | |
| Uniform Delay, d1 | 6.7 | | | 5.8 | | | 9.2 | | | | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | | | |
| Incremental Delay, d2 | 1.3 | | | 0.2 | | | 9.2 | | | | | |
| Delay (s) | 8.0 | | | 6.0 | | | 18.4 | | | | | |
| Level of Service | A | | | A | | | B | | | | | |
| Approach Delay (s) | 8.0 | | | 6.0 | | | 18.4 | | | 0.0 | | |
| Approach LOS | A | | | A | | | B | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 10.5 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.67 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 29.6 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 69.8% | | | ICU Level of Service | | | C | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
10: Moeser Ln & Richmond St 6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 298 | 368 | 65 | 350 | 0 | 184 | 0 | 11 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Frpb, ped/bikes | | 0.98 | | | | 1.00 | | | | 1.00 | | |
| Flpb, ped/bikes | | 1.00 | | | | 1.00 | | | | 1.00 | | |
| Fr | | 0.93 | | | | 1.00 | | | | 0.99 | | |
| Flt Protected | | 1.00 | | | | 0.99 | | | | 0.95 | | |
| Satd. Flow (prot) | | 1693 | | | | 1847 | | | | 1755 | | |
| Flt Permitted | | 1.00 | | | | 0.75 | | | | 0.74 | | |
| Satd. Flow (perm) | | 1693 | | | | 1401 | | | | 1356 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 324 | 400 | 71 | 380 | 0 | 200 | 0 | 12 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 648 | 0 | 0 | 451 | 0 | 0 | 205 | 0 | 0 | 0 | 0 |
| Confl. Peds. (#/hr) | 28 | | 11 | 11 | | 28 | 4 | | 5 | 5 | | 4 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | | 17.9 | | | 17.9 | | | 8.5 | | | | |
| Effective Green, g (s) | | 17.9 | | | 17.9 | | | 8.5 | | | | |
| Actuated g/C Ratio | | 0.52 | | | 0.52 | | | 0.25 | | | | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | | 881 | | | 729 | | | 335 | | | | |
| v/s Ratio Prot | c0.38 | | | | | | | | | | | |
| v/s Ratio Perm | | | | | 0.32 | | | c0.15 | | | | |
| v/c Ratio | | 0.74 | | | 0.62 | | | 0.61 | | | | |
| Uniform Delay, d1 | | 6.4 | | | 5.8 | | | 11.5 | | | | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | | 3.2 | | | 1.6 | | | 3.3 | | | | |
| Delay (s) | | 9.6 | | | 7.4 | | | 14.8 | | | | |
| Level of Service | | A | | | A | | | B | | | | |
| Approach Delay (s) | | 9.6 | | | 7.4 | | | 14.8 | | | 0.0 | |
| Approach LOS | | A | | | A | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 9.7 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.70 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 34.4 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 88.4% | | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
11: Central Ave & Richmond St

6/7/2012

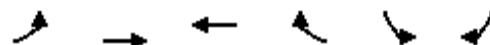


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 56 | 171 | 32 | 11 | 282 | 77 | 33 | 453 | 4 | 36 | 587 | 124 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 0.98 | | | | 0.99 | | | 1.00 | | | 0.99 | |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Fr | 0.98 | | | | 0.97 | | | 1.00 | | | 0.98 | |
| Flt Protected | 0.99 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1768 | | | | 1780 | | | 1853 | | | 1804 | |
| Flt Permitted | 0.79 | | | | 0.99 | | | 0.93 | | | 0.96 | |
| Satd. Flow (perm) | 1411 | | | | 1760 | | | 1726 | | | 1742 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 61 | 186 | 35 | 12 | 307 | 84 | 36 | 492 | 4 | 39 | 638 | 135 |
| RTOR Reduction (vph) | 0 | 9 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 13 | 0 |
| Lane Group Flow (vph) | 0 | 273 | 0 | 0 | 386 | 0 | 0 | 532 | 0 | 0 | 799 | 0 |
| Confl. Peds. (#/hr) | 23 | | 86 | 86 | | 23 | 27 | | 11 | 11 | | 27 |
| Confl. Bikes (#/hr) | | | 4 | | | 3 | | | 2 | | | 1 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 16.0 | | | 16.0 | | | 31.0 | | | 31.0 | | |
| Effective Green, g (s) | 16.0 | | | 16.0 | | | 31.0 | | | 31.0 | | |
| Actuated g/C Ratio | 0.29 | | | 0.29 | | | 0.56 | | | 0.56 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Lane Grp Cap (vph) | 410 | | | 512 | | | 973 | | | 982 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | 0.19 | | | c0.22 | | | 0.31 | | | c0.46 | | |
| v/c Ratio | 0.67 | | | 0.75 | | | 0.55 | | | 0.81 | | |
| Uniform Delay, d1 | 17.1 | | | 17.7 | | | 7.6 | | | 9.7 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.56 | | | 1.00 | | |
| Incremental Delay, d2 | 8.3 | | | 9.9 | | | 0.8 | | | 7.4 | | |
| Delay (s) | 25.4 | | | 27.6 | | | 12.5 | | | 17.0 | | |
| Level of Service | C | | | C | | | B | | | B | | |
| Approach Delay (s) | 25.4 | | | 27.6 | | | 12.5 | | | 17.0 | | |
| Approach LOS | C | | | C | | | B | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 19.1 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.79 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 55.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 94.4% | | | ICU Level of Service | | | F | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
12: Fairmont Ave & Richmond St

6/7/2012



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|-------|----------------------|-------|------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 27 | 291 | 300 | 463 | 533 | 65 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | | |
| Frpb, ped/bikes | 1.00 | 0.91 | 0.98 | | | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | | |
| Fr _t | 1.00 | 0.92 | 0.99 | | | |
| Fl _t Protected | 1.00 | 1.00 | 0.96 | | | |
| Satd. Flow (prot) | 1855 | 1553 | 1729 | | | |
| Fl _t Permitted | 0.67 | 1.00 | 0.96 | | | |
| Satd. Flow (perm) | 1251 | 1553 | 1729 | | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 29 | 316 | 326 | 503 | 579 | 71 |
| RTOR Reduction (vph) | 0 | 0 | 101 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 0 | 345 | 728 | 0 | 642 | 0 |
| Confl. Peds. (#/hr) | 76 | | | 76 | 16 | 131 |
| Confl. Bikes (#/hr) | | | | | 5 | |
| Turn Type | Perm | | | | | |
| Protected Phases | | 4 | 8 | | 6 | |
| Permitted Phases | 4 | | | | | |
| Actuated Green, G (s) | 27.0 | 27.0 | 20.0 | | | |
| Effective Green, g (s) | 27.0 | 27.0 | 20.0 | | | |
| Actuated g/C Ratio | 0.49 | 0.49 | 0.36 | | | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | | |
| Lane Grp Cap (vph) | 614 | 762 | 629 | | | |
| v/s Ratio Prot | | c0.47 | c0.37 | | | |
| v/s Ratio Perm | 0.28 | | | | | |
| v/c Ratio | 0.56 | 0.96 | 1.02 | | | |
| Uniform Delay, d1 | 9.8 | 13.4 | 17.5 | | | |
| Progression Factor | 1.00 | 1.00 | 1.33 | | | |
| Incremental Delay, d2 | 3.7 | 23.4 | 32.1 | | | |
| Delay (s) | 13.5 | 36.8 | 55.3 | | | |
| Level of Service | B | D | E | | | |
| Approach Delay (s) | 13.5 | 36.8 | 55.3 | | | |
| Approach LOS | B | D | E | | | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | 39.0 | HCM Level of Service | | | D | |
| HCM Volume to Capacity ratio | 0.98 | | | | | |
| Actuated Cycle Length (s) | 55.0 | Sum of lost time (s) | | | 8.0 | |
| Intersection Capacity Utilization | 88.2% | ICU Level of Service | | | E | |
| Analysis Period (min) | 15 | | | | | |
| c Critical Lane Group | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
13: Fairmont Ave & Colusa Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBT | NBL2 | NBL | NBR2 | SEL | SET | SER | SER2 |
|-----------------------------------|-------|------|------|------|----------------------|------|------|------|------|------|------|--------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 62 | 8 | 198 | 73 | 2 | 62 | 22 | 1 | 4 | 253 | 29 | 93 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | | | 0.95 | | |
| Fr _t | 0.89 | | | | 1.00 | | | | | 0.98 | | |
| Flt Protected | 0.99 | | | | 1.00 | | | | | 1.00 | | |
| Satd. Flow (prot) | 1648 | | | | 1863 | | | | | 1734 | | |
| Flt Permitted | 0.95 | | | | 1.00 | | | | | 1.00 | | |
| Satd. Flow (perm) | 1572 | | | | 1863 | | | | | 1730 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 67 | 9 | 215 | 79 | 2 | 67 | 24 | 1 | 4 | 275 | 32 | 101 |
| RTOR Reduction (vph) | 0 | 13 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 71 |
| Lane Group Flow (vph) | 0 | 357 | 0 | 0 | 2 | 0 | 91 | 0 | 0 | 320 | 0 | 20 |
| Turn Type | Perm | | | | Perm | | | | Perm | | | custom |
| Protected Phases | | 6 | | | 2 | | | 4 | | 8 | | |
| Permitted Phases | 6 | | | | | 4 | | | 8 | | | 4 |
| Actuated Green, G (s) | 17.1 | | | | 17.1 | | | 6.6 | | 18.8 | | 6.6 |
| Effective Green, g (s) | 17.1 | | | | 17.1 | | | 6.6 | | 18.8 | | 6.6 |
| Actuated g/C Ratio | 0.31 | | | | 0.31 | | | 0.12 | | 0.34 | | 0.12 |
| Clearance Time (s) | 4.5 | | | | 4.5 | | | 4.5 | | 4.5 | | 4.5 |
| Vehicle Extension (s) | 3.0 | | | | 3.0 | | | 3.0 | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 480 | | | | 569 | | | 209 | | 581 | | 177 |
| v/s Ratio Prot | | | | | 0.00 | | | | | | | |
| v/s Ratio Perm | c0.23 | | | | | 0.05 | | | 0.18 | | 0.01 | |
| v/c Ratio | 0.74 | | | | 0.00 | | | 0.44 | | 0.55 | | 0.11 |
| Uniform Delay, d1 | 17.5 | | | | 13.5 | | | 23.0 | | 15.2 | | 22.1 |
| Progression Factor | 1.00 | | | | 1.00 | | | 1.00 | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 6.1 | | | | 0.0 | | | 1.5 | | 1.1 | | 0.3 |
| Delay (s) | 23.6 | | | | 13.5 | | | 24.4 | | 16.3 | | 22.4 |
| Level of Service | C | | | | B | | | C | | B | | C |
| Approach Delay (s) | 23.6 | | | | 13.5 | | | 24.4 | | 17.6 | | |
| Approach LOS | C | | | | B | | | C | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 20.0 | | | | HCM Level of Service | | | | B | | | |
| HCM Volume to Capacity ratio | 0.66 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 56.0 | | | | Sum of lost time (s) | | | | 13.5 | | | |
| Intersection Capacity Utilization | 73.3% | | | | ICU Level of Service | | | | D | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 13: Fairmont Ave & Colusa Ave

6/7/2012



| Movement | NWL2 | NWL | NWT |
|------------------------|-------|------|------|
| Lane Configurations | | | |
| Volume (vph) | 1 | 165 | 157 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.5 | 4.5 |
| Lane Util. Factor | | 1.00 | 1.00 |
| Fr _t | | 1.00 | 1.00 |
| Flt Protected | | 0.95 | 1.00 |
| Satd. Flow (prot) | | 1770 | 1863 |
| Flt Permitted | | 0.44 | 1.00 |
| Satd. Flow (perm) | | 812 | 1863 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1 | 179 | 171 |
| RTOR Reduction (vph) | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 180 | 171 |
| Turn Type | Perm | Perm | |
| Protected Phases | | | 8 |
| Permitted Phases | 8 | 8 | |
| Actuated Green, G (s) | 18.8 | 18.8 | |
| Effective Green, g (s) | 18.8 | 18.8 | |
| Actuated g/C Ratio | 0.34 | 0.34 | |
| Clearance Time (s) | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 273 | 625 | |
| v/s Ratio Prot | | 0.09 | |
| v/s Ratio Perm | c0.22 | | |
| v/c Ratio | 0.66 | 0.27 | |
| Uniform Delay, d1 | 15.9 | 13.6 | |
| Progression Factor | 1.00 | 1.00 | |
| Incremental Delay, d2 | 5.7 | 0.2 | |
| Delay (s) | 21.5 | 13.8 | |
| Level of Service | C | B | |
| Approach Delay (s) | | 17.8 | |
| Approach LOS | | B | |
| Intersection Summary | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 1: MacDonald Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|-------|------|------|----------------------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑↑ | |
| Volume (vph) | 31 | 403 | 108 | 212 | 775 | 90 | 297 | 97 | 263 | 28 | 55 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.96 | 1.00 | 0.98 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | | 0.97 | 1.00 | 1.00 | 0.99 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3433 | 1863 | 1520 | 1747 | 1828 | | 1713 | 3539 | 1521 | 1743 | 4764 | |
| Flt Permitted | 0.12 | 1.00 | 1.00 | 0.44 | 1.00 | | 0.70 | 1.00 | 1.00 | 0.69 | 1.00 | |
| Satd. Flow (perm) | 428 | 1863 | 1520 | 805 | 1828 | | 1253 | 3539 | 1521 | 1259 | 4764 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 34 | 438 | 117 | 230 | 842 | 98 | 323 | 105 | 286 | 30 | 60 | 27 |
| RTOR Reduction (vph) | 0 | 0 | 52 | 0 | 6 | 0 | 0 | 0 | 197 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 34 | 438 | 65 | 230 | 934 | 0 | 323 | 105 | 89 | 30 | 68 | 0 |
| Confl. Peds. (#/hr) | 12 | | 24 | 24 | | 12 | 19 | | 9 | 9 | | 19 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 2 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 33.8 | 33.8 | 33.8 | 33.8 | 33.8 | | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | |
| Effective Green, g (s) | 33.8 | 33.8 | 33.8 | 33.8 | 33.8 | | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | |
| Actuated g/C Ratio | 0.56 | 0.56 | 0.56 | 0.56 | 0.56 | | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 238 | 1036 | 845 | 448 | 1016 | | 392 | 1106 | 475 | 393 | 1489 | |
| v/s Ratio Prot | | 0.24 | | c0.51 | | | 0.03 | | | | 0.01 | |
| v/s Ratio Perm | 0.08 | | 0.04 | 0.29 | | | c0.26 | | 0.06 | 0.02 | | |
| v/c Ratio | 0.14 | 0.42 | 0.08 | 0.51 | 0.92 | | 0.82 | 0.09 | 0.19 | 0.08 | 0.05 | |
| Uniform Delay, d1 | 6.5 | 7.8 | 6.3 | 8.4 | 12.3 | | 19.4 | 14.8 | 15.3 | 14.7 | 14.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 0.3 | 0.0 | 1.0 | 12.8 | | 13.1 | 0.0 | 0.2 | 0.1 | 0.0 | |
| Delay (s) | 6.8 | 8.1 | 6.3 | 9.4 | 25.0 | | 32.5 | 14.8 | 15.5 | 14.8 | 14.6 | |
| Level of Service | A | A | A | A | C | | C | B | B | B | B | |
| Approach Delay (s) | | | 7.7 | | 21.9 | | | 23.1 | | | 14.6 | |
| Approach LOS | | | A | | C | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 18.7 | | | | HCM Level of Service | | | B | | |
| HCM Volume to Capacity ratio | | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.8 | | | | Sum of lost time (s) | | | 8.0 | | |
| Intersection Capacity Utilization | | | 82.8% | | | | ICU Level of Service | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
2: Cutting Blvd & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|----------------------|-------|------|------|--------|-------|------|------|------|------|
| Lane Configurations | ↑ | | ↑↑ | ↑↑ | ↑↑ | ↑ | ↑↑ | ↑↑↑ | | | ↑↑ | ↑ |
| Volume (vph) | 194 | 0 | 574 | 449 | 504 | 88 | 475 | 1270 | 0 | 0 | 578 | 197 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | | | 0.95 | 1.00 |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | 3433 | 5085 | | | 3539 | 1583 |
| Flt Permitted | 0.45 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 833 | | 2787 | 3433 | 3539 | 1583 | 3526 | 5085 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 211 | 0 | 624 | 488 | 548 | 96 | 516 | 1380 | 0 | 0 | 628 | 214 |
| RTOR Reduction (vph) | 0 | 0 | 203 | 0 | 0 | 31 | 0 | 0 | 0 | 0 | 0 | 140 |
| Lane Group Flow (vph) | 211 | 0 | 421 | 488 | 548 | 65 | 516 | 1380 | 0 | 0 | 628 | 74 |
| Turn Type | custom | | custom | Perm | | Perm | custom | | | | Perm | |
| Protected Phases | | | | | 3 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 5 | 3 | | 3 | 5 | | | | 6 | |
| Actuated Green, G (s) | 12.2 | | 19.8 | 22.1 | 22.1 | 22.1 | 4.1 | 27.8 | | | 20.7 | 20.7 |
| Effective Green, g (s) | 12.2 | | 19.8 | 22.1 | 22.1 | 22.1 | 4.1 | 27.8 | | | 20.7 | 20.7 |
| Actuated g/C Ratio | 0.17 | | 0.27 | 0.30 | 0.30 | 0.30 | 0.06 | 0.38 | | | 0.28 | 0.28 |
| Clearance Time (s) | 3.5 | | | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 139 | | 755 | 1038 | 1070 | 479 | 198 | 1934 | | | 1002 | 448 |
| v/s Ratio Prot | | | | c0.15 | | | c0.27 | | | | 0.18 | |
| v/s Ratio Perm | c0.25 | | 0.15 | 0.14 | | 0.04 | c0.15 | | | | 0.05 | |
| v/c Ratio | 1.52 | | 0.56 | 0.47 | 0.51 | 0.14 | 2.61 | 0.71 | | | 0.63 | 0.16 |
| Uniform Delay, d1 | 30.4 | | 22.9 | 20.7 | 21.0 | 18.6 | 34.5 | 19.3 | | | 22.8 | 19.7 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 266.3 | | 0.9 | 0.3 | 0.4 | 0.1 | 737.2 | 1.3 | | | 1.2 | 0.2 |
| Delay (s) | 296.8 | | 23.8 | 21.1 | 21.5 | 18.7 | 771.7 | 20.5 | | | 24.1 | 19.9 |
| Level of Service | F | | C | C | C | B | F | C | | | C | B |
| Approach Delay (s) | 92.8 | | | | 21.1 | | | 225.0 | | | 23.0 | |
| Approach LOS | F | | | | C | | | F | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 116.3 | | HCM Level of Service | | | | | F | | | | |
| HCM Volume to Capacity ratio | 0.90 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 73.1 | | Sum of lost time (s) | | | | | 10.0 | | | | |
| Intersection Capacity Utilization | 67.5% | | ICU Level of Service | | | | | C | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|-----------------------------------|-------|------|----------------------|------|------|------|-------|------|-------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 46 | 33 | 35 | 2 | 29 | 32 | 15 | 239 | 61 | 24 | 1330 | 115 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.97 | 1.00 | | | | | 0.96 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1810 | 1583 | | | | | 1790 | 1583 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.16 | 1.00 | | | | | 0.71 | 1.00 | | 0.10 | 1.00 | 1.00 |
| Satd. Flow (perm) | 306 | 1583 | | | | | 1322 | 1583 | | 177 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 50 | 36 | 38 | 2 | 32 | 35 | 16 | 260 | 66 | 26 | 1446 | 125 |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 244 | 0 | 0 | 0 | 61 |
| Lane Group Flow (vph) | 0 | 86 | 39 | 0 | 0 | 0 | 83 | 16 | 0 | 92 | 1446 | 64 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | pm+pt | pm+pt | | Perm |
| Protected Phases | | 3 | | | | | | 7 | | 5 | 5 | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | 2 |
| Actuated Green, G (s) | 41.0 | 41.0 | | | | | 9.0 | 9.0 | | 52.0 | 42.0 | 42.0 |
| Effective Green, g (s) | 41.0 | 41.0 | | | | | 9.0 | 9.0 | | 52.0 | 42.0 | 42.0 |
| Actuated g/C Ratio | 0.28 | 0.28 | | | | | 0.06 | 0.06 | | 0.36 | 0.29 | 0.29 |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 86 | 446 | | | | | 82 | 98 | | 173 | 1021 | 457 |
| v/s Ratio Prot | | | | | | | | | | 0.04 | c0.41 | |
| v/s Ratio Perm | c0.28 | 0.02 | | | | | c0.06 | 0.01 | | 0.15 | | 0.04 |
| v/c Ratio | 1.00 | 0.09 | | | | | 1.01 | 0.16 | | 0.53 | 1.42 | 0.14 |
| Uniform Delay, d1 | 52.3 | 38.5 | | | | | 68.3 | 64.7 | | 37.0 | 51.8 | 38.4 |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 97.0 | 0.1 | | | | | 102.8 | 0.8 | | 3.1 | 193.1 | 0.1 |
| Delay (s) | 149.3 | 38.6 | | | | | 171.1 | 65.5 | | 40.1 | 244.9 | 38.5 |
| Level of Service | F | D | | | | | F | E | | D | F | D |
| Approach Delay (s) | 114.2 | | | | | | 91.1 | | | | 218.1 | |
| Approach LOS | F | | | | | | F | | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 177.6 | | HCM Level of Service | | | | | | | F | | |
| HCM Volume to Capacity ratio | 1.11 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 145.6 | | Sum of lost time (s) | | | | | 20.0 | | | | |
| Intersection Capacity Utilization | 82.1% | | ICU Level of Service | | | | | E | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | | | ↑↑ | | ↑ |
| Volume (vph) | 324 | 1016 | 236 | 8 | 14 | 274 | 113 | 46 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | | | | 0.97 | | 1.00 |
| Fr _t | 1.00 | 0.97 | | | | 0.96 | | 0.85 |
| Flt Protected | 0.95 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | 3433 | 3436 | | | | 3341 | | 1583 |
| Flt Permitted | 0.09 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | 336 | 3436 | | | | 3341 | | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 352 | 1104 | 257 | 9 | 15 | 298 | 123 | 50 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 |
| Lane Group Flow (vph) | 352 | 1370 | 0 | 0 | 0 | 436 | 0 | 8 |
| Turn Type | pm+pt | | | | Perm | | | Perm |
| Protected Phases | 1 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | 53.0 | 43.0 | | | | 23.6 | | 23.6 |
| Effective Green, g (s) | 53.0 | 43.0 | | | | 23.6 | | 23.6 |
| Actuated g/C Ratio | 0.36 | 0.30 | | | | 0.16 | | 0.16 |
| Clearance Time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 335 | 1015 | | | | 542 | | 257 |
| v/s Ratio Prot | c0.07 | 0.40 | | | | | | |
| v/s Ratio Perm | 0.31 | | | | | 0.13 | | 0.01 |
| v/c Ratio | 1.05 | 1.35 | | | | 0.80 | | 0.03 |
| Uniform Delay, d1 | 38.4 | 51.3 | | | | 58.8 | | 51.4 |
| Progression Factor | 1.00 | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 63.1 | 164.0 | | | | 8.5 | | 0.1 |
| Delay (s) | 101.5 | 215.3 | | | | 67.2 | | 51.4 |
| Level of Service | F | F | | | | E | | D |
| Approach Delay (s) | | 192.0 | | | | 65.6 | | |
| Approach LOS | | F | | | | E | | |

Intersection Summary

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
4: Potrero Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|-------|------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 105 | 191 | 155 | 69 | 185 | 452 | 138 | 959 | 26 | 420 | 612 | 95 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3163 | | 1770 | 3525 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.24 | 1.00 | 1.00 | 0.56 | 1.00 | | 0.35 | 1.00 | | 0.16 | 1.00 | 1.00 |
| Satd. Flow (perm) | 446 | 1863 | 1583 | 1035 | 3163 | | 643 | 3525 | | 304 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 114 | 208 | 168 | 75 | 201 | 491 | 150 | 1042 | 28 | 457 | 665 | 103 |
| RTOR Reduction (vph) | 0 | 0 | 115 | 0 | 124 | 0 | 0 | 3 | 0 | 0 | 0 | 58 |
| Lane Group Flow (vph) | 114 | 208 | 53 | 75 | 568 | 0 | 150 | 1067 | 0 | 457 | 665 | 45 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | | 28.0 | 24.2 | | 28.6 | 24.5 | 24.5 |
| Effective Green, g (s) | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | | 28.0 | 24.2 | | 28.6 | 24.5 | 24.5 |
| Actuated g/C Ratio | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 | | 0.50 | 0.43 | | 0.51 | 0.44 | 0.44 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 140 | 584 | 496 | 325 | 992 | | 399 | 1529 | | 264 | 1554 | 695 |
| v/s Ratio Prot | | 0.11 | | | 0.18 | | 0.03 | 0.30 | | c0.13 | 0.19 | |
| v/s Ratio Perm | c0.26 | | 0.03 | 0.07 | | | 0.16 | | | c0.76 | | 0.03 |
| v/c Ratio | 0.81 | 0.36 | 0.11 | 0.23 | 0.57 | | 0.38 | 0.70 | | 1.73 | 0.43 | 0.07 |
| Uniform Delay, d1 | 17.7 | 14.8 | 13.6 | 14.2 | 16.0 | | 7.7 | 12.8 | | 11.3 | 10.8 | 9.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 29.1 | 0.4 | 0.1 | 0.4 | 0.8 | | 0.6 | 1.4 | | 344.4 | 0.2 | 0.0 |
| Delay (s) | 46.8 | 15.2 | 13.7 | 14.5 | 16.8 | | 8.3 | 14.2 | | 355.7 | 11.0 | 9.1 |
| Level of Service | D | B | B | B | B | | A | B | | F | B | A |
| Approach Delay (s) | | 22.0 | | | 16.6 | | | 13.5 | | | 139.4 | |
| Approach LOS | | C | | | B | | | B | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 56.9 | | | HCM Level of Service | | | E | | | | |
| HCM Volume to Capacity ratio | | 1.28 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 55.8 | | | Sum of lost time (s) | | | 6.0 | | | | |
| Intersection Capacity Utilization | | 90.3% | | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 5: Moeser Ln & San Pablo Ave

6/7/2012



| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|-------|----------------------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↔ | ↑↑ | | ↑ | ↑↑ |
| Volume (vph) | 210 | 531 | 60 | 1086 | 136 | 497 | 631 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 |
| Frpb, ped/bikes | 1.00 | 0.96 | 1.00 | 0.99 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1520 | 1770 | 3459 | | 1769 | 3539 |
| Fl _t Permitted | 0.95 | 1.00 | 0.27 | 1.00 | | 0.20 | 1.00 |
| Satd. Flow (perm) | 1770 | 1520 | 508 | 3459 | | 372 | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 228 | 577 | 65 | 1180 | 148 | 540 | 686 |
| RTOR Reduction (vph) | 0 | 107 | 0 | 16 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 228 | 470 | 65 | 1312 | 0 | 540 | 686 |
| Confl. Peds. (#/hr) | | 41 | | | 18 | 18 | |
| Confl. Bikes (#/hr) | | | | | 8 | | |
| Turn Type | | Perm | pm+pt | | pm+pt | | |
| Protected Phases | 4 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | | 4 | 2 | | 6 | | |
| Actuated Green, G (s) | 26.0 | 26.0 | 24.0 | 20.0 | | 24.0 | 20.0 |
| Effective Green, g (s) | 26.0 | 26.0 | 24.0 | 20.0 | | 24.0 | 20.0 |
| Actuated g/C Ratio | 0.43 | 0.43 | 0.40 | 0.33 | | 0.40 | 0.33 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Grp Cap (vph) | 767 | 659 | 287 | 1153 | | 242 | 1180 |
| v/s Ratio Prot | 0.13 | | 0.02 | 0.38 | c0.15 | 0.19 | |
| v/s Ratio Perm | | c0.31 | 0.08 | | c0.74 | | |
| v/c Ratio | 0.30 | 0.71 | 0.23 | 1.14 | | 2.23 | 0.58 |
| Uniform Delay, d ₁ | 11.1 | 13.9 | 11.5 | 20.0 | | 18.3 | 16.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d ₂ | 1.0 | 6.5 | 1.8 | 73.0 | | 567.3 | 2.1 |
| Delay (s) | 12.0 | 20.4 | 13.4 | 93.0 | | 585.6 | 18.6 |
| Level of Service | B | C | B | F | | F | B |
| Approach Delay (s) | 18.1 | | | 89.3 | | 268.3 | |
| Approach LOS | B | | | F | | F | |
| Intersection Summary | | | | | | | |
| HCM Average Control Delay | | 136.7 | | HCM Level of Service | | F | |
| HCM Volume to Capacity ratio | | 1.41 | | | | | |
| Actuated Cycle Length (s) | | 60.0 | | Sum of lost time (s) | | 9.0 | |
| Intersection Capacity Utilization | | 93.8% | | ICU Level of Service | | F | |
| Analysis Period (min) | | 15 | | | | | |

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
6: Central Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Volume (vph) | 382 | 229 | 153 | 52 | 210 | 76 | 159 | 866 | 57 | 44 | 576 | 210 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.97 | | 1.00 | 0.99 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 0.98 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1681 | 1741 | 1583 | | 3393 | | 1770 | 3506 | | 1770 | 3397 | |
| Flt Permitted | 0.53 | 0.76 | 1.00 | | 0.55 | | 0.18 | 1.00 | | 0.20 | 1.00 | |
| Satd. Flow (perm) | 943 | 1338 | 1583 | | 1884 | | 339 | 3506 | | 373 | 3397 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 415 | 249 | 166 | 57 | 228 | 83 | 173 | 941 | 62 | 48 | 626 | 228 |
| RTOR Reduction (vph) | 0 | 0 | 115 | 0 | 27 | 0 | 0 | 5 | 0 | 0 | 37 | 0 |
| Lane Group Flow (vph) | 295 | 369 | 51 | 0 | 341 | 0 | 173 | 998 | 0 | 48 | 817 | 0 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | |
| Protected Phases | | 4 | | | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 3 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 31.0 | 31.0 | 31.0 | | 30.0 | | 28.0 | 22.0 | | 24.0 | 20.0 | |
| Effective Green, g (s) | 31.0 | 31.0 | 31.0 | | 30.0 | | 28.0 | 22.0 | | 24.0 | 20.0 | |
| Actuated g/C Ratio | 0.31 | 0.31 | 0.31 | | 0.30 | | 0.28 | 0.22 | | 0.24 | 0.20 | |
| Clearance Time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Grp Cap (vph) | 291 | 413 | 488 | | 562 | | 180 | 767 | | 145 | 676 | |
| v/s Ratio Prot | | | | | | | c0.06 | c0.28 | | 0.01 | 0.24 | |
| v/s Ratio Perm | c0.31 | 0.28 | 0.03 | | c0.18 | | 0.21 | | | 0.07 | | |
| v/c Ratio | 1.01 | 0.89 | 0.10 | | 0.61 | | 0.96 | 1.30 | | 0.33 | 1.21 | |
| Uniform Delay, d1 | 34.8 | 33.2 | 24.8 | | 30.2 | | 34.1 | 39.2 | | 31.2 | 40.2 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 56.3 | 24.3 | 0.4 | | 4.8 | | 57.6 | 145.2 | | 6.0 | 107.4 | |
| Delay (s) | 91.1 | 57.4 | 25.3 | | 35.0 | | 91.7 | 184.4 | | 37.3 | 147.7 | |
| Level of Service | F | E | C | | D | | F | F | | D | F | |
| Approach Delay (s) | | 63.0 | | | 35.0 | | | 170.8 | | | 141.8 | |
| Approach LOS | | E | | | D | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 120.2 | | | HCM Level of Service | | | F | | | | |
| HCM Volume to Capacity ratio | | 0.95 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 100.5 | | | Sum of lost time (s) | | | 12.5 | | | | |
| Intersection Capacity Utilization | | 71.1% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 7: Fairmont Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|-------|------|-------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 11 | 170 | 16 | 110 | 171 | 56 | 72 | 1024 | 121 | 88 | 801 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | | 0.99 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.99 | | | 0.98 | | 1.00 | 0.98 | | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | | 0.98 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1752 | 1833 | | | 3359 | | 1768 | 3469 | | 1769 | 3530 | |
| Flt Permitted | 0.51 | 1.00 | | | 0.79 | | 0.21 | 1.00 | | 0.14 | 1.00 | |
| Satd. Flow (perm) | 937 | 1833 | | | 2682 | | 387 | 3469 | | 266 | 3530 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 185 | 17 | 120 | 186 | 61 | 78 | 1113 | 132 | 96 | 871 | 12 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 25 | 0 | 0 | 14 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 12 | 197 | 0 | 0 | 342 | 0 | 78 | 1231 | 0 | 96 | 882 | 0 |
| Confl. Peds. (#/hr) | 21 | | 30 | 30 | | 21 | 30 | | 10 | 10 | | 30 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | 4 | | | | 1 |
| Turn Type | Perm | | Perm | | | pm+pt | | | pm+pt | | | |
| Protected Phases | | 4 | | | 8 | | 1 | 6 | | 5 | | 2 |
| Permitted Phases | 4 | | | 8 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 25.0 | 25.0 | | | 25.0 | | 32.0 | 28.0 | | 32.0 | 28.0 | |
| Effective Green, g (s) | 25.0 | 25.0 | | | 25.0 | | 32.0 | 28.0 | | 32.0 | 28.0 | |
| Actuated g/C Ratio | 0.37 | 0.37 | | | 0.37 | | 0.47 | 0.41 | | 0.47 | 0.41 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Grp Cap (vph) | 344 | 674 | | | 986 | | 263 | 1428 | | 214 | 1454 | |
| v/s Ratio Prot | | 0.11 | | | | | 0.02 | c0.36 | | c0.03 | 0.25 | |
| v/s Ratio Perm | 0.01 | | | c0.13 | | | 0.12 | | | 0.19 | | |
| v/c Ratio | 0.03 | 0.29 | | | 0.35 | | 0.30 | 0.86 | | 0.45 | 0.61 | |
| Uniform Delay, d1 | 13.8 | 15.2 | | | 15.6 | | 10.8 | 18.2 | | 13.1 | 15.7 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.2 | 1.1 | | | 1.0 | | 2.9 | 7.1 | | 6.7 | 1.9 | |
| Delay (s) | 14.0 | 16.3 | | | 16.6 | | 13.7 | 25.3 | | 19.7 | 17.6 | |
| Level of Service | B | B | | | B | | B | C | | B | B | |
| Approach Delay (s) | | 16.2 | | | 16.6 | | | 24.6 | | | 17.8 | |
| Approach LOS | | B | | | B | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 20.7 | | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.61 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 68.0 | | | Sum of lost time (s) | | | 11.0 | | | | |
| Intersection Capacity Utilization | | 92.1% | | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
8: Key Blvd & Elm St

6/7/2012



| Movement | EBL | EBR | NBL | NBT | SBT | SBR | SBR2 | NEL | NER |
|-----------------------------------|-------|-------|------|-------|----------------------|------|------|-------|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 0 | 118 | 291 | 112 | 133 | 0 | 4 | 176 | 101 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | | 4.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | | | 0.99 | 1.00 | | | 1.00 | 1.00 |
| Fr _t | 0.86 | | | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Fl _t Protected | 1.00 | | | 0.97 | 1.00 | | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1611 | | | 1783 | 1856 | | | 1770 | 1583 |
| Fl _t Permitted | 1.00 | | | 0.65 | 1.00 | | | 0.95 | 1.00 |
| Satd. Flow (perm) | 1611 | | | 1196 | 1856 | | | 1770 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 128 | 316 | 122 | 145 | 0 | 4 | 191 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 92 |
| Lane Group Flow (vph) | 128 | 0 | 0 | 438 | 148 | 0 | 0 | 191 | 18 |
| Confl. Peds. (#/hr) | | | | 5 | | | | 2 | |
| Turn Type | | | | Perm | | | | Perm | |
| Protected Phases | 3 | | | 4 2 | 7 2 | | | 8 | |
| Permitted Phases | | | | 4 2 | | | | 8 | |
| Actuated Green, G (s) | 16.0 | | | 32.0 | 32.0 | | | 16.0 | 16.0 |
| Effective Green, g (s) | 16.0 | | | 32.0 | 32.0 | | | 16.0 | 16.0 |
| Actuated g/C Ratio | 0.16 | | | 0.32 | 0.32 | | | 0.16 | 0.16 |
| Clearance Time (s) | 4.0 | | | | | | | 4.0 | 4.0 |
| Lane Grp Cap (vph) | 258 | | | 383 | 594 | | | 283 | 253 |
| v/s Ratio Prot | c0.08 | | | | c0.08 | | | c0.11 | |
| v/s Ratio Perm | | | | c0.37 | | | | 0.01 | |
| v/c Ratio | 0.50 | | | 1.14 | 0.25 | | | 0.67 | 0.07 |
| Uniform Delay, d ₁ | 38.3 | | | 34.0 | 25.1 | | | 39.6 | 35.7 |
| Progression Factor | 1.00 | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d ₂ | 6.7 | | | 91.2 | 1.0 | | | 12.2 | 0.5 |
| Delay (s) | 45.0 | | | 125.2 | 26.1 | | | 51.7 | 36.2 |
| Level of Service | D | | | F | C | | | D | D |
| Approach Delay (s) | 45.0 | | | 125.2 | 26.1 | | | 46.1 | |
| Approach LOS | D | | | F | C | | | D | |
| Intersection Summary | | | | | | | | | |
| HCM Average Control Delay | | 77.1 | | | HCM Level of Service | | | E | |
| HCM Volume to Capacity ratio | | 0.74 | | | | | | | |
| Actuated Cycle Length (s) | | 100.0 | | | Sum of lost time (s) | | | 20.0 | |
| Intersection Capacity Utilization | | 59.6% | | | ICU Level of Service | | | B | |
| Analysis Period (min) | | 15 | | | | | | | |
| c Critical Lane Group | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
9: Potrero Ave & Richmond St

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 51 | 142 | 399 | 31 | 82 | 18 | 399 | 0 | 0 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 1.00 | | | | 1.00 | | | | | | | |
| Flt Protected | 0.91 | | | | 0.98 | | | | | | | |
| Flt Permitted | | | | | | | | | | | | |
| Satd. Flow (prot) | 1.00 | | | | 0.99 | | | | | | | |
| Satd. Flow (perm) | 1686 | | | | 1806 | | | | | 1770 | | |
| RTOR Reduction (vph) | 0 | 187 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 456 | 0 | 0 | 131 | 0 | 0 | 434 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 16.0 | | | 16.0 | | | 16.0 | | | | | |
| Effective Green, g (s) | 16.0 | | | 16.0 | | | 16.0 | | | | | |
| Actuated g/C Ratio | 0.40 | | | 0.40 | | | 0.40 | | | | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | | | |
| Lane Grp Cap (vph) | 654 | | | 628 | | | 564 | | | | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.28 | | | 0.08 | | | c0.31 | | | | | |
| v/c Ratio | 0.70 | | | 0.21 | | | 0.77 | | | | | |
| Uniform Delay, d1 | 10.0 | | | 7.9 | | | 10.4 | | | | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | | | |
| Incremental Delay, d2 | 6.1 | | | 0.8 | | | 9.7 | | | | | |
| Delay (s) | 16.1 | | | 8.6 | | | 20.1 | | | | | |
| Level of Service | B | | | A | | | C | | | | | |
| Approach Delay (s) | 16.1 | | | 8.6 | | | 20.1 | | | 0.0 | | |
| Approach LOS | B | | | A | | | C | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 16.6 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.73 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 40.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 66.8% | | | ICU Level of Service | | | C | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
10: Moeser Ln & Richmond St 6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 277 | 279 | 26 | 298 | 0 | 348 | 0 | 26 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Frpb, ped/bikes | 0.99 | | | | 1.00 | | | | 1.00 | | | |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | | 1.00 | | | |
| Fr | 0.93 | | | | 1.00 | | | | 0.99 | | | |
| Flt Protected | 1.00 | | | | 1.00 | | | | 0.96 | | | |
| Satd. Flow (prot) | 1712 | | | | 1855 | | | | 1756 | | | |
| Flt Permitted | 1.00 | | | | 0.85 | | | | 0.74 | | | |
| Satd. Flow (perm) | 1712 | | | | 1584 | | | | 1361 | | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 301 | 303 | 28 | 324 | 0 | 378 | 0 | 28 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 91 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 513 | 0 | 0 | 352 | 0 | 0 | 399 | 0 | 0 | 0 | 0 |
| Confl. Peds. (#/hr) | 15 | | 7 | 7 | | 15 | 2 | | 2 | 2 | | 2 |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Perm | | | Perm | | | Perm | | Perm | | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 16.0 | | | 16.0 | | | 16.0 | | | | | |
| Effective Green, g (s) | 16.0 | | | 16.0 | | | 16.0 | | | | | |
| Actuated g/C Ratio | 0.40 | | | 0.40 | | | 0.40 | | | | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | | | |
| Lane Grp Cap (vph) | 685 | | | 634 | | | 544 | | | | | |
| v/s Ratio Prot | c0.30 | | | | | | | | | | | |
| v/s Ratio Perm | | | | 0.22 | | | c0.29 | | | | | |
| v/c Ratio | 0.75 | | | 0.56 | | | 0.73 | | | | | |
| Uniform Delay, d1 | 10.3 | | | 9.3 | | | 10.2 | | | | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | | | |
| Incremental Delay, d2 | 7.4 | | | 3.5 | | | 8.5 | | | | | |
| Delay (s) | 17.7 | | | 12.7 | | | 18.7 | | | | | |
| Level of Service | B | | | B | | | B | | | | | |
| Approach Delay (s) | 17.7 | | | 12.7 | | | 18.7 | | | 0.0 | | |
| Approach LOS | B | | | B | | | B | | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 16.7 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.74 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 40.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 71.4% | | | ICU Level of Service | | | C | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
11: Central Ave & Richmond St

6/7/2012

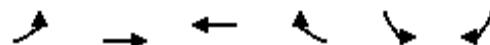


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 94 | 191 | 40 | 3 | 95 | 38 | 35 | 612 | 8 | 36 | 560 | 85 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | | | | 4.0 | | | | 4.0 | | | 4.0 |
| Lane Util. Factor | | | | | | | | | | | | |
| Frpb, ped/bikes | 1.00 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 0.99 | | | | 0.98 | | | 1.00 | | | 1.00 | |
| Fr | 0.99 | | | | 0.96 | | | 1.00 | | | 0.98 | |
| Flt Protected | 0.99 | | | | 1.00 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1766 | | | | 1755 | | | 1853 | | | 1819 | |
| Flt Permitted | 0.88 | | | | 0.99 | | | 0.95 | | | 0.95 | |
| Satd. Flow (perm) | 1580 | | | | 1744 | | | 1757 | | | 1729 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 102 | 208 | 43 | 3 | 103 | 41 | 38 | 665 | 9 | 39 | 609 | 92 |
| RTOR Reduction (vph) | 0 | 9 | 0 | 0 | 26 | 0 | 0 | 1 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 344 | 0 | 0 | 121 | 0 | 0 | 711 | 0 | 0 | 731 | 0 |
| Confl. Peds. (#/hr) | 29 | | 44 | 44 | | 29 | 17 | | 21 | 21 | | 17 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 2 | | | 1 |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 16.0 | | | 16.0 | | | 31.0 | | | 31.0 | | |
| Effective Green, g (s) | 16.0 | | | 16.0 | | | 31.0 | | | 31.0 | | |
| Actuated g/C Ratio | 0.29 | | | 0.29 | | | 0.56 | | | 0.56 | | |
| Clearance Time (s) | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | | |
| Lane Grp Cap (vph) | 460 | | | 507 | | | 990 | | | 975 | | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.22 | | | 0.07 | | | 0.40 | | | c0.42 | | |
| v/c Ratio | 0.75 | | | 0.24 | | | 0.72 | | | 0.75 | | |
| Uniform Delay, d1 | 17.7 | | | 14.9 | | | 8.8 | | | 9.1 | | |
| Progression Factor | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 10.6 | | | 1.1 | | | 4.5 | | | 5.3 | | |
| Delay (s) | 28.3 | | | 16.0 | | | 13.3 | | | 14.3 | | |
| Level of Service | C | | | B | | | B | | | B | | |
| Approach Delay (s) | 28.3 | | | 16.0 | | | 13.3 | | | 14.3 | | |
| Approach LOS | C | | | B | | | B | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 16.6 | | | HCM Level of Service | | | B | | | | | |
| HCM Volume to Capacity ratio | 0.75 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 55.0 | | | Sum of lost time (s) | | | 8.0 | | | | | |
| Intersection Capacity Utilization | 88.2% | | | ICU Level of Service | | | E | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 12: Fairmont Ave & Richmond St

6/7/2012



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|--------|----------------------|------|-------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 122 | 331 | 283 | 502 | 490 | 96 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | |
| Frpb, ped/bikes | | 1.00 | 0.91 | | 0.97 | |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | |
| Fr _t | | 1.00 | 0.91 | | 0.98 | |
| Fl _t Protected | | 0.99 | 1.00 | | 0.96 | |
| Satd. Flow (prot) | | 1838 | 1546 | | 1699 | |
| Fl _t Permitted | | 0.36 | 1.00 | | 0.96 | |
| Satd. Flow (perm) | | 679 | 1546 | | 1699 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 133 | 360 | 308 | 546 | 533 | 104 |
| RTOR Reduction (vph) | 0 | 0 | 85 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 0 | 493 | 769 | 0 | 627 | 0 |
| Confl. Peds. (#/hr) | 53 | | | 53 | 26 | 98 |
| Confl. Bikes (#/hr) | | | | 3 | | 49 |
| Turn Type | Perm | | | | | |
| Protected Phases | | 4 | 8 | | 6 | |
| Permitted Phases | 4 | | | | | |
| Actuated Green, G (s) | | 43.0 | 43.0 | | 24.0 | |
| Effective Green, g (s) | | 43.0 | 43.0 | | 24.0 | |
| Actuated g/C Ratio | | 0.57 | 0.57 | | 0.32 | |
| Clearance Time (s) | | 4.0 | 4.0 | | 4.0 | |
| Lane Grp Cap (vph) | | 389 | 886 | | 544 | |
| v/s Ratio Prot | | | 0.50 | | c0.37 | |
| v/s Ratio Perm | | c0.73 | | | | |
| v/c Ratio | | 1.27 | 0.87 | | 1.15 | |
| Uniform Delay, d1 | | 16.0 | 13.6 | | 25.5 | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 139.3 | 11.2 | | 88.5 | |
| Delay (s) | | 155.3 | 24.8 | | 114.0 | |
| Level of Service | | F | C | | F | |
| Approach Delay (s) | | 155.3 | 24.8 | | 114.0 | |
| Approach LOS | | F | C | | F | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 85.9 | HCM Level of Service | | F | |
| HCM Volume to Capacity ratio | | 1.23 | | | | |
| Actuated Cycle Length (s) | | 75.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 116.5% | ICU Level of Service | | H | |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
13: Fairmont Ave & Colusa Ave

6/7/2012



| Movement | EBL | EBT | EBR | EBR2 | WBT | WBR | NBL2 | NBL | SET | SER | SER2 | NWL2 |
|------------------------|-------|------|------|------|------|------|------|------|------|------|--------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 138 | 5 | 176 | 84 | 11 | 1 | 71 | 19 | 117 | 16 | 77 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | | | | 1.00 | | | 1.00 | 0.95 | | 0.95 | |
| Fr _t | 0.91 | | | | 0.99 | | | 1.00 | 0.98 | | 0.85 | |
| Flt Protected | 0.98 | | | | 1.00 | | | 0.95 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | 1672 | | | | 1843 | | | 1770 | 1726 | | 1504 | |
| Flt Permitted | 0.88 | | | | 1.00 | | | 0.95 | 1.00 | | 1.00 | |
| Satd. Flow (perm) | 1499 | | | | 1843 | | | 1770 | 1726 | | 1504 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 150 | 5 | 191 | 91 | 12 | 1 | 77 | 21 | 127 | 17 | 84 | 1 |
| RTOR Reduction (vph) | 0 | 14 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 49 | 0 |
| Lane Group Flow (vph) | 0 | 423 | 0 | 0 | 12 | 0 | 0 | 98 | 149 | 0 | 27 | 0 |
| Turn Type | Perm | | | | | | | Perm | | | custom | Perm |
| Protected Phases | | 6! | | | | 2! | | | 4 | | 8 | |
| Permitted Phases | | 6! | | | | | | 4 | | | 6 | 8 |
| Actuated Green, G (s) | 18.9 | | | | 18.9 | | | 6.7 | 13.9 | | 18.9 | |
| Effective Green, g (s) | 18.9 | | | | 18.9 | | | 6.7 | 13.9 | | 18.9 | |
| Actuated g/C Ratio | 0.36 | | | | 0.36 | | | 0.13 | 0.26 | | 0.36 | |
| Clearance Time (s) | 4.5 | | | | 4.5 | | | 4.5 | 4.5 | | 4.5 | |
| Vehicle Extension (s) | 3.0 | | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 535 | | | | 657 | | | 224 | 453 | | 536 | |
| v/s Ratio Prot | | | | | 0.01 | | | | 0.09 | | | |
| v/s Ratio Perm | c0.28 | | | | | | | 0.06 | | | 0.02 | |
| v/c Ratio | 0.79 | | | | 0.02 | | | 0.44 | 0.33 | | 0.05 | |
| Uniform Delay, d1 | 15.3 | | | | 11.0 | | | 21.4 | 15.8 | | 11.2 | |
| Progression Factor | 1.00 | | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 7.9 | | | | 0.0 | | | 1.4 | 0.4 | | 0.0 | |
| Delay (s) | 23.1 | | | | 11.1 | | | 22.8 | 16.2 | | 11.2 | |
| Level of Service | C | | | | B | | | C | B | | B | |
| Approach Delay (s) | 23.1 | | | | 11.1 | | | 22.8 | 14.5 | | | |
| Approach LOS | C | | | | B | | | C | B | | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 20.4 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.69 | | |
| Actuated Cycle Length (s) | 53.0 | Sum of lost time (s) | 13.5 |
| Intersection Capacity Utilization | 71.6% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |

! Phase conflict between lane groups.

c Critical Lane Group

2016 Wildcat and Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 13: Fairmont Ave & Colusa Ave



| Movement | NWL | NWT |
|------------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | 201 | 235 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Total Lost time (s) | 4.5 | 4.5 |
| Lane Util. Factor | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 |
| Flt Permitted | 0.66 | 1.00 |
| Satd. Flow (perm) | 1221 | 1863 |
| Peak-hour factor, PHF | 0.92 | 0.92 |
| Adj. Flow (vph) | 218 | 255 |
| RTOR Reduction (vph) | 0 | 0 |
| Lane Group Flow (vph) | 219 | 255 |
| Turn Type | Perm | |
| Protected Phases | 8 | |
| Permitted Phases | 8 | |
| Actuated Green, G (s) | 13.9 | 13.9 |
| Effective Green, g (s) | 13.9 | 13.9 |
| Actuated g/C Ratio | 0.26 | 0.26 |
| Clearance Time (s) | 4.5 | 4.5 |
| Vehicle Extension (s) | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 320 | 489 |
| v/s Ratio Prot | 0.14 | |
| v/s Ratio Perm | 0.18 | |
| v/c Ratio | 0.68 | |
| Uniform Delay, d1 | 17.6 | 16.7 |
| Progression Factor | 1.00 | 1.00 |
| Incremental Delay, d2 | 5.9 | 1.0 |
| Delay (s) | 23.5 | 17.7 |
| Level of Service | C | B |
| Approach Delay (s) | 20.4 | |
| Approach LOS | C | |

Intersection Summary

APPENDIX L

Central Pressure Zone Pipeline (El Cerrito/Richmond) Level of Service Calculations

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2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

1: MacDonald Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|------|------|----------------------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑↑ | ↑↑ | ↑ | ↑↑ | ↑↑↑ | |
| Volume (vph) | 20 | 592 | 85 | 133 | 317 | 35 | 135 | 47 | 176 | 43 | 75 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3411 | 1863 | 1554 | 1767 | 1832 | | 1770 | 3539 | 1540 | 1762 | 4862 | |
| Flt Permitted | 0.53 | 1.00 | 1.00 | 0.31 | 1.00 | | 0.68 | 1.00 | 1.00 | 0.72 | 1.00 | |
| Satd. Flow (perm) | 1893 | 1863 | 1554 | 582 | 1832 | | 1265 | 3539 | 1540 | 1339 | 4862 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 22 | 643 | 92 | 145 | 345 | 38 | 147 | 51 | 191 | 47 | 82 | 28 |
| RTOR Reduction (vph) | 0 | 0 | 42 | 0 | 8 | 0 | 0 | 0 | 148 | 0 | 22 | 0 |
| Lane Group Flow (vph) | 22 | 643 | 50 | 145 | 375 | 0 | 147 | 51 | 43 | 47 | 88 | 0 |
| Confl. Peds. (#/hr) | 10 | | 6 | 6 | | 10 | | | 4 | 4 | | |
| Confl. Bikes (#/hr) | | | 7 | | | 2 | | | 2 | | | 2 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 18.7 | 18.7 | 18.7 | 18.7 | 18.7 | | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 | |
| Effective Green, g (s) | 18.7 | 18.7 | 18.7 | 18.7 | 18.7 | | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 | |
| Actuated g/C Ratio | 0.54 | 0.54 | 0.54 | 0.54 | 0.54 | | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 1026 | 1010 | 842 | 315 | 993 | | 286 | 800 | 348 | 303 | 1099 | |
| v/s Ratio Prot | c0.35 | | | 0.20 | | | | 0.01 | | | 0.02 | |
| v/s Ratio Perm | 0.01 | | 0.03 | 0.25 | | | c0.12 | | 0.03 | 0.04 | | |
| v/c Ratio | 0.02 | 0.64 | 0.06 | 0.46 | 0.38 | | 0.51 | 0.06 | 0.12 | 0.16 | 0.08 | |
| Uniform Delay, d1 | 3.7 | 5.5 | 3.7 | 4.8 | 4.5 | | 11.7 | 10.5 | 10.6 | 10.7 | 10.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 1.3 | 0.0 | 1.1 | 0.2 | | 1.6 | 0.0 | 0.2 | 0.2 | 0.0 | |
| Delay (s) | 3.7 | 6.8 | 3.8 | 5.9 | 4.8 | | 13.2 | 10.5 | 10.8 | 10.9 | 10.6 | |
| Level of Service | A | A | A | A | A | | B | B | B | B | B | |
| Approach Delay (s) | | 6.4 | | | 5.1 | | | 11.7 | | | 10.7 | |
| Approach LOS | | A | | | A | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 7.5 | | | | HCM Level of Service | | | A | | |
| HCM Volume to Capacity ratio | | | 0.60 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 34.5 | | | | Sum of lost time (s) | | | 8.0 | | |
| Intersection Capacity Utilization | | | 62.7% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

2: Cutting Blvd & San Pablo Ave

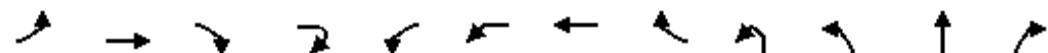
6/7/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|-------|--------|-------|----------------------|------|--------|-------|------|------|-------|------|
| Lane Configurations | 1 | | 2,3 | 1,2 | 1,2 | 1 | 1,2 | 1,2 | | 1 | 1,2 | 1 |
| Volume (vph) | 199 | 0 | 810 | 115 | 258 | 52 | 356 | 435 | 0 | 0 | 514 | 174 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | | | 0.95 | 1.00 |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | 3433 | 5085 | | | 3539 | 1583 |
| Flt Permitted | 0.58 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 1080 | | 2787 | 3433 | 3539 | 1583 | 3526 | 5085 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 216 | 0 | 880 | 125 | 280 | 57 | 387 | 473 | 0 | 0 | 559 | 189 |
| RTOR Reduction (vph) | 0 | 0 | 548 | 0 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 136 |
| Lane Group Flow (vph) | 216 | 0 | 332 | 125 | 280 | 11 | 387 | 473 | 0 | 0 | 559 | 53 |
| Turn Type | custom | | custom | Perm | | Perm | custom | | | | Perm | |
| Protected Phases | | | | | 3 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 5 | 3 | | 3 | 5 | | | | 6 | |
| Actuated Green, G (s) | 12.2 | | 19.8 | 10.5 | 10.5 | 10.5 | 4.1 | 22.8 | | | 15.7 | 15.7 |
| Effective Green, g (s) | 12.2 | | 19.8 | 10.5 | 10.5 | 10.5 | 4.1 | 22.8 | | | 15.7 | 15.7 |
| Actuated g/C Ratio | 0.22 | | 0.35 | 0.19 | 0.19 | 0.19 | 0.07 | 0.40 | | | 0.28 | 0.28 |
| Clearance Time (s) | 3.5 | | | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 233 | | 977 | 638 | 658 | 294 | 256 | 2052 | | | 983 | 440 |
| v/s Ratio Prot | | | | c0.08 | | | 0.09 | | | | c0.16 | |
| v/s Ratio Perm | c0.20 | | 0.12 | 0.04 | | 0.01 | c0.11 | | | | 0.03 | |
| v/c Ratio | 0.93 | | 0.34 | 0.20 | 0.43 | 0.04 | 1.51 | 0.23 | | | 0.57 | 0.12 |
| Uniform Delay, d1 | 21.7 | | 13.5 | 19.4 | 20.3 | 18.9 | 26.2 | 11.1 | | | 17.5 | 15.2 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 39.1 | | 0.2 | 0.2 | 0.4 | 0.1 | 249.4 | 0.1 | | | 0.8 | 0.1 |
| Delay (s) | 60.8 | | 13.7 | 19.6 | 20.8 | 18.9 | 275.6 | 11.1 | | | 18.3 | 15.4 |
| Level of Service | E | | B | B | C | B | F | B | | | B | B |
| Approach Delay (s) | | 23.0 | | | 20.2 | | | 130.2 | | | 17.5 | |
| Approach LOS | | C | | | C | | | F | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 50.4 | | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | 0.73 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 56.5 | | | Sum of lost time (s) | | | 14.0 | | | | |
| Intersection Capacity Utilization | | 57.5% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|------------------------|-------|------|------|------|------|------|-------|------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 16 | 33 | 24 | 2 | 43 | 40 | 5 | 72 | 33 | 8 | 509 | 93 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.98 | 1.00 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1833 | 1583 | | | | | 1779 | 1583 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.24 | 1.00 | | | | | 0.70 | 1.00 | | 0.08 | 1.00 | 1.00 |
| Satd. Flow (perm) | 449 | 1583 | | | | | 1301 | 1583 | | 148 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 17 | 36 | 26 | 2 | 47 | 43 | 5 | 78 | 36 | 9 | 553 | 101 |
| RTOR Reduction (vph) | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 71 | 0 | 0 | 0 | 63 |
| Lane Group Flow (vph) | 0 | 53 | 26 | 0 | 0 | 0 | 95 | 7 | 0 | 45 | 553 | 38 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | pm+pt | pm+pt | | Perm |
| Protected Phases | | 3 | | | | | | 7 | | 5 | 5 | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | 2 |
| Actuated Green, G (s) | 14.0 | 14.0 | | | | | 11.3 | 11.3 | | 57.7 | 50.2 | 50.2 |
| Effective Green, g (s) | 14.0 | 14.0 | | | | | 11.3 | 11.3 | | 57.7 | 50.2 | 50.2 |
| Actuated g/C Ratio | 0.11 | 0.11 | | | | | 0.09 | 0.09 | | 0.43 | 0.38 | 0.38 |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 47 | 167 | | | | | 111 | 135 | | 156 | 1339 | 599 |
| v/s Ratio Prot | | | | | | | | | | 0.02 | 0.16 | |
| v/s Ratio Perm | c0.12 | 0.02 | | | | | c0.07 | 0.00 | | 0.11 | 0.02 | |
| v/c Ratio | 1.13 | 0.16 | | | | | 0.86 | 0.05 | | 0.29 | 0.41 | 0.06 |
| Uniform Delay, d1 | 59.3 | 54.0 | | | | | 59.9 | 55.8 | | 26.6 | 30.4 | 26.3 |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 171.1 | 0.4 | | | | | 43.7 | 0.2 | | 1.0 | 0.2 | 0.0 |
| Delay (s) | 230.4 | 54.4 | | | | | 103.6 | 55.9 | | 27.6 | 30.6 | 26.3 |
| Level of Service | F | D | | | | | F | E | | C | C | C |
| Approach Delay (s) | 169.6 | | | | | | 82.1 | | | | 29.8 | |
| Approach LOS | F | | | | | | F | | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 41.0 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.89 | | |
| Actuated Cycle Length (s) | 132.7 | Sum of lost time (s) | 20.0 |
| Intersection Capacity Utilization | 80.3% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | | | ↑↑ | | ↑ |
| Volume (vph) | 569 | 925 | 379 | 10 | 13 | 168 | 119 | 16 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | | | | 0.97 | | 0.91 |
| Fr _t | 1.00 | 0.96 | | | | 0.94 | | 0.85 |
| Flt Protected | 0.95 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | 3433 | 3382 | | | | 3298 | 1441 | |
| Flt Permitted | 0.31 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | 1136 | 3382 | | | | 3298 | 1441 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 618 | 1005 | 412 | 11 | 14 | 183 | 129 | 17 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 13 |
| Lane Group Flow (vph) | 618 | 1427 | 0 | 0 | 0 | 328 | 0 | 2 |
| Turn Type | pm+pt | | | | Perm | | | Perm |
| Protected Phases | 1 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | 73.0 | 62.5 | | | | 18.4 | | 18.4 |
| Effective Green, g (s) | 73.0 | 62.5 | | | | 18.4 | | 18.4 |
| Actuated g/C Ratio | 0.55 | 0.47 | | | | 0.14 | | 0.14 |
| Clearance Time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 950 | 1593 | | | | 457 | | 200 |
| v/s Ratio Prot | c0.09 | c0.42 | | | | | | |
| v/s Ratio Perm | 0.27 | | | | | 0.10 | | 0.00 |
| v/c Ratio | 0.65 | 0.90 | | | | 0.72 | | 0.01 |
| Uniform Delay, d1 | 17.9 | 32.1 | | | | 54.7 | | 49.3 |
| Progression Factor | 1.00 | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 1.6 | 7.0 | | | | 5.3 | | 0.0 |
| Delay (s) | 19.5 | 39.1 | | | | 60.0 | | 49.3 |
| Level of Service | B | D | | | | E | | D |
| Approach Delay (s) | | 33.2 | | | | 59.5 | | |
| Approach LOS | | C | | | | E | | |

Intersection Summary

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

4: Potrero Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|-------|------|-------|------|------|-------|-------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↗ | ↑ ↘ | ↑ ↗ ↘ | ↑ ↘ | ↑ ↗ | ↑ ↘ | ↑ ↗ | ↑ ↘ | ↑ ↗ ↘ | ↑ ↗ |
| Volume (vph) | 51 | 288 | 192 | 108 | 403 | 105 | 132 | 437 | 15 | 116 | 858 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3430 | | 1770 | 3522 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.33 | 1.00 | 1.00 | 0.39 | 1.00 | | 0.22 | 1.00 | | 0.44 | 1.00 | 1.00 |
| Satd. Flow (perm) | 607 | 1863 | 1583 | 730 | 3430 | | 413 | 3522 | | 817 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 55 | 313 | 209 | 117 | 438 | 114 | 143 | 475 | 16 | 126 | 933 | 37 |
| RTOR Reduction (vph) | 0 | 0 | 148 | 0 | 42 | 0 | 0 | 3 | 0 | 0 | 0 | 21 |
| Lane Group Flow (vph) | 55 | 313 | 61 | 117 | 510 | 0 | 143 | 488 | 0 | 126 | 933 | 16 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | 14.9 | 14.9 | 14.9 | 14.9 | 14.9 | | 25.7 | 21.9 | | 27.1 | 22.6 | 22.6 |
| Effective Green, g (s) | 14.9 | 14.9 | 14.9 | 14.9 | 14.9 | | 25.7 | 21.9 | | 27.1 | 22.6 | 22.6 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | | 0.50 | 0.43 | | 0.53 | 0.44 | 0.44 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 176 | 541 | 460 | 212 | 996 | | 307 | 1504 | | 515 | 1559 | 697 |
| v/s Ratio Prot | c0.17 | | | 0.15 | | | c0.03 | 0.14 | | c0.02 | c0.26 | |
| v/s Ratio Perm | 0.09 | | 0.04 | 0.16 | | | 0.20 | | | 0.11 | | 0.01 |
| v/c Ratio | 0.31 | 0.58 | 0.13 | 0.55 | 0.51 | | 0.47 | 0.32 | | 0.24 | 0.60 | 0.02 |
| Uniform Delay, d1 | 14.2 | 15.5 | 13.4 | 15.4 | 15.2 | | 7.4 | 9.8 | | 6.2 | 10.9 | 8.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.0 | 1.5 | 0.1 | 3.1 | 0.4 | | 1.1 | 0.1 | | 0.2 | 0.6 | 0.0 |
| Delay (s) | 15.2 | 17.0 | 13.6 | 18.5 | 15.6 | | 8.5 | 9.9 | | 6.4 | 11.5 | 8.1 |
| Level of Service | B | B | B | B | B | | A | A | | A | B | A |
| Approach Delay (s) | | 15.6 | | | 16.1 | | | 9.6 | | | 10.8 | |
| Approach LOS | | B | | | B | | | A | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 12.7 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.57 | | |
| Actuated Cycle Length (s) | 51.3 | Sum of lost time (s) | 9.0 |
| Intersection Capacity Utilization | 65.5% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |



| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
|---------------------------|-------|------|-------|------|-------|-------|-------|
| Lane Configurations | ↑ ↗ | ↑ ↗ | ↗ ↘ | ↑ ↗ | | ↗ ↘ | ↑ ↗ |
| Volume (vph) | 336 | 98 | 35 | 493 | 101 | 165 | 848 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 |
| Frpb, ped/bikes | 1.00 | 0.98 | 1.00 | 0.99 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1546 | 1770 | 3429 | | 1767 | 3539 |
| Fl _t Permitted | 0.95 | 1.00 | 0.25 | 1.00 | | 0.33 | 1.00 |
| Satd. Flow (perm) | 1770 | 1546 | 465 | 3429 | | 621 | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 365 | 107 | 38 | 536 | 110 | 179 | 922 |
| RTOR Reduction (vph) | 0 | 74 | 0 | 24 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 365 | 33 | 38 | 622 | 0 | 179 | 922 |
| Confl. Peds. (#/hr) | 1 | 20 | | | 10 | 10 | |
| Confl. Bikes (#/hr) | | | | | 2 | | |
| Turn Type | | Perm | pm+pt | | pm+pt | | |
| Protected Phases | 4 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | 4 | 2 | | | 6 | |
| Actuated Green, G (s) | 15.2 | 15.2 | 23.1 | 21.7 | | 26.3 | 23.3 |
| Effective Green, g (s) | 15.2 | 15.2 | 23.1 | 21.7 | | 26.3 | 23.3 |
| Actuated g/C Ratio | 0.30 | 0.30 | 0.46 | 0.43 | | 0.53 | 0.47 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 539 | 471 | 252 | 1491 | | 396 | 1652 |
| v/s Ratio Prot | c0.21 | | 0.00 | 0.18 | | c0.03 | c0.26 |
| v/s Ratio Perm | | 0.02 | 0.07 | | | 0.21 | |
| v/c Ratio | 0.68 | 0.07 | 0.15 | 0.42 | | 0.45 | 0.56 |
| Uniform Delay, d1 | 15.2 | 12.3 | 7.5 | 9.7 | | 6.4 | 9.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.4 | 0.1 | 0.3 | 0.2 | | 0.8 | 0.4 |
| Delay (s) | 18.6 | 12.4 | 7.8 | 9.9 | | 7.3 | 10.0 |
| Level of Service | B | B | A | A | | A | B |
| Approach Delay (s) | 17.2 | | | 9.8 | | | 9.6 |
| Approach LOS | B | | | A | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.2 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.60 | | |
| Actuated Cycle Length (s) | 49.9 | Sum of lost time (s) | 9.0 |
| Intersection Capacity Utilization | 56.9% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

6: Central Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|------|--------|------|-------|------|------|-------|-------|------|
| Lane Configurations | 1 | 2 | 3 | | | | 4 | 5 | | 6 | 7 | 8 |
| Volume (vph) | 145 | 272 | 101 | 109 | 306 | 38 | 19 | 495 | 75 | 38 | 650 | 198 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1681 | 1765 | 1583 | | 3454 | | 1770 | 3469 | | 1770 | 3415 | |
| Flt Permitted | 0.47 | 0.97 | 1.00 | | 0.55 | | 0.16 | 1.00 | | 0.24 | 1.00 | |
| Satd. Flow (perm) | 836 | 1708 | 1583 | | 1918 | | 291 | 3469 | | 454 | 3415 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 158 | 296 | 110 | 118 | 333 | 41 | 21 | 538 | 82 | 41 | 707 | 215 |
| RTOR Reduction (vph) | 0 | 0 | 83 | 0 | 6 | 0 | 0 | 11 | 0 | 0 | 25 | 0 |
| Lane Group Flow (vph) | 142 | 312 | 27 | 0 | 486 | 0 | 21 | 609 | 0 | 41 | 897 | 0 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | |
| Protected Phases | | 4 | | | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 3 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 21.9 | 21.9 | 21.9 | | 26.4 | | 27.7 | 25.6 | | 28.9 | 26.2 | |
| Effective Green, g (s) | 21.9 | 21.9 | 21.9 | | 26.4 | | 27.7 | 25.6 | | 28.9 | 26.2 | |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | | 0.29 | | 0.31 | 0.28 | | 0.32 | 0.29 | |
| Clearance Time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 203 | 415 | 385 | | 562 | | 124 | 986 | | 185 | 993 | |
| v/s Ratio Prot | | | | | | | 0.00 | 0.18 | | c0.01 | c0.26 | |
| v/s Ratio Perm | 0.17 | c0.18 | 0.02 | | c0.25 | | 0.05 | | | 0.06 | | |
| v/c Ratio | 0.70 | 0.75 | 0.07 | | 1.30dl | | 0.17 | 0.62 | | 0.22 | 0.90 | |
| Uniform Delay, d1 | 31.1 | 31.6 | 26.3 | | 30.2 | | 23.9 | 28.0 | | 22.0 | 30.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 10.1 | 7.5 | 0.1 | | 13.0 | | 0.6 | 1.2 | | 0.6 | 11.3 | |
| Delay (s) | 41.2 | 39.1 | 26.3 | | 43.2 | | 24.6 | 29.2 | | 22.6 | 42.0 | |
| Level of Service | D | D | C | | D | | C | C | | C | D | |
| Approach Delay (s) | | 37.1 | | | 43.2 | | | 29.0 | | | 41.2 | |
| Approach LOS | | D | | | D | | | C | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 37.8 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.82 | | |
| Actuated Cycle Length (s) | 90.1 | Sum of lost time (s) | 12.5 |
| Intersection Capacity Utilization | 68.7% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |

dl Defacto Left Lane. Recode with 1 though lane as a left lane.

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project AM Peak

7: Fairmont Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|-------|------|-------|------|------|-------|-------|------|-------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | | | ↔ ↔ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | |
| Volume (vph) | 2 | 232 | 14 | 94 | 212 | 114 | 24 | 363 | 77 | 107 | 746 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 0.99 | 1.00 | |
| Fr _t | 1.00 | 0.99 | | | 0.96 | | 1.00 | 0.97 | | 1.00 | 1.00 | |
| Fl _t Protected | 0.95 | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1745 | 1844 | | | 3316 | | 1769 | 3407 | | 1756 | 3524 | |
| Fl _t Permitted | 0.42 | 1.00 | | | 0.75 | | 0.33 | 1.00 | | 0.41 | 1.00 | |
| Satd. Flow (perm) | 772 | 1844 | | | 2499 | | 605 | 3407 | | 764 | 3524 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 252 | 15 | 102 | 230 | 124 | 26 | 395 | 84 | 116 | 811 | 22 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 64 | 0 | 0 | 24 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 2 | 263 | 0 | 0 | 392 | 0 | 26 | 455 | 0 | 116 | 831 | 0 |
| Confl. Peds. (#/hr) | 43 | | 22 | 22 | | 43 | 10 | | 37 | 37 | | 10 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | | | pm+pt | | | pm+pt | | | |
| Protected Phases | | 4 | | | 8 | | 1 | 6 | | 5 | | 2 |
| Permitted Phases | 4 | | | 8 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 13.6 | 13.6 | | | 13.6 | | 24.3 | 23.7 | | 30.5 | | 26.9 |
| Effective Green, g (s) | 13.6 | 13.6 | | | 13.6 | | 24.3 | 23.7 | | 30.5 | | 26.9 |
| Actuated g/C Ratio | 0.26 | 0.26 | | | 0.26 | | 0.47 | 0.45 | | 0.59 | | 0.52 |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | 3.0 | 3.0 | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 202 | 481 | | | 652 | | 296 | 1550 | | 520 | | 1819 |
| v/s Ratio Prot | | 0.14 | | | | | 0.00 | 0.13 | | c0.02 | | c0.24 |
| v/s Ratio Perm | 0.00 | | | c0.16 | | | 0.04 | | | 0.11 | | |
| v/c Ratio | 0.01 | 0.55 | | | 0.60 | | 0.09 | 0.29 | | 0.22 | | 0.46 |
| Uniform Delay, d1 | 14.3 | 16.6 | | | 16.9 | | 7.5 | 8.9 | | 4.9 | | 8.0 |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 0.0 | 1.3 | | | 1.6 | | 0.1 | 0.1 | | 0.2 | | 0.2 |
| Delay (s) | 14.3 | 17.9 | | | 18.4 | | 7.7 | 9.0 | | 5.2 | | 8.2 |
| Level of Service | B | B | | | B | | A | A | | A | | A |
| Approach Delay (s) | | 17.8 | | | 18.4 | | | 9.0 | | | 7.8 | |
| Approach LOS | | B | | | B | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.5 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.47 | | |
| Actuated Cycle Length (s) | 52.1 | Sum of lost time (s) | 7.0 |
| Intersection Capacity Utilization | 74.7% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak

1: MacDonald Ave & San Pablo Ave

9/19/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑↑ | | | ↔ | | | ↔ | |
| Volume (vph) | 20 | 592 | 85 | 133 | 317 | 35 | 135 | 47 | 176 | 43 | 75 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | | 0.98 | | | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | | | 0.93 | | | 0.98 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.98 | | | 0.99 | |
| Satd. Flow (prot) | 3393 | 1863 | 1517 | 1770 | 1830 | | | 1678 | | | 1783 | |
| Fl _t Permitted | 0.41 | 1.00 | 1.00 | 0.18 | 1.00 | | | 0.98 | | | 0.99 | |
| Satd. Flow (perm) | 1479 | 1863 | 1517 | 340 | 1830 | | | 1678 | | | 1783 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 22 | 643 | 92 | 145 | 345 | 38 | 147 | 51 | 191 | 47 | 82 | 28 |
| RTOR Reduction (vph) | 0 | 0 | 50 | 0 | 4 | 0 | 0 | 38 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 22 | 643 | 42 | 145 | 379 | 0 | 0 | 351 | 0 | 0 | 148 | 0 |
| Confl. Peds. (#/hr) | 10 | | 6 | 6 | | 10 | | | 4 | 4 | | |
| Confl. Bikes (#/hr) | | | 7 | | | 2 | | | 2 | | | 2 |
| Turn Type | Perm | | Perm | Perm | | | Split | | | Split | | |
| Protected Phases | | 4 | | | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | | | |
| Actuated Green, G (s) | 41.0 | 41.0 | 41.0 | 41.0 | 41.0 | | | 21.0 | | | 16.0 | |
| Effective Green, g (s) | 41.0 | 41.0 | 41.0 | 41.0 | 41.0 | | | 21.0 | | | 16.0 | |
| Actuated g/C Ratio | 0.46 | 0.46 | 0.46 | 0.46 | 0.46 | | | 0.23 | | | 0.18 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 674 | 849 | 691 | 155 | 834 | | | 392 | | | 317 | |
| v/s Ratio Prot | | 0.35 | | | 0.21 | | | c0.21 | | | c0.08 | |
| v/s Ratio Perm | 0.01 | | 0.03 | c0.43 | | | | | | | | |
| v/c Ratio | 0.03 | 0.76 | 0.06 | 0.94 | 0.45 | | | 0.89 | | | 0.47 | |
| Uniform Delay, d ₁ | 13.5 | 20.4 | 13.7 | 23.2 | 16.8 | | | 33.4 | | | 33.2 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d ₂ | 0.1 | 6.3 | 0.2 | 56.9 | 1.8 | | | 25.4 | | | 4.9 | |
| Delay (s) | 13.6 | 26.6 | 13.9 | 80.1 | 18.6 | | | 58.8 | | | 38.0 | |
| Level of Service | B | C | B | F | B | | | E | | | D | |
| Approach Delay (s) | | 24.7 | | | 35.5 | | | 58.8 | | | 38.0 | |
| Approach LOS | | C | | | D | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 36.2 | | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | 0.83 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 90.0 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 76.1% | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

1: MacDonald Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|-------|------|-------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑↑ | |
| Volume (vph) | 33 | 436 | 117 | 229 | 837 | 97 | 321 | 105 | 284 | 31 | 59 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.96 | 1.00 | 0.98 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | | 0.96 | 1.00 | 1.00 | 0.98 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 3433 | 1863 | 1515 | 1747 | 1828 | | 1706 | 3539 | 1518 | 1741 | 4755 | |
| Flt Permitted | 0.10 | 1.00 | 1.00 | 0.41 | 1.00 | | 0.69 | 1.00 | 1.00 | 0.68 | 1.00 | |
| Satd. Flow (perm) | 368 | 1863 | 1515 | 757 | 1828 | | 1241 | 3539 | 1518 | 1246 | 4755 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 36 | 474 | 127 | 249 | 910 | 105 | 349 | 114 | 309 | 34 | 64 | 29 |
| RTOR Reduction (vph) | 0 | 0 | 54 | 0 | 6 | 0 | 0 | 0 | 214 | 0 | 20 | 0 |
| Lane Group Flow (vph) | 36 | 474 | 73 | 249 | 1009 | 0 | 349 | 114 | 95 | 34 | 73 | 0 |
| Confl. Peds. (#/hr) | 12 | | 24 | 24 | | 12 | 19 | | 9 | 9 | | 19 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 2 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 39.3 | 39.3 | 39.3 | 39.3 | 39.3 | | 21.1 | 21.1 | 21.1 | 21.1 | 21.1 | |
| Effective Green, g (s) | 39.3 | 39.3 | 39.3 | 39.3 | 39.3 | | 21.1 | 21.1 | 21.1 | 21.1 | 21.1 | |
| Actuated g/C Ratio | 0.57 | 0.57 | 0.57 | 0.57 | 0.57 | | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 211 | 1070 | 870 | 435 | 1050 | | 383 | 1092 | 468 | 384 | 1467 | |
| v/s Ratio Prot | | 0.25 | | | c0.55 | | | 0.03 | | | 0.02 | |
| v/s Ratio Perm | 0.10 | | 0.05 | 0.33 | | | c0.28 | | 0.06 | 0.03 | | |
| v/c Ratio | 0.17 | 0.44 | 0.08 | 0.57 | 0.96 | | 0.91 | 0.10 | 0.20 | 0.09 | 0.05 | |
| Uniform Delay, d1 | 6.9 | 8.3 | 6.5 | 9.2 | 13.8 | | 22.7 | 16.9 | 17.5 | 16.8 | 16.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.3 | 0.0 | 1.8 | 19.0 | | 25.3 | 0.0 | 0.2 | 0.1 | 0.0 | |
| Delay (s) | 7.2 | 8.6 | 6.5 | 11.0 | 32.8 | | 48.0 | 16.9 | 17.7 | 16.9 | 16.6 | |
| Level of Service | A | A | A | B | C | | D | B | B | B | B | |
| Approach Delay (s) | | 8.1 | | | 28.5 | | | 31.3 | | | 16.7 | |
| Approach LOS | | A | | | C | | | C | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 24.1 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.94 | | |
| Actuated Cycle Length (s) | 68.4 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 87.8% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

2: Cutting Blvd & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|--------|------|--------|-------|------|------|--------|-------|------|------|-------|------|
| Lane Configurations | ↑ | | ↑↑↑ | ↑↑↑ | ↑↑↑ | ↑↑↑ | ↑↑↑ | ↑↑↑ | | ↑↑↑ | ↑↑↑ | ↑↑↑ |
| Volume (vph) | 209 | 0 | 620 | 108 | 545 | 96 | 513 | 951 | 0 | 0 | 625 | 213 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | | | 0.95 | 1.00 |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | 3433 | 5085 | | | 3539 | 1583 |
| Flt Permitted | 0.43 | | 1.00 | 0.95 | 1.00 | 1.00 | 0.98 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 798 | | 2787 | 3433 | 3539 | 1583 | 3526 | 5085 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 227 | 0 | 674 | 117 | 592 | 104 | 558 | 1034 | 0 | 0 | 679 | 232 |
| RTOR Reduction (vph) | 0 | 0 | 481 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 141 |
| Lane Group Flow (vph) | 227 | 0 | 193 | 117 | 592 | 71 | 558 | 1034 | 0 | 0 | 679 | 91 |
| Turn Type | custom | | custom | Perm | | Perm | custom | | | | Perm | |
| Protected Phases | | | | | 3 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 5 | 3 | | 3 | 5 | | | | 6 | |
| Actuated Green, G (s) | 12.2 | | 19.8 | 19.3 | 19.3 | 19.3 | 4.1 | 26.7 | | | 19.6 | 19.6 |
| Effective Green, g (s) | 12.2 | | 19.8 | 19.3 | 19.3 | 19.3 | 4.1 | 26.7 | | | 19.6 | 19.6 |
| Actuated g/C Ratio | 0.18 | | 0.29 | 0.28 | 0.28 | 0.28 | 0.06 | 0.39 | | | 0.28 | 0.28 |
| Clearance Time (s) | 3.5 | | | 3.5 | 3.5 | 3.5 | 3.0 | 4.0 | | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 141 | | 797 | 957 | 987 | 442 | 209 | 1962 | | | 1002 | 448 |
| v/s Ratio Prot | | | | c0.17 | | | 0.20 | | | | c0.19 | |
| v/s Ratio Perm | c0.28 | | 0.07 | 0.03 | | 0.04 | c0.16 | | | | 0.06 | |
| v/c Ratio | 1.61 | | 0.24 | 0.12 | 0.60 | 0.16 | 2.67 | 0.53 | | | 0.68 | 0.20 |
| Uniform Delay, d1 | 28.5 | | 18.9 | 18.6 | 21.6 | 18.8 | 32.6 | 16.4 | | | 22.0 | 18.9 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 304.8 | | 0.2 | 0.1 | 1.0 | 0.2 | 765.0 | 0.3 | | | 1.8 | 0.2 |
| Delay (s) | 333.3 | | 19.1 | 18.7 | 22.6 | 19.0 | 797.5 | 16.6 | | | 23.8 | 19.1 |
| Level of Service | F | | B | B | C | B | F | B | | | C | B |
| Approach Delay (s) | 98.3 | | | | 21.6 | | | 290.3 | | | 22.6 | |
| Approach LOS | F | | | | C | | | F | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 139.6 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.01 | | |
| Actuated Cycle Length (s) | 69.2 | Sum of lost time (s) | 14.0 |
| Intersection Capacity Utilization | 71.9% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

3: Peerless Ave & San Pablo Ave

6/7/2012

| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR | |
|-----------------------------------|-------|------|----------------------|------|------|------|-------|------|-------|-------|------|------|-----|
| Lane Configurations | | | | | | | | | | | | | |
| Volume (vph) | 50 | 35 | 38 | 2 | 32 | 34 | 16 | 258 | 66 | 26 | 1016 | 124 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | | | | | | | | | | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 0.95 | 1.00 | |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 0.97 | 1.00 | | | | | 0.96 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1810 | 1583 | | | | | 1790 | 1583 | | 1770 | 3539 | 1583 | |
| Flt Permitted | 0.15 | 1.00 | | | | | 0.71 | 1.00 | | 0.09 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 276 | 1583 | | | | | 1313 | 1583 | | 173 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Adj. Flow (vph) | 54 | 38 | 41 | 2 | 35 | 37 | 17 | 280 | 72 | 28 | 1104 | 135 | |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 265 | 0 | 0 | 0 | 87 | |
| Lane Group Flow (vph) | 0 | 92 | 42 | 0 | 0 | 0 | 89 | 15 | 0 | 100 | 1104 | 48 | |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | pm+pt | pm+pt | | Perm | |
| Protected Phases | | 3 | | | | | | 7 | | 5 | 5 | 2 | |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | 2 | |
| Actuated Green, G (s) | 42.0 | 42.0 | | | | | 8.0 | 8.0 | | 53.0 | 43.0 | 43.0 | |
| Effective Green, g (s) | 42.0 | 42.0 | | | | | 8.0 | 8.0 | | 53.0 | 43.0 | 43.0 | |
| Actuated g/C Ratio | 0.29 | 0.29 | | | | | 0.05 | 0.05 | | 0.36 | 0.29 | 0.29 | |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 79 | 453 | | | | | 72 | 86 | | 171 | 1037 | 464 | |
| v/s Ratio Prot | | | | | | | | | | 0.04 | 0.31 | | |
| v/s Ratio Perm | c0.33 | 0.03 | | | | | c0.07 | 0.01 | | 0.17 | | 0.03 | |
| v/c Ratio | 1.16 | 0.09 | | | | | 1.24 | 0.18 | | 0.58 | 1.06 | 0.10 | |
| Uniform Delay, d1 | 52.4 | 38.4 | | | | | 69.4 | 66.3 | | 37.2 | 51.9 | 37.8 | |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 152.4 | 0.1 | | | | | 182.5 | 1.0 | | 5.0 | 46.8 | 0.1 | |
| Delay (s) | 204.8 | 38.5 | | | | | 251.9 | 67.2 | | 42.3 | 98.7 | 37.9 | |
| Level of Service | F | D | | | | | F | E | | D | F | D | |
| Approach Delay (s) | 151.8 | | | | | | 111.8 | | | | 88.4 | | |
| Approach LOS | F | | | | | | F | | | | F | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM Average Control Delay | 103.2 | | HCM Level of Service | | | | | | | F | | | |
| HCM Volume to Capacity ratio | 1.13 | | | | | | | | | | | | |
| Actuated Cycle Length (s) | 146.8 | | Sum of lost time (s) | | | | | | 20.0 | | | | |
| Intersection Capacity Utilization | 75.4% | | ICU Level of Service | | | | | | D | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

3: Peerless Ave & San Pablo Ave

6/7/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | | | ↑↑ | | ↑ |
| Volume (vph) | 350 | 732 | 255 | 9 | 15 | 296 | 122 | 50 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | | | | 0.97 | | 1.00 |
| Fr _t | 1.00 | 0.96 | | | | 0.96 | | 0.85 |
| Flt Protected | 0.95 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | 3433 | 3399 | | | | 3341 | | 1583 |
| Flt Permitted | 0.09 | 1.00 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | 336 | 3399 | | | | 3341 | | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 380 | 796 | 277 | 10 | 16 | 322 | 133 | 54 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 45 |
| Lane Group Flow (vph) | 380 | 1082 | 0 | 0 | 0 | 471 | 0 | 9 |
| Turn Type | pm+pt | | | Perm | | | Perm | |
| Protected Phases | 1 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | 52.0 | 43.0 | | | | 24.8 | | 24.8 |
| Effective Green, g (s) | 52.0 | 43.0 | | | | 24.8 | | 24.8 |
| Actuated g/C Ratio | 0.35 | 0.29 | | | | 0.17 | | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | | | | 4.0 | | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | | | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 309 | 996 | | | | 564 | | 267 |
| v/s Ratio Prot | c0.08 | 0.32 | | | | | | |
| v/s Ratio Perm | c0.36 | | | | | 0.14 | | 0.01 |
| v/c Ratio | 1.23 | 1.09 | | | | 0.84 | | 0.03 |
| Uniform Delay, d1 | 40.4 | 51.9 | | | | 59.0 | | 51.0 |
| Progression Factor | 1.00 | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | 128.5 | 55.0 | | | | 10.3 | | 0.1 |
| Delay (s) | 168.9 | 106.9 | | | | 69.4 | | 51.0 |
| Level of Service | F | F | | | | E | | D |
| Approach Delay (s) | | 123.0 | | | | 67.5 | | |
| Approach LOS | | F | | | | E | | |

Intersection Summary

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

4: Potrero Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|------|-------|-------|------|------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 114 | 206 | 167 | 75 | 200 | 67 | 149 | 1037 | 28 | 88 | 661 | 102 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3406 | | 1770 | 3525 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.56 | 1.00 | 1.00 | 0.51 | 1.00 | | 0.32 | 1.00 | | 0.17 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1036 | 1863 | 1583 | 953 | 3406 | | 590 | 3525 | | 324 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 124 | 224 | 182 | 82 | 217 | 73 | 162 | 1127 | 30 | 96 | 718 | 111 |
| RTOR Reduction (vph) | 0 | 0 | 135 | 0 | 54 | 0 | 0 | 3 | 0 | 0 | 0 | 60 |
| Lane Group Flow (vph) | 124 | 224 | 47 | 82 | 236 | 0 | 162 | 1154 | 0 | 96 | 718 | 51 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | 12.9 | 12.9 | 12.9 | 12.9 | 12.9 | | 27.6 | 23.8 | | 26.0 | 23.0 | 23.0 |
| Effective Green, g (s) | 12.9 | 12.9 | 12.9 | 12.9 | 12.9 | | 27.6 | 23.8 | | 26.0 | 23.0 | 23.0 |
| Actuated g/C Ratio | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 | | 0.56 | 0.48 | | 0.52 | 0.46 | 0.46 |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 269 | 484 | 411 | 247 | 884 | | 418 | 1688 | | 257 | 1638 | 733 |
| v/s Ratio Prot | c0.12 | | | 0.07 | | c0.03 | c0.33 | | | 0.02 | 0.20 | |
| v/s Ratio Perm | 0.12 | | 0.03 | 0.09 | | | 0.19 | | | 0.17 | | 0.03 |
| v/c Ratio | 0.46 | 0.46 | 0.11 | 0.33 | 0.27 | | 0.39 | 0.68 | | 0.37 | 0.44 | 0.07 |
| Uniform Delay, d1 | 15.5 | 15.5 | 14.0 | 14.9 | 14.6 | | 5.6 | 10.0 | | 6.9 | 9.0 | 7.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.3 | 0.7 | 0.1 | 0.8 | 0.2 | | 0.6 | 1.2 | | 0.9 | 0.2 | 0.0 |
| Delay (s) | 16.7 | 16.2 | 14.2 | 15.7 | 14.8 | | 6.2 | 11.2 | | 7.8 | 9.2 | 7.5 |
| Level of Service | B | B | B | B | B | | A | B | | A | A | A |
| Approach Delay (s) | | 15.6 | | | 15.0 | | | 10.6 | | | 8.8 | |
| Approach LOS | | B | | | B | | | B | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.4 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.58 | | |
| Actuated Cycle Length (s) | 49.7 | Sum of lost time (s) | 9.0 |
| Intersection Capacity Utilization | 62.8% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |



| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
|---------------------------|-------|------|-------|-------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↔ | ↑↑ | | ↑ | ↑↑ |
| Volume (vph) | 226 | 72 | 65 | 1173 | 147 | 155 | 682 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 4.0 | | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 |
| Frpb, ped/bikes | 1.00 | 0.96 | 1.00 | 0.99 | | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 1519 | 1770 | 3460 | | 1769 | 3539 |
| Fl _t Permitted | 0.95 | 1.00 | 0.37 | 1.00 | | 0.11 | 1.00 |
| Satd. Flow (perm) | 1770 | 1519 | 684 | 3460 | | 206 | 3539 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 246 | 78 | 71 | 1275 | 160 | 168 | 741 |
| RTOR Reduction (vph) | 0 | 61 | 0 | 11 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 246 | 17 | 71 | 1424 | 0 | 168 | 741 |
| Confl. Peds. (#/hr) | | | 41 | | 18 | 18 | |
| Confl. Bikes (#/hr) | | | | | 8 | | |
| Turn Type | | Perm | pm+pt | | pm+pt | | |
| Protected Phases | 4 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | | 4 | 2 | | 6 | | |
| Actuated Green, G (s) | 13.8 | 13.8 | 35.5 | 33.3 | 41.3 | 36.2 | |
| Effective Green, g (s) | 13.8 | 13.8 | 35.5 | 33.3 | 41.3 | 36.2 | |
| Actuated g/C Ratio | 0.22 | 0.22 | 0.57 | 0.54 | 0.66 | 0.58 | |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 4.0 | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 393 | 337 | 429 | 1852 | 265 | 2060 | |
| v/s Ratio Prot | c0.14 | | 0.01 | c0.41 | c0.05 | 0.21 | |
| v/s Ratio Perm | | 0.01 | 0.09 | | 0.37 | | |
| v/c Ratio | 0.63 | 0.05 | 0.17 | 0.77 | 0.63 | 0.36 | |
| Uniform Delay, d1 | 21.9 | 19.0 | 6.0 | 11.4 | 8.9 | 6.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 3.1 | 0.1 | 0.2 | 2.0 | 4.9 | 0.1 | |
| Delay (s) | 25.0 | 19.1 | 6.2 | 13.4 | 13.8 | 7.0 | |
| Level of Service | C | B | A | B | B | A | |
| Approach Delay (s) | 23.6 | | | 13.0 | | 8.2 | |
| Approach LOS | C | | | B | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 12.7 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.76 | | |
| Actuated Cycle Length (s) | 62.2 | Sum of lost time (s) | 13.0 |
| Intersection Capacity Utilization | 75.2% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

6: Central Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|-------|------|-------|------|------|-------|------|------|
| Lane Configurations | 1 | 4 | 1 | | | | 1 | 4 | | 1 | 4 | |
| Volume (vph) | 413 | 247 | 165 | 56 | 226 | 82 | 172 | 935 | 61 | 48 | 622 | 226 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.97 | | 1.00 | 0.99 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 0.98 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1681 | 1741 | 1583 | | 3394 | | 1770 | 3507 | | 1770 | 3398 | |
| Flt Permitted | 0.52 | 0.74 | 1.00 | | 0.52 | | 0.09 | 1.00 | | 0.10 | 1.00 | |
| Satd. Flow (perm) | 917 | 1305 | 1583 | | 1765 | | 171 | 3507 | | 184 | 3398 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 449 | 268 | 179 | 61 | 246 | 89 | 187 | 1016 | 66 | 52 | 676 | 246 |
| RTOR Reduction (vph) | 0 | 0 | 117 | 0 | 18 | 0 | 0 | 3 | 0 | 0 | 25 | 0 |
| Lane Group Flow (vph) | 319 | 398 | 62 | 0 | 378 | 0 | 187 | 1079 | 0 | 52 | 897 | 0 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | | pm+pt | | |
| Protected Phases | | 4 | | | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | 3 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 50.5 | 50.5 | 50.5 | | 30.0 | | 54.5 | 48.3 | | 43.7 | 40.5 | |
| Effective Green, g (s) | 50.5 | 50.5 | 50.5 | | 30.0 | | 54.5 | 48.3 | | 43.7 | 40.5 | |
| Actuated g/C Ratio | 0.35 | 0.35 | 0.35 | | 0.21 | | 0.37 | 0.33 | | 0.30 | 0.28 | |
| Clearance Time (s) | 3.5 | 3.5 | 3.5 | | 3.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 318 | 453 | 549 | | 364 | | 185 | 1164 | | 90 | 946 | |
| v/s Ratio Prot | | | | | | | c0.08 | 0.31 | | 0.01 | 0.26 | |
| v/s Ratio Perm | c0.35 | 0.30 | 0.04 | | c0.21 | | c0.30 | | | 0.16 | | |
| v/c Ratio | 1.00 | 0.88 | 0.11 | | 1.04 | | 1.01 | 0.93 | | 0.58 | 0.95 | |
| Uniform Delay, d1 | 47.5 | 44.6 | 32.3 | | 57.8 | | 39.7 | 46.9 | | 40.7 | 51.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 51.3 | 17.3 | 0.1 | | 57.3 | | 69.0 | 12.4 | | 8.7 | 17.8 | |
| Delay (s) | 98.8 | 61.9 | 32.4 | | 115.0 | | 108.7 | 59.3 | | 49.4 | 69.3 | |
| Level of Service | F | E | C | | F | | F | E | | D | E | |
| Approach Delay (s) | 69.1 | | | | 115.0 | | | 66.6 | | | 68.2 | |
| Approach LOS | | E | | | F | | | E | | | E | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 73.1 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.00 | | |
| Actuated Cycle Length (s) | 145.5 | Sum of lost time (s) | 9.5 |
| Intersection Capacity Utilization | 75.7% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) No Project PM Peak

7: Fairmont Ave & San Pablo Ave

6/7/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|-------|-------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↑ | ↑ | | | ↔ | | ↑ | ↑ | | ↑ | ↑ | |
| Volume (vph) | 11 | 183 | 17 | 118 | 184 | 60 | 77 | 1106 | 131 | 96 | 866 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.99 | | | 0.98 | | 1.00 | 0.98 | | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | | 0.98 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1756 | 1834 | | | 3365 | | 1768 | 3470 | | 1769 | 3531 | |
| Flt Permitted | 0.46 | 1.00 | | | 0.74 | | 0.22 | 1.00 | | 0.15 | 1.00 | |
| Satd. Flow (perm) | 859 | 1834 | | | 2531 | | 406 | 3470 | | 273 | 3531 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 199 | 18 | 128 | 200 | 65 | 84 | 1202 | 142 | 104 | 941 | 12 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 28 | 0 | 0 | 11 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 12 | 212 | 0 | 0 | 365 | 0 | 84 | 1333 | 0 | 104 | 952 | 0 |
| Confl. Peds. (#/hr) | 21 | | 30 | 30 | | 21 | 30 | | 10 | 10 | | 30 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 4 | | | 1 |
| Turn Type | Perm | | Perm | | | pm+pt | | | pm+pt | | | |
| Protected Phases | | 4 | | | 8 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | | 8 | | | 6 | | | 2 | | |
| Actuated Green, G (s) | 13.7 | 13.7 | | | 13.7 | | 31.7 | 28.0 | | 30.3 | 27.3 | |
| Effective Green, g (s) | 13.7 | 13.7 | | | 13.7 | | 31.7 | 28.0 | | 30.3 | 27.3 | |
| Actuated g/C Ratio | 0.25 | 0.25 | | | 0.25 | | 0.57 | 0.50 | | 0.54 | 0.49 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | 3.0 | 4.0 | | 3.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 211 | 451 | | | 623 | | 322 | 1744 | | 229 | 1731 | |
| v/s Ratio Prot | | 0.12 | | | | | c0.02 | c0.38 | | c0.02 | 0.27 | |
| v/s Ratio Perm | 0.01 | | | | c0.14 | | 0.13 | | | 0.22 | | |
| v/c Ratio | 0.06 | 0.47 | | | 0.59 | | 0.26 | 0.76 | | 0.45 | 0.55 | |
| Uniform Delay, d1 | 16.1 | 17.9 | | | 18.5 | | 6.1 | 11.2 | | 8.1 | 9.9 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.1 | 0.8 | | | 1.4 | | 0.4 | 2.0 | | 1.4 | 0.4 | |
| Delay (s) | 16.2 | 18.7 | | | 19.9 | | 6.5 | 13.2 | | 9.5 | 10.3 | |
| Level of Service | B | B | | | B | | A | B | | A | B | |
| Approach Delay (s) | | 18.5 | | | 19.9 | | | 12.8 | | | 10.2 | |
| Approach LOS | | B | | | B | | | B | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 13.3 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.67 | | |
| Actuated Cycle Length (s) | 55.7 | Sum of lost time (s) | 10.0 |
| Intersection Capacity Utilization | 86.5% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak

2: Cutting Blvd & San Pablo Ave

9/19/2012



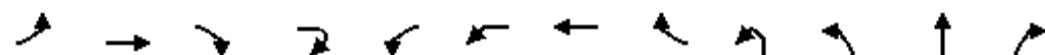
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|----------------------|------|------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 199 | 0 | 810 | 115 | 258 | 52 | 356 | 435 | 0 | 0 | 514 | 174 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | | | 0.97 | |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | | 1822 | | | 1799 | |
| Flt Permitted | 0.48 | | 1.00 | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | |
| Satd. Flow (perm) | 901 | | 2787 | 3433 | 3539 | 1583 | | 1822 | | | 1799 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 216 | 0 | 880 | 125 | 280 | 57 | 387 | 473 | 0 | 0 | 559 | 189 |
| RTOR Reduction (vph) | 0 | 0 | 655 | 0 | 0 | 42 | 0 | 0 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 216 | 0 | 225 | 125 | 280 | 15 | 0 | 860 | 0 | 0 | 740 | 0 |
| Turn Type | custom | | custom | Perm | | Perm | Split | | | Split | | |
| Protected Phases | | | | | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | 37.0 | | 37.0 | 37.0 | 37.0 | 37.0 | | 51.5 | | | 45.0 | |
| Effective Green, g (s) | 37.0 | | 37.0 | 37.0 | 37.0 | 37.0 | | 51.5 | | | 45.0 | |
| Actuated g/C Ratio | 0.26 | | 0.26 | 0.26 | 0.26 | 0.26 | | 0.36 | | | 0.31 | |
| Clearance Time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 230 | | 711 | 876 | 903 | 404 | | 647 | | | 558 | |
| v/s Ratio Prot | | | | 0.08 | | | | c0.47 | | | c0.41 | |
| v/s Ratio Perm | c0.24 | | 0.08 | 0.04 | | 0.01 | | | | | | |
| v/c Ratio | 0.94 | | 0.32 | 0.14 | 0.31 | 0.04 | | 1.33 | | | 1.33 | |
| Uniform Delay, d1 | 52.9 | | 43.7 | 41.7 | 43.7 | 40.6 | | 46.8 | | | 50.0 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 45.4 | | 1.2 | 0.3 | 0.9 | 0.2 | | 158.6 | | | 158.7 | |
| Delay (s) | 98.3 | | 44.9 | 42.1 | 44.6 | 40.8 | | 205.4 | | | 208.7 | |
| Level of Service | F | | D | D | D | D | | F | | | F | |
| Approach Delay (s) | 55.4 | | | | 43.4 | | | 205.4 | | | 208.7 | |
| Approach LOS | E | | | | D | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 130.6 | | HCM Level of Service | | | | | F | | | | |
| HCM Volume to Capacity ratio | 1.22 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 145.0 | | Sum of lost time (s) | | | | | 11.5 | | | | |
| Intersection Capacity Utilization | 111.7% | | ICU Level of Service | | | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak

3: Peerless Ave & San Pablo Ave

9/19/2012

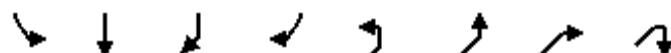


| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|-----------------------------------|--------|------|----------------------|------|------|------|-------|------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 16 | 33 | 24 | 2 | 43 | 40 | 5 | 72 | 33 | 8 | 509 | 93 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | | 0.98 | |
| Flt Protected | 0.98 | 1.00 | | | | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1833 | 1583 | | | | | 1779 | 1583 | | | 1821 | |
| Flt Permitted | 0.31 | 1.00 | | | | | 0.70 | 1.00 | | | 0.89 | |
| Satd. Flow (perm) | 577 | 1583 | | | | | 1301 | 1583 | | | 1625 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 17 | 36 | 26 | 2 | 47 | 43 | 5 | 78 | 36 | 9 | 553 | 101 |
| RTOR Reduction (vph) | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 74 | 0 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 0 | 53 | 26 | 0 | 0 | 0 | 95 | 4 | 0 | 0 | 695 | 0 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | Perm | Perm | | |
| Protected Phases | | 3 | | | | | | 7 | | | | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | |
| Actuated Green, G (s) | 21.0 | 21.0 | | | | | 8.0 | 8.0 | | | 28.0 | |
| Effective Green, g (s) | 21.0 | 21.0 | | | | | 8.0 | 8.0 | | | 28.0 | |
| Actuated g/C Ratio | 0.14 | 0.14 | | | | | 0.05 | 0.05 | | | 0.19 | |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 81 | 222 | | | | | 69 | 84 | | | 303 | |
| v/s Ratio Prot | | | | | | | | | | | | |
| v/s Ratio Perm | c0.09 | 0.02 | | | | | c0.07 | 0.00 | | | c0.43 | |
| v/c Ratio | 0.65 | 0.12 | | | | | 1.38 | 0.05 | | | 2.29 | |
| Uniform Delay, d1 | 61.1 | 56.4 | | | | | 71.0 | 67.4 | | | 61.0 | |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 34.4 | 1.1 | | | | | 237.6 | 1.1 | | | 592.4 | |
| Delay (s) | 95.5 | 57.5 | | | | | 308.6 | 68.5 | | | 653.4 | |
| Level of Service | F | E | | | | | F | E | | | F | |
| Approach Delay (s) | 82.4 | | | | | | 200.3 | | | | 653.4 | |
| Approach LOS | F | | | | | | F | | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 968.0 | | HCM Level of Service | | | | | | F | | | |
| HCM Volume to Capacity ratio | 2.12 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 150.0 | | Sum of lost time (s) | | | | | 20.0 | | | | |
| Intersection Capacity Utilization | 172.5% | | ICU Level of Service | | | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 3: Peerless Ave & San Pablo Ave

9/19/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|-------|--------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | |
| Volume (vph) | 569 | 925 | 379 | 10 | 13 | 168 | 119 | 16 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | | | | | 0.97 | 0.91 | |
| Fr _t | | | | | | 0.94 | 0.85 | |
| Flt Protected | | | | | | 0.97 | 1.00 | |
| Satd. Flow (prot) | | | | | | 3298 | 1441 | |
| Flt Permitted | | | | | | 0.97 | 1.00 | |
| Satd. Flow (perm) | | | | | | 3298 | 1441 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 618 | 1005 | 412 | 11 | 14 | 183 | 129 | 17 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| Lane Group Flow (vph) | 0 | 2046 | 0 | 0 | 0 | 328 | 0 | 3 |
| Turn Type | Split | | | | Perm | | Perm | |
| Protected Phases | 6 | 6 | | | | 4 | | |
| Permitted Phases | | | | | 4 | | | 4 |
| Actuated Green, G (s) | | 45.0 | | | | 28.0 | | 28.0 |
| Effective Green, g (s) | | 45.0 | | | | 28.0 | | 28.0 |
| Actuated g/C Ratio | | 0.30 | | | | 0.19 | | 0.19 |
| Clearance Time (s) | | 4.0 | | | | 4.0 | | 4.0 |
| Lane Grp Cap (vph) | | 535 | | | | 616 | | 269 |
| v/s Ratio Prot | | c1.15 | | | | | | |
| v/s Ratio Perm | | | | | | 0.10 | | 0.00 |
| v/c Ratio | | 3.82 | | | | 0.53 | | 0.01 |
| Uniform Delay, d1 | | 52.5 | | | | 55.1 | | 49.7 |
| Progression Factor | | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | | 1275.5 | | | | 3.3 | | 0.1 |
| Delay (s) | | 1328.0 | | | | 58.4 | | 49.8 |
| Level of Service | | F | | | | E | | D |
| Approach Delay (s) | | 1328.0 | | | | 58.0 | | |
| Approach LOS | | F | | | | E | | |
| Intersection Summary | | | | | | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak

4: Potrero Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|-------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 51 | 288 | 192 | 108 | 403 | 105 | 132 | 437 | 15 | 116 | 858 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | | 1.00 | | | 1.00 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3430 | | | 1836 | | | 1844 | |
| Flt Permitted | 0.18 | 1.00 | 1.00 | 0.19 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (perm) | 332 | 1863 | 1583 | 355 | 3430 | | | 1836 | | | 1844 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 55 | 313 | 209 | 117 | 438 | 114 | 143 | 475 | 16 | 126 | 933 | 37 |
| RTOR Reduction (vph) | 0 | 0 | 164 | 0 | 17 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 55 | 313 | 45 | 117 | 535 | 0 | 0 | 633 | 0 | 0 | 1095 | 0 |
| Turn Type | Perm | | Perm | Perm | | | Split | | | Split | | |
| Protected Phases | | 4 | | | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | | | |
| Actuated Green, G (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | | | 37.0 | | | 58.0 | |
| Effective Green, g (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | | | 37.0 | | | 58.0 | |
| Actuated g/C Ratio | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 | | | 0.27 | | | 0.43 | |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 71 | 400 | 340 | 76 | 737 | | | 503 | | | 792 | |
| v/s Ratio Prot | | 0.17 | | | 0.16 | | | c0.34 | | | c0.59 | |
| v/s Ratio Perm | 0.17 | | 0.03 | c0.33 | | | | | | | | |
| v/c Ratio | 0.77 | 0.78 | 0.13 | 1.54 | 0.73 | | | 1.26 | | | 1.38 | |
| Uniform Delay, d1 | 49.9 | 50.0 | 42.8 | 53.0 | 49.3 | | | 49.0 | | | 38.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 56.1 | 14.1 | 0.8 | 297.8 | 6.2 | | | 131.9 | | | 179.9 | |
| Delay (s) | 106.0 | 64.2 | 43.6 | 350.8 | 55.4 | | | 180.9 | | | 218.4 | |
| Level of Service | F | E | D | F | E | | | F | | | F | |
| Approach Delay (s) | | 60.7 | | | 107.1 | | | 180.9 | | | 218.4 | |
| Approach LOS | | E | | | F | | | F | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 154.8 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.38 | | |
| Actuated Cycle Length (s) | 135.0 | Sum of lost time (s) | 11.0 |
| Intersection Capacity Utilization | 92.4% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak
 5: Moeser Ln & San Pablo Ave

9/19/2012



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|--------|-------|----------------------|------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 336 | 98 | 493 | 136 | 165 | 848 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.92 | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Fr _t | 1.00 | 0.85 | 0.97 | | | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1770 | 1462 | 1785 | | | 1848 |
| Fl _t Permitted | 0.95 | 1.00 | 1.00 | | | 0.99 |
| Satd. Flow (perm) | 1770 | 1462 | 1785 | | | 1848 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 365 | 107 | 536 | 148 | 179 | 922 |
| RTOR Reduction (vph) | 0 | 78 | 7 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 365 | 29 | 677 | 0 | 0 | 1101 |
| Confl. Peds. (#/hr) | 1 | 20 | | 10 | 10 | |
| Confl. Bikes (#/hr) | | | | | | 2 |
| Turn Type | | Perm | | Split | | |
| Protected Phases | 4 | | 2 | | 6 | 6 |
| Permitted Phases | | | 4 | | | |
| Actuated Green, G (s) | 26.0 | 26.0 | 46.0 | | | 67.0 |
| Effective Green, g (s) | 26.0 | 26.0 | 46.0 | | | 67.0 |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.31 | | | 0.45 |
| Clearance Time (s) | 3.0 | 3.0 | 4.0 | | | 4.0 |
| Lane Grp Cap (vph) | 307 | 253 | 547 | | | 825 |
| v/s Ratio Prot | c0.21 | | c0.38 | | | c0.60 |
| v/s Ratio Perm | | | 0.02 | | | |
| v/c Ratio | 1.19 | 0.12 | 1.24 | | | 1.33 |
| Uniform Delay, d1 | 62.0 | 52.3 | 52.0 | | | 41.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 112.8 | 0.9 | 122.0 | | | 158.8 |
| Delay (s) | 174.8 | 53.2 | 174.0 | | | 200.3 |
| Level of Service | F | D | F | | | F |
| Approach Delay (s) | 147.3 | | 174.0 | | | 200.3 |
| Approach LOS | F | | F | | | F |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 181.2 | | HCM Level of Service | | F |
| HCM Volume to Capacity ratio | | 1.27 | | | | |
| Actuated Cycle Length (s) | | 150.0 | | Sum of lost time (s) | | 11.0 |
| Intersection Capacity Utilization | | 119.9% | | ICU Level of Service | | H |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak

6: Central Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|------|------|----------------------|-------|-------|------|------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 145 | 272 | 101 | 0 | 0 | 453 | 0 | 514 | 75 | 0 | 688 | 198 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 0.97 | | | | | | 0.85 | | 0.98 | | | 0.97 |
| Flt Protected | | 0.99 | | | | | | 1.00 | | | | 1.00 |
| Satd. Flow (prot) | | 1789 | | | | | 2787 | | 1831 | | | 1807 |
| Flt Permitted | | 0.99 | | | | | | 1.00 | | | | 1.00 |
| Satd. Flow (perm) | | 1789 | | | | | 2787 | | 1831 | | | 1807 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 158 | 296 | 110 | 0 | 0 | 492 | 0 | 559 | 82 | 0 | 748 | 215 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 0 | 368 | 0 | 4 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 0 | 557 | 0 | 0 | 0 | 124 | 0 | 637 | 0 | 0 | 955 | 0 |
| Turn Type | Perm | | | | | | custom | | | | | |
| Protected Phases | | 4 | | | | | | 6 | | | 2 | |
| Permitted Phases | 4 | | | | | | 8 | | | | | |
| Actuated Green, G (s) | | 33.5 | | | | | 34.0 | | 36.0 | | | 54.0 |
| Effective Green, g (s) | | 33.5 | | | | | 34.0 | | 36.0 | | | 54.0 |
| Actuated g/C Ratio | | 0.25 | | | | | 0.25 | | 0.27 | | | 0.40 |
| Clearance Time (s) | | 3.5 | | | | | 3.0 | | 4.0 | | | 4.0 |
| Lane Grp Cap (vph) | | 444 | | | | | 702 | | 488 | | | 723 |
| v/s Ratio Prot | | | | | | | | c0.35 | | | | c0.53 |
| v/s Ratio Perm | | 0.31 | | | | | 0.04 | | | | | |
| v/c Ratio | | 1.26 | | | | | 0.18 | | 1.31 | | | 1.32 |
| Uniform Delay, d1 | | 50.8 | | | | | 39.5 | | 49.5 | | | 40.5 |
| Progression Factor | | 1.00 | | | | | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | | 132.1 | | | | | 0.5 | | 152.0 | | | 154.1 |
| Delay (s) | | 182.8 | | | | | 40.1 | | 201.5 | | | 194.6 |
| Level of Service | | F | | | | | D | | F | | | F |
| Approach Delay (s) | | 182.8 | | | | | 40.1 | | 201.5 | | | 194.6 |
| Approach LOS | | F | | | | | D | | F | | | F |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 165.2 | | | | | HCM Level of Service | | | F | | |
| HCM Volume to Capacity ratio | | 1.30 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 135.0 | | | | | Sum of lost time (s) | | | 11.5 | | |
| Intersection Capacity Utilization | | 85.9% | | | | | ICU Level of Service | | | E | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project AM Peak

7: Fairmont Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 2 | 232 | 14 | 94 | 212 | 114 | 24 | 363 | 77 | 107 | 746 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | | 0.97 | | | 0.98 | | | 1.00 | |
| Flpb, ped/bikes | 0.96 | 1.00 | | | 0.99 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 0.99 | | | 0.96 | | | 0.98 | | | 1.00 | |
| Fl _t Protected | 0.95 | 1.00 | | | 0.99 | | | 1.00 | | | 0.99 | |
| Satd. Flow (prot) | 1693 | 1839 | | | 3227 | | | 1779 | | | 1845 | |
| Fl _t Permitted | 0.28 | 1.00 | | | 0.61 | | | 1.00 | | | 0.99 | |
| Satd. Flow (perm) | 502 | 1839 | | | 1994 | | | 1779 | | | 1845 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 2 | 252 | 15 | 102 | 230 | 124 | 26 | 395 | 84 | 116 | 811 | 22 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 32 | 0 | 0 | 6 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 2 | 265 | 0 | 0 | 424 | 0 | 0 | 499 | 0 | 0 | 948 | 0 |
| Confl. Peds. (#/hr) | 43 | | 22 | 22 | | 43 | 10 | | 37 | 37 | | 10 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | | | | Split | | | Split | | |
| Protected Phases | | 4 | | | 8 | | 6 | 6 | | 2 | 2 | |
| Permitted Phases | 4 | | 8 | | | | | | | | | |
| Actuated Green, G (s) | 25.0 | 25.0 | | | 25.0 | | | 29.0 | | | 54.0 | |
| Effective Green, g (s) | 25.0 | 25.0 | | | 25.0 | | | 29.0 | | | 54.0 | |
| Actuated g/C Ratio | 0.21 | 0.21 | | | 0.21 | | | 0.24 | | | 0.45 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 105 | 383 | | | 415 | | | 430 | | | 830 | |
| v/s Ratio Prot | | 0.14 | | | | | | c0.28 | | | c0.51 | |
| v/s Ratio Perm | 0.00 | | | | c0.21 | | | | | | | |
| v/c Ratio | 0.02 | 0.69 | | | 1.02 | | | 1.16 | | | 1.14 | |
| Uniform Delay, d1 | 37.8 | 43.9 | | | 47.5 | | | 45.5 | | | 33.0 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.3 | 9.9 | | | 49.5 | | | 95.1 | | | 78.4 | |
| Delay (s) | 38.1 | 53.8 | | | 97.0 | | | 140.6 | | | 111.4 | |
| Level of Service | D | D | | | F | | | F | | | F | |
| Approach Delay (s) | | 53.7 | | | 97.0 | | | 140.6 | | | 111.4 | |
| Approach LOS | | D | | | F | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 108.1 | | | HCM Level of Service | | | F | | | | |
| HCM Volume to Capacity ratio | | 1.12 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 120.0 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 127.1% | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

1: MacDonald Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑↑ | ↑↑ | | ↔ | ↔ | | ↔ | ↔ | ↔ |
| Volume (vph) | 33 | 436 | 117 | 229 | 837 | 97 | 321 | 105 | 284 | 31 | 59 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | 4.0 | | 4.0 | |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.87 | 1.00 | 0.99 | | | | 0.97 | | 0.97 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | | | 0.95 | | 0.97 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.98 | | 0.99 | |
| Satd. Flow (prot) | 3433 | 1863 | 1374 | 1770 | 1825 | | | | 1679 | | 1737 | |
| Fl _t Permitted | 0.06 | 1.00 | 1.00 | 0.30 | 1.00 | | | | 0.98 | | 0.99 | |
| Satd. Flow (perm) | 216 | 1863 | 1374 | 565 | 1825 | | | | 1679 | | 1737 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 36 | 474 | 127 | 249 | 910 | 105 | 349 | 114 | 309 | 34 | 64 | 29 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 3 | 0 | 0 | 16 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 36 | 474 | 57 | 249 | 1012 | 0 | 0 | 756 | 0 | 0 | 120 | 0 |
| Confl. Peds. (#/hr) | 12 | | 24 | 24 | | 12 | 19 | | 9 | 9 | | 19 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 2 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Split | | | Split | | |
| Protected Phases | | 4 | | | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | | | |
| Actuated Green, G (s) | 67.0 | 67.0 | 67.0 | 67.0 | 67.0 | | | 55.0 | | | 16.0 | |
| Effective Green, g (s) | 67.0 | 67.0 | 67.0 | 67.0 | 67.0 | | | 55.0 | | | 16.0 | |
| Actuated g/C Ratio | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 | | | 0.37 | | | 0.11 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 96 | 832 | 614 | 252 | 815 | | | 616 | | | 185 | |
| v/s Ratio Prot | | 0.25 | | | c0.55 | | | c0.45 | | | c0.07 | |
| v/s Ratio Perm | 0.17 | | 0.04 | 0.44 | | | | | | | | |
| v/c Ratio | 0.38 | 0.57 | 0.09 | 0.99 | 1.24 | | | 1.23 | | | 0.65 | |
| Uniform Delay, d1 | 27.6 | 30.8 | 24.0 | 41.1 | 41.5 | | | 47.5 | | | 64.3 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 10.8 | 2.8 | 0.3 | 53.7 | 119.3 | | | 116.3 | | | 16.2 | |
| Delay (s) | 38.4 | 33.6 | 24.2 | 94.8 | 160.8 | | | 163.8 | | | 80.5 | |
| Level of Service | D | C | C | F | F | | | F | | | F | |
| Approach Delay (s) | | 32.0 | | | 147.8 | | | 163.8 | | | 80.5 | |
| Approach LOS | | C | | | F | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 122.8 | | | HCM Level of Service | | | F | | | | |
| HCM Volume to Capacity ratio | | 1.17 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 150.0 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 111.1% | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

2: Cutting Blvd & San Pablo Ave

9/19/2012

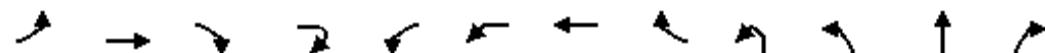


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|--------|--------|----------------------|------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 209 | 0 | 620 | 108 | 545 | 96 | 513 | 951 | 0 | 0 | 625 | 213 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | | 0.88 | 0.97 | 0.95 | 1.00 | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | | | 0.97 | |
| Flt Protected | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | |
| Satd. Flow (prot) | 1770 | | 2787 | 3433 | 3539 | 1583 | | 1831 | | | 1799 | |
| Flt Permitted | 0.23 | | 1.00 | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | |
| Satd. Flow (perm) | 436 | | 2787 | 3433 | 3539 | 1583 | | 1831 | | | 1799 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 227 | 0 | 674 | 117 | 592 | 104 | 558 | 1034 | 0 | 0 | 679 | 232 |
| RTOR Reduction (vph) | 0 | 0 | 486 | 0 | 0 | 58 | 0 | 0 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 227 | 0 | 188 | 117 | 592 | 46 | 0 | 1592 | 0 | 0 | 902 | 0 |
| Turn Type | custom | | custom | Perm | | Perm | Split | | | Split | | |
| Protected Phases | | | | | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | 40.5 | | 40.5 | 40.5 | 40.5 | 40.5 | | 54.0 | | | 39.0 | |
| Effective Green, g (s) | 40.5 | | 40.5 | 40.5 | 40.5 | 40.5 | | 54.0 | | | 39.0 | |
| Actuated g/C Ratio | 0.28 | | 0.28 | 0.28 | 0.28 | 0.28 | | 0.37 | | | 0.27 | |
| Clearance Time (s) | 3.5 | | 3.5 | 3.5 | 3.5 | 3.5 | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 122 | | 778 | 959 | 988 | 442 | | 682 | | | 484 | |
| v/s Ratio Prot | | | | 0.17 | | | | c0.87 | | | c0.50 | |
| v/s Ratio Perm | c0.52 | | 0.07 | 0.03 | | 0.03 | | | | | | |
| v/c Ratio | 1.86 | | 0.24 | 0.12 | 0.60 | 0.10 | | 2.33 | | | 1.86 | |
| Uniform Delay, d1 | 52.2 | | 40.4 | 39.0 | 45.2 | 38.8 | | 45.5 | | | 53.0 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 416.9 | | 0.7 | 0.3 | 2.7 | 0.5 | | 605.0 | | | 396.7 | |
| Delay (s) | 469.2 | | 41.1 | 39.2 | 47.9 | 39.2 | | 650.5 | | | 449.7 | |
| Level of Service | F | | D | D | D | D | | F | | | F | |
| Approach Delay (s) | | 149.0 | | | 45.6 | | | 650.5 | | | 449.7 | |
| Approach LOS | | F | | | D | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 383.3 | | HCM Level of Service | | | | F | | | | |
| HCM Volume to Capacity ratio | | 2.05 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 145.0 | | Sum of lost time (s) | | | | 11.5 | | | | |
| Intersection Capacity Utilization | | 164.3% | | ICU Level of Service | | | | H | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

3: Peerless Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR |
|-----------------------------------|--------|------|----------------------|------|------|------|-------|------|--------|--------|--------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 50 | 35 | 38 | 2 | 32 | 34 | 16 | 258 | 66 | 26 | 1016 | 124 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 0.85 | | | | | 1.00 | 0.85 | | | 0.99 | |
| Flt Protected | 0.97 | 1.00 | | | | | 0.96 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1810 | 1583 | | | | | 1790 | 1583 | | | 1831 | |
| Flt Permitted | 0.12 | 1.00 | | | | | 0.71 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | 227 | 1583 | | | | | 1313 | 1583 | | | 1831 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 54 | 38 | 41 | 2 | 35 | 37 | 17 | 280 | 72 | 28 | 1104 | 135 |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 265 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 92 | 42 | 0 | 0 | 0 | 89 | 15 | 0 | 0 | 1337 | 0 |
| Turn Type | Perm | | Perm | | Perm | Perm | | Perm | custom | custom | | |
| Protected Phases | | 3 | | | | | | 7 | | 2 | 2 | 2 |
| Permitted Phases | 3 | | 3 | | 7 | 7 | | 7 | 2 | 2 | | |
| Actuated Green, G (s) | 26.0 | 26.0 | | | | | 8.0 | 8.0 | | | 33.0 | |
| Effective Green, g (s) | 26.0 | 26.0 | | | | | 8.0 | 8.0 | | | 33.0 | |
| Actuated g/C Ratio | 0.17 | 0.17 | | | | | 0.05 | 0.05 | | | 0.22 | |
| Clearance Time (s) | 4.0 | 4.0 | | | | | 4.0 | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 39 | 274 | | | | | 70 | 84 | | | 403 | |
| v/s Ratio Prot | | | | | | | | | | | c0.73 | |
| v/s Ratio Perm | c0.40 | 0.03 | | | | | c0.07 | 0.01 | | | | |
| v/c Ratio | 2.36 | 0.15 | | | | | 1.27 | 0.18 | | | 3.32 | |
| Uniform Delay, d1 | 62.0 | 52.7 | | | | | 71.0 | 67.9 | | | 58.5 | |
| Progression Factor | 1.00 | 1.00 | | | | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 683.2 | 1.2 | | | | | 196.9 | 4.6 | | | 1048.9 | |
| Delay (s) | 745.2 | 53.8 | | | | | 267.9 | 72.4 | | | 1107.4 | |
| Level of Service | F | D | | | | | F | E | | | F | |
| Approach Delay (s) | 525.0 | | | | | | 119.6 | | | | 1107.4 | |
| Approach LOS | F | | | | | | F | | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 879.8 | | HCM Level of Service | | | | | | F | | | |
| HCM Volume to Capacity ratio | 2.49 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 150.0 | | Sum of lost time (s) | | | | | 20.0 | | | | |
| Intersection Capacity Utilization | 177.4% | | ICU Level of Service | | | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak
 3: Peerless Ave & San Pablo Ave

9/19/2012



| Movement | SBL | SBT | SBR | SBR2 | NEL2 | NEL | NER | NER2 |
|------------------------|--------|--------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | |
| Volume (vph) | 350 | 732 | 255 | 9 | 15 | 296 | 122 | 50 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | | 4.0 | | 4.0 |
| Lane Util. Factor | | 1.00 | | | | 0.97 | | 1.00 |
| Fr _t | | 0.97 | | | | 0.96 | | 0.85 |
| Flt Protected | | 0.99 | | | | 0.97 | | 1.00 |
| Satd. Flow (prot) | | 1790 | | | | 3341 | | 1583 |
| Flt Permitted | | 0.99 | | | | 0.97 | | 1.00 |
| Satd. Flow (perm) | | 1790 | | | | 3341 | | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 380 | 796 | 277 | 10 | 16 | 322 | 133 | 54 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 |
| Lane Group Flow (vph) | 0 | 1463 | 0 | 0 | 0 | 471 | 0 | 10 |
| Turn Type | custom | | | | Perm | | Perm | |
| Protected Phases | 6 | 6 | | | | 4 | | |
| Permitted Phases | 6 | | | | 4 | | | 4 |
| Actuated Green, G (s) | | 35.0 | | | | 28.0 | | 28.0 |
| Effective Green, g (s) | | 35.0 | | | | 28.0 | | 28.0 |
| Actuated g/C Ratio | | 0.23 | | | | 0.19 | | 0.19 |
| Clearance Time (s) | | 4.0 | | | | 4.0 | | 4.0 |
| Lane Grp Cap (vph) | | 418 | | | | 624 | | 295 |
| v/s Ratio Prot | | c0.82 | | | | | | |
| v/s Ratio Perm | | | | | | 0.14 | | 0.01 |
| v/c Ratio | | 3.50 | | | | 0.75 | | 0.03 |
| Uniform Delay, d1 | | 57.5 | | | | 57.8 | | 49.9 |
| Progression Factor | | 1.00 | | | | 1.00 | | 1.00 |
| Incremental Delay, d2 | | 1131.0 | | | | 8.3 | | 0.2 |
| Delay (s) | | 1188.5 | | | | 66.0 | | 50.1 |
| Level of Service | | F | | | | E | | D |
| Approach Delay (s) | | 1188.5 | | | | 64.4 | | |
| Approach LOS | | F | | | | E | | |
| Intersection Summary | | | | | | | | |

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

4: Potrero Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|--------|------|-------|----------------------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑↑ | | ↔ | ↔ | | ↓ | ↔ | ↔ |
| Volume (vph) | 114 | 206 | 167 | 75 | 200 | 67 | 149 | 1037 | 28 | 88 | 661 | 102 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | | 1.00 | | | 0.98 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 3406 | | | 1846 | | | 1823 | |
| Flt Permitted | 0.40 | 1.00 | 1.00 | 0.29 | 1.00 | | | 0.99 | | | 0.99 | |
| Satd. Flow (perm) | 740 | 1863 | 1583 | 536 | 3406 | | | 1846 | | | 1823 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 124 | 224 | 182 | 82 | 217 | 73 | 162 | 1127 | 30 | 96 | 718 | 111 |
| RTOR Reduction (vph) | 0 | 0 | 149 | 0 | 23 | 0 | 0 | 1 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 124 | 224 | 33 | 82 | 267 | 0 | 0 | 1318 | 0 | 0 | 922 | 0 |
| Turn Type | Perm | | Perm | Perm | | | Split | | | Split | | |
| Protected Phases | | 4 | | | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | | | |
| Actuated Green, G (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | | | 62.0 | | | 46.0 | |
| Effective Green, g (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | | | 62.0 | | | 46.0 | |
| Actuated g/C Ratio | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | | | 0.43 | | | 0.32 | |
| Clearance Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 133 | 334 | 284 | 96 | 611 | | | 789 | | | 578 | |
| v/s Ratio Prot | | 0.12 | | | 0.08 | | | c0.71 | | | c0.51 | |
| v/s Ratio Perm | c0.17 | | 0.02 | 0.15 | | | | | | | | |
| v/c Ratio | 0.93 | 0.67 | 0.11 | 0.85 | 0.44 | | | 1.67 | | | 1.59 | |
| Uniform Delay, d1 | 58.6 | 55.5 | 49.9 | 57.7 | 53.0 | | | 41.5 | | | 49.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 61.7 | 10.3 | 0.8 | 58.2 | 2.3 | | | 307.5 | | | 275.6 | |
| Delay (s) | 120.3 | 65.8 | 50.7 | 115.9 | 55.2 | | | 349.0 | | | 325.1 | |
| Level of Service | F | E | D | F | E | | | F | | | F | |
| Approach Delay (s) | | 73.3 | | | 68.6 | | | 349.0 | | | 325.1 | |
| Approach LOS | | E | | | E | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 262.4 | | | HCM Level of Service | | | F | | | | |
| HCM Volume to Capacity ratio | | 1.50 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 145.0 | | | Sum of lost time (s) | | | 11.0 | | | | |
| Intersection Capacity Utilization | | 115.0% | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

5: Moeser Ln & San Pablo Ave

9/19/2012



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|--------|-------|----------------------|------|-------|
| Lane Configurations | ↑ ↗ | ↗ ↑ | ↑ ↘ | ↗ ↘ | ↖ ↘ | ↖ ↑ |
| Volume (vph) | 226 | 72 | 1173 | 212 | 155 | 682 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.86 | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Fr _t | 1.00 | 0.85 | 0.98 | | | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1770 | 1368 | 1799 | | | 1846 |
| Fl _t Permitted | 0.95 | 1.00 | 1.00 | | | 0.99 |
| Satd. Flow (perm) | 1770 | 1368 | 1799 | | | 1846 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 246 | 78 | 1275 | 230 | 168 | 741 |
| RTOR Reduction (vph) | 0 | 64 | 4 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 246 | 14 | 1501 | 0 | 0 | 909 |
| Confl. Peds. (#/hr) | | 41 | | 18 | 18 | |
| Confl. Bikes (#/hr) | | | | 8 | | |
| Turn Type | | Perm | | Split | | |
| Protected Phases | 4 | | 2 | | 6 | 6 |
| Permitted Phases | | 4 | | | | |
| Actuated Green, G (s) | 26.0 | 26.0 | 69.0 | | | 44.0 |
| Effective Green, g (s) | 26.0 | 26.0 | 69.0 | | | 44.0 |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.46 | | | 0.29 |
| Clearance Time (s) | 3.0 | 3.0 | 4.0 | | | 4.0 |
| Lane Grp Cap (vph) | 307 | 237 | 828 | | | 541 |
| v/s Ratio Prot | c0.14 | | c0.83 | | | c0.49 |
| v/s Ratio Perm | | 0.01 | | | | |
| v/c Ratio | 0.80 | 0.06 | 1.81 | | | 1.68 |
| Uniform Delay, d1 | 59.5 | 51.8 | 40.5 | | | 53.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 19.4 | 0.5 | 370.4 | | | 314.1 |
| Delay (s) | 78.9 | 52.2 | 410.9 | | | 367.1 |
| Level of Service | E | D | F | | | F |
| Approach Delay (s) | 72.5 | | 410.9 | | | 367.1 |
| Approach LOS | E | | F | | | F |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 356.3 | | HCM Level of Service | | F |
| HCM Volume to Capacity ratio | | 1.58 | | | | |
| Actuated Cycle Length (s) | | 150.0 | | Sum of lost time (s) | | 11.0 |
| Intersection Capacity Utilization | | 151.0% | | ICU Level of Service | | H |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

6: Central Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|------|------|----------------------|-------|-------|------|------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 413 | 247 | 165 | 0 | 0 | 364 | 0 | 1107 | 61 | 0 | 670 | 226 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | | | | | | | | |
| Lane Util. Factor | | | | | | | | | | | | |
| Fr _t | 0.97 | | | | | | 0.85 | | 0.99 | | | 0.97 |
| Flt Protected | | 0.98 | | | | | | 1.00 | | | | 1.00 |
| Satd. Flow (prot) | | 1768 | | | | | 2787 | | 1850 | | | 1799 |
| Flt Permitted | | 0.98 | | | | | | 1.00 | | | | 1.00 |
| Satd. Flow (perm) | | 1768 | | | | | 2787 | | 1850 | | | 1799 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 449 | 268 | 179 | 0 | 0 | 396 | 0 | 1203 | 66 | 0 | 728 | 246 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 0 | 279 | 0 | 1 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 890 | 0 | 0 | 0 | 117 | 0 | 1268 | 0 | 0 | 965 | 0 |
| Turn Type | Perm | | | | | | custom | | | | | |
| Protected Phases | | 4 | | | | | | | 6 | | | 2 |
| Permitted Phases | 4 | | | | | | 8 | | | | | |
| Actuated Green, G (s) | | 42.5 | | | | | 43.0 | | 49.0 | | | 42.0 |
| Effective Green, g (s) | | 42.5 | | | | | 43.0 | | 49.0 | | | 42.0 |
| Actuated g/C Ratio | | 0.29 | | | | | 0.30 | | 0.34 | | | 0.29 |
| Clearance Time (s) | | 3.5 | | | | | 3.0 | | 4.0 | | | 4.0 |
| Lane Grp Cap (vph) | | 518 | | | | | 826 | | 625 | | | 521 |
| v/s Ratio Prot | | | | | | | | c0.69 | | | | c0.54 |
| v/s Ratio Perm | | 0.50 | | | | | 0.04 | | | | | |
| v/c Ratio | | 1.72 | | | | | 0.14 | | 2.03 | | | 1.85 |
| Uniform Delay, d1 | | 51.2 | | | | | 37.5 | | 48.0 | | | 51.5 |
| Progression Factor | | 1.00 | | | | | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | | 331.0 | | | | | 0.4 | | 468.3 | | | 391.3 |
| Delay (s) | | 382.2 | | | | | 37.8 | | 516.3 | | | 442.8 |
| Level of Service | | F | | | | | D | | F | | | F |
| Approach Delay (s) | | 382.2 | | | | | 37.8 | | 516.3 | | | 442.8 |
| Approach LOS | | F | | | | | D | | F | | | F |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 408.5 | | | | | HCM Level of Service | | | F | | |
| HCM Volume to Capacity ratio | | 1.87 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 145.0 | | | | | Sum of lost time (s) | | | 11.5 | | |
| Intersection Capacity Utilization | | 130.6% | | | | | ICU Level of Service | | | H | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

2022 Central Pressure Zone Pipeline (El Cerrito/Richmond) with Project PM Peak

7: Fairmont Ave & San Pablo Ave

9/19/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|--------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ | ↓ | | | ↔ | | | ↔ | | | ↔ | |
| Volume (vph) | 11 | 183 | 17 | 118 | 184 | 60 | 77 | 1106 | 131 | 96 | 866 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 0.95 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | | 0.99 | | | 0.99 | | | 1.00 | |
| Flpb, ped/bikes | 0.97 | 1.00 | | | 0.98 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 0.99 | | | 0.98 | | | 0.99 | | | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1721 | 1822 | | | 3294 | | | 1822 | | | 1850 | |
| Flt Permitted | 0.27 | 1.00 | | | 0.59 | | | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | 481 | 1822 | | | 1972 | | | 1822 | | | 1850 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 199 | 18 | 128 | 200 | 65 | 84 | 1202 | 142 | 104 | 941 | 12 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 11 | 0 | 0 | 2 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 12 | 215 | 0 | 0 | 382 | 0 | 0 | 1426 | 0 | 0 | 1057 | 0 |
| Confl. Peds. (#/hr) | 21 | | 30 | 30 | | 21 | 30 | | 10 | 10 | | 30 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 4 | | | 1 |
| Turn Type | Perm | | Perm | | | | Split | | | Split | | |
| Protected Phases | | 4 | | | 8 | | 6 | 6 | | 2 | 2 | |
| Permitted Phases | 4 | | 8 | | | | | | | | | |
| Actuated Green, G (s) | 25.0 | 25.0 | | | 25.0 | | | 60.0 | | | 53.0 | |
| Effective Green, g (s) | 25.0 | 25.0 | | | 25.0 | | | 60.0 | | | 53.0 | |
| Actuated g/C Ratio | 0.17 | 0.17 | | | 0.17 | | | 0.40 | | | 0.35 | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Grp Cap (vph) | 80 | 304 | | | 329 | | | 729 | | | 654 | |
| v/s Ratio Prot | | 0.12 | | | | | | c0.78 | | | c0.57 | |
| v/s Ratio Perm | 0.02 | | | | c0.19 | | | | | | | |
| v/c Ratio | 0.15 | 0.71 | | | 1.28dl | | | 1.96 | | | 1.62 | |
| Uniform Delay, d1 | 53.4 | 59.0 | | | 62.5 | | | 45.0 | | | 48.5 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 3.9 | 12.9 | | | 101.0 | | | 435.0 | | | 284.3 | |
| Delay (s) | 57.3 | 72.0 | | | 163.5 | | | 480.0 | | | 332.8 | |
| Level of Service | E | E | | | F | | | F | | | F | |
| Approach Delay (s) | | 71.2 | | | 163.5 | | | 480.0 | | | 332.8 | |
| Approach LOS | | E | | | F | | | F | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|------|
| HCM Average Control Delay | 359.8 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.68 | | |
| Actuated Cycle Length (s) | 150.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 134.9% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

dl Defacto Left Lane. Recode with 1 though lane as a left lane.

c Critical Lane Group

APPENDIX M

Central Pressure Zone Pipeline (Richmond/San Pablo) Level of Service Calculations

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HCM Signalized Intersection Capacity Analysis

1: 23rd St & San Pablo Ave

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|----------------------|------|-------|------|------|------|-------|------|
| Lane Configurations | ↑ | ↓ | ↑ | | ↑ | ↑ | ↑ | ↑↓ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 362 | 316 | 74 | 8 | 238 | 15 | 82 | 224 | 53 | 25 | 386 | 343 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.99 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1681 | 1761 | 1583 | | 1860 | 1583 | 1770 | 3438 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.95 | 0.99 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1681 | 1761 | 1583 | | 1860 | 1583 | 1770 | 3438 | | 1770 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 430 | 375 | 88 | 10 | 283 | 18 | 97 | 266 | 63 | 30 | 458 | 407 |
| RTOR Reduction (vph) | 0 | 0 | 66 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 387 | 418 | 22 | 0 | 293 | 3 | 97 | 329 | 0 | 30 | 458 | 407 |
| Turn Type | Split | | Perm | Split | | Perm | Prot | | Prot | | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 3 | | | | | 6 | |
| Actuated Green, G (s) | 19.6 | 19.6 | 19.6 | | 15.1 | 15.1 | 5.3 | 25.3 | | 2.0 | 22.0 | 22.0 |
| Effective Green, g (s) | 19.6 | 19.6 | 19.6 | | 15.1 | 15.1 | 5.3 | 25.3 | | 2.0 | 22.0 | 22.0 |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.25 | | 0.19 | 0.19 | 0.07 | 0.32 | | 0.03 | 0.28 | 0.28 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 422 | 443 | 398 | | 360 | 306 | 120 | 1115 | | 45 | 998 | 446 |
| v/s Ratio Prot | 0.23 | c0.24 | | | c0.16 | | c0.05 | 0.10 | | 0.02 | 0.13 | |
| v/s Ratio Perm | | | 0.01 | | | 0.00 | | | | | c0.26 | |
| v/c Ratio | 0.92 | 0.94 | 0.06 | | 0.81 | 0.01 | 0.81 | 0.30 | | 0.67 | 0.46 | 0.91 |
| Uniform Delay, d1 | 28.4 | 28.7 | 22.2 | | 30.1 | 25.4 | 35.8 | 19.7 | | 37.7 | 23.1 | 27.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 0.70 | 0.65 | 0.69 |
| Incremental Delay, d2 | 24.4 | 28.8 | 0.1 | | 13.2 | 0.0 | 31.5 | 0.7 | | 30.5 | 1.5 | 24.9 |
| Delay (s) | 52.8 | 57.4 | 22.2 | | 43.3 | 25.4 | 67.4 | 20.4 | | 56.8 | 16.4 | 43.5 |
| Level of Service | D | E | C | | D | C | E | C | | E | B | D |
| Approach Delay (s) | | 52.0 | | | 42.2 | | | 31.1 | | | 30.1 | |
| Approach LOS | | D | | | D | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 39.5 | | | HCM Level of Service | | | | D | | | |
| HCM Volume to Capacity ratio | | 0.89 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 78.0 | | | Sum of lost time (s) | | | | 16.0 | | | |
| Intersection Capacity Utilization | | 66.4% | | | ICU Level of Service | | | | C | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Market Ave & 23rd St

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|------|------|----------------------|-------|------|------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 142 | 196 | 93 | 208 | 165 | 27 | 102 | 318 | 95 | 29 | 527 | 75 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1824 | | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1824 | | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 176 | 243 | 115 | 258 | 204 | 33 | 126 | 394 | 118 | 36 | 653 | 93 |
| RTOR Reduction (vph) | 0 | 0 | 96 | 0 | 7 | 0 | 0 | 0 | 66 | 0 | 0 | 17 |
| Lane Group Flow (vph) | 176 | 243 | 19 | 258 | 230 | 0 | 126 | 394 | 52 | 36 | 653 | 76 |
| Confl. Peds. (#/hr) | | | | | 27 | | | | | | | |
| Turn Type | Split | | Perm | Split | | | Prot | | Perm | Prot | | Perm |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | 2 | | | 6 |
| Actuated Green, G (s) | 14.5 | 14.5 | 14.5 | 15.1 | 15.1 | | 7.1 | 38.0 | 38.0 | 3.4 | 34.3 | 34.3 |
| Effective Green, g (s) | 14.5 | 14.5 | 14.5 | 15.1 | 15.1 | | 7.1 | 38.0 | 38.0 | 3.4 | 34.3 | 34.3 |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | | 0.08 | 0.44 | 0.44 | 0.04 | 0.39 | 0.39 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 295 | 311 | 264 | 307 | 317 | | 144 | 814 | 691 | 69 | 734 | 624 |
| v/s Ratio Prot | 0.10 | c0.13 | | c0.15 | 0.13 | | c0.07 | c0.21 | | 0.02 | c0.35 | |
| v/s Ratio Perm | | | 0.01 | | | | | | 0.03 | | | 0.05 |
| v/c Ratio | 0.60 | 0.78 | 0.07 | 0.84 | 0.73 | | 0.88 | 0.48 | 0.07 | 0.52 | 0.89 | 0.12 |
| Uniform Delay, d1 | 33.5 | 34.7 | 30.6 | 34.8 | 34.0 | | 39.5 | 17.5 | 14.3 | 41.0 | 24.6 | 16.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.2 | 12.0 | 0.1 | 18.3 | 8.1 | | 40.4 | 0.5 | 0.0 | 6.9 | 12.7 | 0.1 |
| Delay (s) | 36.8 | 46.7 | 30.7 | 53.1 | 42.1 | | 79.9 | 18.0 | 14.3 | 47.9 | 37.3 | 16.9 |
| Level of Service | D | D | C | D | D | | E | B | B | D | D | B |
| Approach Delay (s) | | 40.0 | | | 47.8 | | | 29.5 | | | 35.4 | |
| Approach LOS | | D | | | D | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 37.4 | | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | 0.89 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 87.0 | | | | | Sum of lost time (s) | | | 20.0 | | |
| Intersection Capacity Utilization | | 76.3% | | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Rheem Ave & 23rd St

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↔ | ↔ | ↑ | ↑ | ↑↓ | ↑ | ↑ | ↑↓ | ↑ |
| Volume (vph) | 80 | 181 | 128 | 127 | 157 | 35 | 60 | 464 | 138 | 33 | 551 | 43 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.95 | | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | | 1.00 | | 0.99 | 1.00 | | 0.98 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.99 | | 1.00 | 0.97 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1751 | 1863 | 1509 | | 1779 | | 1744 | 3340 | | 1731 | 3477 | |
| Flt Permitted | 0.54 | 1.00 | 1.00 | | 0.78 | | 0.35 | 1.00 | | 0.34 | 1.00 | |
| Satd. Flow (perm) | 1002 | 1863 | 1509 | | 1415 | | 639 | 3340 | | 624 | 3477 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 95 | 215 | 152 | 151 | 186 | 42 | 71 | 551 | 164 | 39 | 654 | 51 |
| RTOR Reduction (vph) | 0 | 0 | 53 | 0 | 12 | 0 | 0 | 65 | 0 | 0 | 13 | 0 |
| Lane Group Flow (vph) | 95 | 215 | 99 | 0 | 367 | 0 | 71 | 650 | 0 | 39 | 692 | 0 |
| Confl. Peds. (#/hr) | 29 | | 48 | 14 | | 82 | 34 | | 67 | 53 | | 63 |
| Confl. Bikes (#/hr) | | | 3 | | | 5 | | | 1 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 13.3 | 13.3 | 13.3 | | 13.3 | | 16.6 | 16.6 | | 16.6 | 16.6 | |
| Effective Green, g (s) | 13.3 | 13.3 | 13.3 | | 13.3 | | 16.6 | 16.6 | | 16.6 | 16.6 | |
| Actuated g/C Ratio | 0.35 | 0.35 | 0.35 | | 0.35 | | 0.44 | 0.44 | | 0.44 | 0.44 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 352 | 654 | 530 | | 497 | | 280 | 1463 | | 273 | 1523 | |
| v/s Ratio Prot | | 0.12 | | | | | 0.19 | | | c0.20 | | |
| v/s Ratio Perm | 0.09 | | 0.07 | | c0.26 | | 0.11 | | | 0.06 | | |
| v/c Ratio | 0.27 | 0.33 | 0.19 | | 0.74 | | 0.25 | 0.44 | | 0.14 | 0.45 | |
| Uniform Delay, d1 | 8.8 | 9.0 | 8.5 | | 10.8 | | 6.7 | 7.4 | | 6.4 | 7.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.3 | 0.2 | | 5.7 | | 2.2 | 1.0 | | 1.1 | 1.0 | |
| Delay (s) | 9.2 | 9.3 | 8.7 | | 16.4 | | 8.9 | 8.4 | | 7.5 | 8.5 | |
| Level of Service | A | A | A | | B | | A | A | | A | A | |
| Approach Delay (s) | | 9.1 | | | 16.4 | | | 8.5 | | | 8.4 | |
| Approach LOS | | A | | | B | | | A | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 9.8 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.58 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 37.9 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 70.7% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Barrett Ave & 23rd St NB

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | | | ↑↑ | | | ↑↑↑ | | | | |
| Volume (vph) | 107 | 395 | 0 | 0 | 447 | 102 | 111 | 461 | 64 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | | | 0.91 | | | | |
| Fr _t | 1.00 | 1.00 | | | 0.97 | | | 0.98 | | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | | | 0.99 | | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3440 | | | 4965 | | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | | | 0.99 | | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3440 | | | 4965 | | | | |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 140 | 518 | 0 | 0 | 586 | 134 | 145 | 604 | 84 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 41 | 0 | 0 | 26 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 140 | 518 | 0 | 0 | 679 | 0 | 0 | 807 | 0 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | | | Perm | | | | |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | | | | | | | | 2 | | | | |
| Actuated Green, G (s) | 4.5 | 22.4 | | | 13.9 | | | 16.4 | | | | |
| Effective Green, g (s) | 4.5 | 22.4 | | | 13.9 | | | 16.4 | | | | |
| Actuated g/C Ratio | 0.10 | 0.48 | | | 0.30 | | | 0.35 | | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | 170 | 1694 | | | 1022 | | | 1740 | | | | |
| v/s Ratio Prot | c0.08 | 0.15 | | | c0.20 | | | | | | | |
| v/s Ratio Perm | | | | | | | | 0.16 | | | | |
| v/c Ratio | 0.82 | 0.31 | | | 0.66 | | | 0.46 | | | | |
| Uniform Delay, d1 | 20.8 | 7.5 | | | 14.4 | | | 11.8 | | | | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | 26.4 | 0.1 | | | 1.6 | | | 0.9 | | | | |
| Delay (s) | 47.2 | 7.6 | | | 16.1 | | | 12.7 | | | | |
| Level of Service | D | A | | | B | | | B | | | | |
| Approach Delay (s) | | 16.0 | | | 16.1 | | | 12.7 | | | 0.0 | |
| Approach LOS | | B | | | B | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 14.8 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.59 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 46.8 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 48.9% | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Macdonald Ave & 23rd St NB

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↑↑ | | | ↑↑ | ↑ | | ↑↑↑ | | | | |
| Volume (vph) | 64 | 241 | 0 | 0 | 265 | 59 | 70 | 589 | 148 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | | 4.0 | 4.0 | | 4.0 | | | |
| Lane Util. Factor | | 0.95 | | | | 0.95 | 1.00 | | 0.91 | | | |
| Fr _t | | 1.00 | | | | 1.00 | 0.85 | | 0.97 | | | |
| Flt Protected | | 0.99 | | | | 1.00 | 1.00 | | 1.00 | | | |
| Satd. Flow (prot) | | 3502 | | | | 3539 | 1583 | | 4924 | | | |
| Flt Permitted | | 0.81 | | | | 1.00 | 1.00 | | 1.00 | | | |
| Satd. Flow (perm) | | 2882 | | | | 3539 | 1583 | | 4924 | | | |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 85 | 319 | 0 | 0 | 351 | 78 | 93 | 781 | 196 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 55 | 0 | 80 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 404 | 0 | 0 | 351 | 23 | 0 | 990 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | | | | | Perm | Perm | | | | | |
| Protected Phases | | 4 | | | | 8 | | | 2 | | | |
| Permitted Phases | 4 | | | | | | 8 | 2 | | | | |
| Actuated Green, G (s) | | 10.3 | | | | 10.3 | 10.3 | | 16.1 | | | |
| Effective Green, g (s) | | 10.3 | | | | 10.3 | 10.3 | | 16.1 | | | |
| Actuated g/C Ratio | | 0.30 | | | | 0.30 | 0.30 | | 0.47 | | | |
| Clearance Time (s) | | 4.0 | | | | 4.0 | 4.0 | | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | | | | 3.0 | 3.0 | | 3.0 | | | |
| Lane Grp Cap (vph) | | 863 | | | | 1060 | 474 | | 2305 | | | |
| v/s Ratio Prot | | | | | 0.10 | | | | | | | |
| v/s Ratio Perm | | c0.14 | | | | | 0.01 | | 0.20 | | | |
| v/c Ratio | | 0.47 | | | | 0.33 | 0.05 | | 0.43 | | | |
| Uniform Delay, d1 | | 9.8 | | | | 9.4 | 8.6 | | 6.1 | | | |
| Progression Factor | | 1.00 | | | | 1.00 | 1.00 | | 1.00 | | | |
| Incremental Delay, d2 | | 0.4 | | | | 0.2 | 0.0 | | 0.6 | | | |
| Delay (s) | | 10.2 | | | | 9.6 | 8.6 | | 6.7 | | | |
| Level of Service | | B | | | | A | A | | A | | | |
| Approach Delay (s) | | 10.2 | | | | 9.4 | | | 6.7 | | 0.0 | |
| Approach LOS | | B | | | | A | | | A | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 8.0 | | | HCM Level of Service | | | | A | | | |
| HCM Volume to Capacity ratio | | 0.44 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 34.4 | | | Sum of lost time (s) | | | | 8.0 | | | |
| Intersection Capacity Utilization | | 46.4% | | | ICU Level of Service | | | | A | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Rumrill Blvd & San Pablo Ave

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|-------|------|------|------|------|------|------|------|------|------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | | ↑ | | | ↑↑ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 265 | 25 | 6 | 28 | 28 | 24 | 0 | 384 | 11 | 33 | 611 | 250 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.97 | | 0.99 | | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | 0.99 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.96 | | | 1.00 | | 1.00 | 1.00 | 0.85 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1539 | | 1737 | | | 3518 | | 1751 | 3539 | 1583 |
| Fl _t Permitted | 0.72 | 1.00 | 1.00 | | 0.91 | | | 1.00 | | 0.46 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1338 | 1863 | 1539 | | 1614 | | | 3518 | | 843 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 328 | 31 | 7 | 35 | 35 | 30 | 0 | 476 | 14 | 41 | 757 | 310 |
| RTOR Reduction (vph) | 0 | 0 | 5 | 0 | 20 | 0 | 0 | 2 | 0 | 0 | 0 | 131 |
| Lane Group Flow (vph) | 328 | 31 | 2 | 0 | 80 | 0 | 0 | 488 | 0 | 41 | 757 | 179 |
| Confl. Peds. (#/hr) | | | 11 | 7 | | 9 | 9 | | 16 | 9 | | |
| Confl. Bikes (#/hr) | | | | | | 1 | | | 1 | | | |
| Turn Type | Perm | | Perm | Perm | | | | | Perm | | Perm | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | 6 | | 6 | |
| Actuated Green, G (s) | 24.9 | 24.9 | 24.9 | | 24.9 | | | 45.1 | | 45.1 | 45.1 | 45.1 |
| Effective Green, g (s) | 24.9 | 24.9 | 24.9 | | 24.9 | | | 45.1 | | 45.1 | 45.1 | 45.1 |
| Actuated g/C Ratio | 0.32 | 0.32 | 0.32 | | 0.32 | | | 0.58 | | 0.58 | 0.58 | 0.58 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 427 | 595 | 491 | | 515 | | | 2034 | | 487 | 2046 | 915 |
| v/s Ratio Prot | | 0.02 | | | | | | 0.14 | | | c0.21 | |
| v/s Ratio Perm | c0.25 | | 0.00 | | 0.05 | | | | | 0.05 | | 0.11 |
| v/c Ratio | 0.77 | 0.05 | 0.00 | | 0.15 | | | 0.24 | | 0.08 | 0.37 | 0.20 |
| Uniform Delay, d1 | 23.9 | 18.4 | 18.1 | | 19.0 | | | 8.1 | | 7.3 | 8.8 | 7.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 0.22 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 8.1 | 0.0 | 0.0 | | 0.1 | | | 0.2 | | 0.3 | 0.5 | 0.5 |
| Delay (s) | 32.0 | 18.4 | 18.1 | | 19.2 | | | 2.0 | | 7.6 | 9.3 | 8.3 |
| Level of Service | C | B | B | | B | | | A | | A | A | A |
| Approach Delay (s) | | 30.6 | | | 19.2 | | | 2.0 | | | 9.0 | |
| Approach LOS | | C | | | B | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.6 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.51 | | |
| Actuated Cycle Length (s) | 78.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 50.1% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

7: Market Ave & Rumrill Blvd

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|----------------------|------|------|------|------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | | ↑ | ↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | |
| Volume (vph) | 31 | 92 | 32 | 160 | 78 | 64 | 42 | 445 | 145 | 56 | 625 | 42 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.93 | | 1.00 | 0.96 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1759 | 1782 | | 1770 | 1720 | | 1770 | 3386 | | 1770 | 3498 | |
| Flt Permitted | 0.63 | 1.00 | | 0.65 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1167 | 1782 | | 1206 | 1720 | | 1770 | 3386 | | 1770 | 3498 | |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 44 | 129 | 45 | 225 | 110 | 90 | 59 | 626 | 204 | 79 | 880 | 59 |
| RTOR Reduction (vph) | 0 | 23 | 0 | 0 | 55 | 0 | 0 | 57 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 44 | 151 | 0 | 225 | 145 | 0 | 59 | 773 | 0 | 79 | 930 | 0 |
| Confl. Peds. (#/hr) | 9 | | 6 | | | 11 | | | 5 | 2 | | 12 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Turn Type | Perm | | Perm | | | Prot | | | Prot | | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | | | | | | | |
| Actuated Green, G (s) | 13.3 | 13.3 | | 13.3 | 13.3 | | 2.0 | 18.3 | | 2.0 | 18.3 | |
| Effective Green, g (s) | 13.3 | 13.3 | | 13.3 | 13.3 | | 2.0 | 18.3 | | 2.0 | 18.3 | |
| Actuated g/C Ratio | 0.29 | 0.29 | | 0.29 | 0.29 | | 0.04 | 0.40 | | 0.04 | 0.40 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 340 | 520 | | 352 | 502 | | 78 | 1359 | | 78 | 1404 | |
| v/s Ratio Prot | | 0.08 | | | 0.08 | | 0.03 | 0.23 | | c0.04 | c0.27 | |
| v/s Ratio Perm | 0.04 | | c0.19 | | | | | | | | | |
| v/c Ratio | 0.13 | 0.29 | | 0.64 | 0.29 | | 0.76 | 0.57 | | 1.01 | 0.66 | |
| Uniform Delay, d1 | 11.9 | 12.5 | | 14.1 | 12.5 | | 21.6 | 10.6 | | 21.8 | 11.1 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.3 | | 3.8 | 0.3 | | 33.5 | 0.5 | | 105.5 | 1.2 | |
| Delay (s) | 12.1 | 12.8 | | 17.9 | 12.8 | | 55.0 | 11.1 | | 127.3 | 12.3 | |
| Level of Service | B | B | | B | B | | E | B | | F | B | |
| Approach Delay (s) | | 12.7 | | | 15.5 | | | 14.1 | | | 21.2 | |
| Approach LOS | | B | | | B | | | B | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 17.0 | | HCM Level of Service | | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.67 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 45.6 | | Sum of lost time (s) | | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 57.0% | | ICU Level of Service | | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Pennsylvania Ave & Harbour Way-10th St

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 1 | 249 | 45 | 384 | 353 | 24 | 35 | 34 | 221 | 21 | 26 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.95 | 1.00 | 1.00 | | | | 1.00 | 0.97 | | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.99 | | | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Fl _t Protected | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.98 | 1.00 | | 0.98 | 1.00 |
| Satd. Flow (prot) | 1862 | 1502 | 1770 | 3500 | | | | 1813 | 1542 | | 1822 | 1555 |
| Fl _t Permitted | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.82 | 1.00 | | 0.84 | 1.00 |
| Satd. Flow (perm) | 1860 | 1502 | 1770 | 3500 | | | | 1528 | 1542 | | 1573 | 1555 |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 1 | 330 | 60 | 509 | 468 | 32 | 46 | 45 | 293 | 28 | 34 | 5 |
| RTOR Reduction (vph) | 0 | 0 | 45 | 0 | 7 | 0 | 0 | 0 | 243 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 0 | 331 | 15 | 509 | 493 | 0 | 0 | 91 | 50 | 0 | 62 | 1 |
| Confl. Peds. (#/hr) | 1 | | 18 | 13 | | 1 | 5 | | 13 | | | 6 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | |
| Turn Type | Perm | | Perm | Prot | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | 3 | | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 13.9 | 13.9 | 19.4 | 37.3 | | | | 9.3 | 9.3 | | 9.3 | 9.3 |
| Effective Green, g (s) | 13.9 | 13.9 | 19.4 | 37.3 | | | | 9.3 | 9.3 | | 9.3 | 9.3 |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.36 | 0.68 | | | | 0.17 | 0.17 | | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 474 | 382 | 629 | 2391 | | | | 260 | 263 | | 268 | 265 |
| v/s Ratio Prot | | | c0.29 | | | | | | | | | |
| v/s Ratio Perm | c0.18 | 0.01 | | 0.14 | | | | c0.06 | 0.03 | | 0.04 | 0.00 |
| v/c Ratio | 0.70 | 0.04 | 0.81 | 0.21 | | | | 0.35 | 0.19 | | 0.23 | 0.00 |
| Uniform Delay, d1 | 18.4 | 15.3 | 15.9 | 3.2 | | | | 20.0 | 19.4 | | 19.6 | 18.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 4.5 | 0.0 | 7.6 | 0.0 | | | | 0.8 | 0.4 | | 0.4 | 0.0 |
| Delay (s) | 22.9 | 15.4 | 23.5 | 3.2 | | | | 20.8 | 19.8 | | 20.0 | 18.8 |
| Level of Service | C | B | C | A | | | | C | B | | C | B |
| Approach Delay (s) | 21.8 | | | 13.5 | | | | 20.0 | | | 19.9 | |
| Approach LOS | C | | | B | | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 16.8 | | | | HCM Level of Service | | | | B | | | |
| HCM Volume to Capacity ratio | 0.67 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 54.6 | | | | Sum of lost time (s) | | | | 12.0 | | | |
| Intersection Capacity Utilization | 61.0% | | | | ICU Level of Service | | | | B | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Macdonald Ave & Harbour Way

5/25/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|-------|-------|----------------------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 23 | 149 | 31 | 63 | 161 | 48 | 130 | 256 | 98 | 79 | 327 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.94 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.94 | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 | | 1.00 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1770 | 1863 | 1490 | 1770 | 1775 | | 1770 | 1863 | 1486 | | 3495 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.99 | |
| Satd. Flow (perm) | 1770 | 1863 | 1490 | 1770 | 1775 | | 1770 | 1863 | 1486 | | 3495 | |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 30 | 193 | 40 | 82 | 209 | 62 | 168 | 332 | 127 | 102 | 424 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 31 | 0 | 15 | 0 | 0 | 0 | 97 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 30 | 193 | 9 | 82 | 256 | 0 | 168 | 332 | 30 | 0 | 532 | 0 |
| Confl. Peds. (#/hr) | | | 41 | | | 18 | | | 40 | | | 19 |
| Confl. Bikes (#/hr) | | | | | | 2 | | | 4 | | | 3 |
| Turn Type | Prot | | Perm | Prot | | | Split | | Perm | Split | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | | | | 4 | | | | | | 2 | | |
| Actuated Green, G (s) | 1.4 | 13.8 | 13.8 | 3.7 | 16.1 | | 14.8 | 14.8 | 14.8 | | 13.9 | |
| Effective Green, g (s) | 1.4 | 13.8 | 13.8 | 3.7 | 16.1 | | 14.8 | 14.8 | 14.8 | | 13.9 | |
| Actuated g/C Ratio | 0.02 | 0.22 | 0.22 | 0.06 | 0.26 | | 0.24 | 0.24 | 0.24 | | 0.22 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 40 | 413 | 331 | 105 | 459 | | 421 | 443 | 354 | | 781 | |
| v/s Ratio Prot | 0.02 | 0.10 | | c0.05 | c0.14 | | 0.09 | c0.18 | | | c0.15 | |
| v/s Ratio Perm | | | | 0.01 | | | | | | 0.02 | | |
| v/c Ratio | 0.75 | 0.47 | 0.03 | 0.78 | 0.56 | | 0.40 | 0.75 | 0.09 | | 0.68 | |
| Uniform Delay, d1 | 30.2 | 21.0 | 18.9 | 28.9 | 20.0 | | 20.0 | 22.0 | 18.4 | | 22.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 55.2 | 0.8 | 0.0 | 30.4 | 1.5 | | 0.6 | 6.8 | 0.1 | | 2.5 | |
| Delay (s) | 85.5 | 21.8 | 19.0 | 59.3 | 21.4 | | 20.6 | 28.8 | 18.5 | | 24.6 | |
| Level of Service | F | C | B | E | C | | C | C | B | | C | |
| Approach Delay (s) | | | 28.7 | | | 30.2 | | | 24.5 | | 24.6 | |
| Approach LOS | | | C | | | C | | | C | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.3 | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | | 0.63 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 62.2 | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 58.7% | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Macdonald Ave & 22nd St SB

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 224 | 60 | 142 | 307 | 0 | 0 | 0 | 0 | 125 | 1049 | 77 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | | 0.95 | |
| Fr _t | | 0.97 | | | 1.00 | | | | | | 0.99 | |
| Flt Protected | | 1.00 | | | 0.98 | | | | | | 1.00 | |
| Satd. Flow (prot) | | 3427 | | | 3484 | | | | | | 3489 | |
| Flt Permitted | | 1.00 | | | 0.74 | | | | | | 1.00 | |
| Satd. Flow (perm) | | 3427 | | | 2608 | | | | | | 3489 | |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 0 | 272 | 73 | 172 | 372 | 0 | 0 | 0 | 0 | 152 | 1272 | 93 |
| RTOR Reduction (vph) | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 0 | 306 | 0 | 0 | 544 | 0 | 0 | 0 | 0 | 0 | 1509 | 0 |
| Turn Type | | | | | Perm | | | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | | | | 6 | |
| Permitted Phases | | | | 8 | | | | | | | 6 | |
| Actuated Green, G (s) | | 14.6 | | | 14.6 | | | | | | 31.0 | |
| Effective Green, g (s) | | 14.6 | | | 14.6 | | | | | | 31.0 | |
| Actuated g/C Ratio | | 0.27 | | | 0.27 | | | | | | 0.58 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | |
| Lane Grp Cap (vph) | | 933 | | | 710 | | | | | | 2018 | |
| v/s Ratio Prot | | 0.09 | | | | | | | | | | |
| v/s Ratio Perm | | | | c0.21 | | | | | | | 0.43 | |
| v/c Ratio | | 0.33 | | | 0.77 | | | | | | 0.75 | |
| Uniform Delay, d1 | | 15.6 | | | 17.9 | | | | | | 8.4 | |
| Progression Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | |
| Incremental Delay, d2 | | 0.2 | | | 5.0 | | | | | | 2.6 | |
| Delay (s) | | 15.8 | | | 22.9 | | | | | | 11.0 | |
| Level of Service | | B | | | C | | | | | | B | |
| Approach Delay (s) | | 15.8 | | | 22.9 | | | 0.0 | | | 11.0 | |
| Approach LOS | | B | | | C | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 14.4 | | | HCM Level of Service | | | | | B | | |
| HCM Volume to Capacity ratio | | 0.75 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 53.6 | | | Sum of lost time (s) | | | | | 8.0 | | |
| Intersection Capacity Utilization | | 73.6% | | | ICU Level of Service | | | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: 23rd St & San Pablo Ave

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|-------|------|-------|-------|------|------|-------|------|
| Lane Configurations | ↑ | ↓ | ↑ | | ↑ | ↑ | ↑ | ↑↓ | | ↑ | ↑↑ | ↑ |
| Volume (vph) | 695 | 174 | 103 | 31 | 201 | 33 | 113 | 607 | 47 | 36 | 378 | 592 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 0.97 | 1.00 | | 0.99 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1681 | 1718 | 1583 | | 1850 | 1583 | 1770 | 3501 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.95 | 0.97 | 1.00 | | 0.99 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1681 | 1718 | 1583 | | 1850 | 1583 | 1770 | 3501 | | 1770 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 808 | 202 | 120 | 36 | 234 | 38 | 131 | 706 | 55 | 42 | 440 | 689 |
| RTOR Reduction (vph) | 0 | 0 | 73 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 501 | 509 | 47 | 0 | 270 | 18 | 131 | 761 | 0 | 42 | 440 | 689 |
| Turn Type | Split | | Perm | Split | | Perm | Prot | | Prot | | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 3 | | | | | 6 | |
| Actuated Green, G (s) | 35.0 | 35.0 | 35.0 | | 17.0 | 17.0 | 9.0 | 54.4 | | 5.6 | 51.0 | 51.0 |
| Effective Green, g (s) | 35.0 | 35.0 | 35.0 | | 17.0 | 17.0 | 9.0 | 54.4 | | 5.6 | 51.0 | 51.0 |
| Actuated g/C Ratio | 0.27 | 0.27 | 0.27 | | 0.13 | 0.13 | 0.07 | 0.42 | | 0.04 | 0.40 | 0.40 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 460 | 470 | 433 | | 246 | 210 | 124 | 1488 | | 77 | 1410 | 631 |
| v/s Ratio Prot | c0.30 | 0.30 | | | c0.15 | | c0.07 | c0.22 | | 0.02 | 0.12 | |
| v/s Ratio Perm | | | 0.03 | | | 0.01 | | | | | c0.44 | |
| v/c Ratio | 1.09 | 1.08 | 0.11 | | 1.10 | 0.09 | 1.06 | 0.51 | | 0.55 | 0.31 | 1.09 |
| Uniform Delay, d1 | 46.5 | 46.5 | 34.8 | | 55.5 | 48.7 | 59.5 | 27.0 | | 60.0 | 26.4 | 38.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.20 | 0.74 | 0.76 |
| Incremental Delay, d2 | 68.2 | 65.7 | 0.1 | | 85.9 | 0.2 | 96.7 | 1.3 | | 7.6 | 0.1 | 63.3 |
| Delay (s) | 114.7 | 112.2 | 34.9 | | 141.4 | 48.9 | 156.2 | 28.3 | | 79.5 | 19.6 | 92.5 |
| Level of Service | F | F | C | | F | D | F | C | | E | B | F |
| Approach Delay (s) | | 105.1 | | | 130.0 | | | 47.1 | | | 64.6 | |
| Approach LOS | | F | | | F | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 79.0 | | | | | | | | E | | |
| HCM Volume to Capacity ratio | | 1.12 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 128.0 | | | | | | | | 20.0 | | |
| Intersection Capacity Utilization | | 78.7% | | | | | | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Market Ave & 23rd St

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|-------|------|----------------------|-------|------|------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ |
| Volume (vph) | 89 | 201 | 121 | 159 | 168 | 23 | 94 | 632 | 80 | 17 | 328 | 62 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1830 | | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1830 | | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 106 | 239 | 144 | 189 | 200 | 27 | 112 | 750 | 95 | 20 | 390 | 74 |
| RTOR Reduction (vph) | 0 | 0 | 119 | 0 | 6 | 0 | 0 | 0 | 29 | 0 | 0 | 22 |
| Lane Group Flow (vph) | 106 | 239 | 25 | 189 | 221 | 0 | 112 | 750 | 66 | 20 | 390 | 52 |
| Confl. Peds. (#/hr) | | | | | 27 | | | | | | | |
| Turn Type | Split | | Perm | Split | | | Prot | | Perm | Prot | | Perm |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | 2 | | | 6 |
| Actuated Green, G (s) | 14.1 | 14.1 | 14.1 | 13.7 | 13.7 | | 8.1 | 36.1 | 36.1 | 1.4 | 29.4 | 29.4 |
| Effective Green, g (s) | 14.1 | 14.1 | 14.1 | 13.7 | 13.7 | | 8.1 | 36.1 | 36.1 | 1.4 | 29.4 | 29.4 |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | | 0.10 | 0.44 | 0.44 | 0.02 | 0.36 | 0.36 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 307 | 323 | 275 | 298 | 308 | | 176 | 827 | 703 | 30 | 674 | 572 |
| v/s Ratio Prot | 0.06 | c0.13 | | 0.11 | c0.12 | | c0.06 | c0.40 | | 0.01 | 0.21 | |
| v/s Ratio Perm | | | 0.02 | | | | | | 0.04 | | | 0.03 |
| v/c Ratio | 0.35 | 0.74 | 0.09 | 0.63 | 0.72 | | 0.64 | 0.91 | 0.09 | 0.67 | 0.58 | 0.09 |
| Uniform Delay, d1 | 29.5 | 31.9 | 28.2 | 31.5 | 32.0 | | 35.2 | 21.0 | 13.1 | 39.7 | 20.9 | 17.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.7 | 8.6 | 0.1 | 4.4 | 7.8 | | 7.3 | 13.5 | 0.1 | 44.1 | 1.2 | 0.1 |
| Delay (s) | 30.2 | 40.5 | 28.4 | 35.8 | 39.7 | | 42.5 | 34.5 | 13.2 | 83.9 | 22.2 | 17.2 |
| Level of Service | C | D | C | D | D | | D | C | B | F | C | B |
| Approach Delay (s) | | 34.7 | | | 38.0 | | | 33.3 | | | 24.0 | |
| Approach LOS | | C | | | D | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 32.5 | | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | 0.84 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 81.3 | | | | | Sum of lost time (s) | | | 16.0 | | |
| Intersection Capacity Utilization | | 76.7% | | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Rheem Ave & 23rd St

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|-------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↔ | ↔ | ↑ | ↑ | ↑↓ | ↑ | ↑ | ↑↓ | ↑ |
| Volume (vph) | 44 | 143 | 91 | 116 | 155 | 64 | 55 | 909 | 178 | 31 | 624 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.94 | | 0.99 | | 1.00 | 0.98 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | | 1.00 | | 0.99 | 1.00 | | 0.99 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.97 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1759 | 1863 | 1496 | | 1757 | | 1746 | 3399 | | 1758 | 3496 | |
| Flt Permitted | 0.47 | 1.00 | 1.00 | | 0.82 | | 0.31 | 1.00 | | 0.16 | 1.00 | |
| Satd. Flow (perm) | 876 | 1863 | 1496 | | 1466 | | 570 | 3399 | | 295 | 3496 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 53 | 172 | 109 | 139 | 186 | 77 | 66 | 1091 | 214 | 37 | 749 | 41 |
| RTOR Reduction (vph) | 0 | 0 | 74 | 0 | 18 | 0 | 0 | 31 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 53 | 172 | 35 | 0 | 384 | 0 | 66 | 1274 | 0 | 37 | 782 | 0 |
| Confl. Peds. (#/hr) | 16 | | 38 | 9 | | 55 | 29 | | 48 | 39 | | 45 |
| Confl. Bikes (#/hr) | | | 14 | | | 9 | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 15.4 | 15.4 | 15.4 | | 15.4 | | 25.1 | 25.1 | | 25.1 | 25.1 | |
| Effective Green, g (s) | 15.4 | 15.4 | 15.4 | | 15.4 | | 25.1 | 25.1 | | 25.1 | 25.1 | |
| Actuated g/C Ratio | 0.32 | 0.32 | 0.32 | | 0.32 | | 0.52 | 0.52 | | 0.52 | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 278 | 592 | 475 | | 465 | | 295 | 1759 | | 153 | 1809 | |
| v/s Ratio Prot | | 0.09 | | | | | c0.37 | | | | 0.22 | |
| v/s Ratio Perm | 0.06 | | 0.02 | | c0.26 | | 0.12 | | | 0.13 | | |
| v/c Ratio | 0.19 | 0.29 | 0.07 | | 0.83 | | 0.22 | 0.72 | | 0.24 | 0.43 | |
| Uniform Delay, d1 | 12.0 | 12.4 | 11.6 | | 15.3 | | 6.4 | 9.0 | | 6.5 | 7.3 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 0.3 | 0.1 | | 11.4 | | 1.7 | 2.6 | | 3.7 | 0.8 | |
| Delay (s) | 12.4 | 12.7 | 11.6 | | 26.8 | | 8.1 | 11.7 | | 10.2 | 8.0 | |
| Level of Service | B | B | B | | C | | A | B | | B | A | |
| Approach Delay (s) | | 12.3 | | | 26.8 | | | 11.5 | | | 8.1 | |
| Approach LOS | | B | | | C | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 12.7 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.76 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 48.5 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 86.3% | | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Barrett Ave & 23rd St NB

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | | | ↑↑ | | ↑↑ | ↑↑↑ | | | | |
| Volume (vph) | 153 | 767 | 0 | 0 | 424 | 66 | 107 | 1131 | 94 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | | | 0.91 | | | | |
| Fr _t | 1.00 | 1.00 | | | 0.98 | | | 0.99 | | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3468 | | | 5011 | | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3468 | | | 5011 | | | | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 188 | 940 | 0 | 0 | 520 | 81 | 131 | 1386 | 115 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 14 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 188 | 940 | 0 | 0 | 580 | 0 | 0 | 1618 | 0 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | | | Perm | | | | |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | | | | | | | | 2 | | | | |
| Actuated Green, G (s) | 8.7 | 27.0 | | | 14.3 | | | 23.1 | | | | |
| Effective Green, g (s) | 8.7 | 27.0 | | | 14.3 | | | 23.1 | | | | |
| Actuated g/C Ratio | 0.15 | 0.46 | | | 0.25 | | | 0.40 | | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | 265 | 1645 | | | 854 | | | 1992 | | | | |
| v/s Ratio Prot | 0.11 | c0.27 | | | c0.17 | | | | | | | |
| v/s Ratio Perm | | | | | | | | 0.32 | | | | |
| v/c Ratio | 0.71 | 0.57 | | | 0.68 | | | 0.81 | | | | |
| Uniform Delay, d1 | 23.5 | 11.3 | | | 19.8 | | | 15.6 | | | | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | 8.4 | 0.5 | | | 2.2 | | | 3.7 | | | | |
| Delay (s) | 31.9 | 11.8 | | | 22.0 | | | 19.3 | | | | |
| Level of Service | C | B | | | C | | | B | | | | |
| Approach Delay (s) | | 15.2 | | | 22.0 | | | 19.3 | | | 0.0 | |
| Approach LOS | | B | | | C | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 18.4 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.70 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 58.1 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 65.2% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Macdonald Ave & 23rd St NB

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|------|----------------------|------|------|------|------|------|------|
| Lane Configurations | | ↑↑ | | | ↑↑ | ↑ | | ↑↑↑ | | | | |
| Volume (vph) | 99 | 355 | 0 | 0 | 384 | 147 | 150 | 1156 | 163 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | | 4.0 | 4.0 | | 4.0 | | | |
| Lane Util. Factor | | 0.95 | | | | 0.95 | 1.00 | | 0.91 | | | |
| Fr _t | | 1.00 | | | | 1.00 | 0.85 | | 0.98 | | | |
| Flt Protected | | 0.99 | | | | 1.00 | 1.00 | | 0.99 | | | |
| Satd. Flow (prot) | | 3501 | | | | 3539 | 1583 | | 4975 | | | |
| Flt Permitted | | 0.77 | | | | 1.00 | 1.00 | | 0.99 | | | |
| Satd. Flow (perm) | | 2738 | | | | 3539 | 1583 | | 4975 | | | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 118 | 422 | 0 | 0 | 456 | 175 | 178 | 1373 | 194 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 36 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 540 | 0 | 0 | 456 | 168 | 0 | 1709 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | | | | | Perm | Perm | | | | | |
| Protected Phases | | 4 | | | | 8 | | | 2 | | | |
| Permitted Phases | 4 | | | | | | 8 | 2 | | | | |
| Actuated Green, G (s) | | 12.5 | | | | 12.5 | 12.5 | | 16.1 | | | |
| Effective Green, g (s) | | 12.5 | | | | 12.5 | 12.5 | | 16.1 | | | |
| Actuated g/C Ratio | | 0.34 | | | | 0.34 | 0.34 | | 0.44 | | | |
| Clearance Time (s) | | 4.0 | | | | 4.0 | 4.0 | | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | | | | 3.0 | 3.0 | | 3.0 | | | |
| Lane Grp Cap (vph) | | 935 | | | | 1209 | 541 | | 2188 | | | |
| v/s Ratio Prot | | | | | 0.13 | | | | | | | |
| v/s Ratio Perm | | c0.20 | | | | | 0.11 | | 0.34 | | | |
| v/c Ratio | | 0.58 | | | | 0.38 | 0.31 | | 0.78 | | | |
| Uniform Delay, d1 | | 9.9 | | | | 9.1 | 8.9 | | 8.7 | | | |
| Progression Factor | | 1.00 | | | | 1.00 | 1.00 | | 1.00 | | | |
| Incremental Delay, d2 | | 0.9 | | | | 0.2 | 0.3 | | 2.8 | | | |
| Delay (s) | | 10.8 | | | | 9.3 | 9.2 | | 11.6 | | | |
| Level of Service | | B | | | | A | A | | B | | | |
| Approach Delay (s) | | 10.8 | | | | 9.3 | | | 11.6 | | 0.0 | |
| Approach LOS | | B | | | | A | | | B | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 10.9 | | | | HCM Level of Service | | | B | | | |
| HCM Volume to Capacity ratio | | 0.69 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 36.6 | | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | 69.6% | | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Rumrill Blvd & San Pablo Ave

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|----------------------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↙ | | ↖ ↗ | | | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↗ | ↑ ↘ |
| Volume (vph) | 381 | 16 | 27 | 31 | 24 | 25 | 0 | 929 | 21 | 24 | 506 | 217 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.93 | | 0.98 | | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | 0.99 | | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.96 | | | 1.00 | | 1.00 | 1.00 | 0.85 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1477 | | 1705 | | | 3518 | | 1770 | 3539 | 1583 |
| Fl _t Permitted | 0.70 | 1.00 | 1.00 | | 0.90 | | | 1.00 | | 0.15 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1295 | 1863 | 1477 | | 1567 | | | 3518 | | 275 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 462 | 19 | 33 | 38 | 29 | 30 | 0 | 1127 | 25 | 29 | 614 | 263 |
| RTOR Reduction (vph) | 0 | 0 | 19 | 0 | 15 | 0 | 0 | 1 | 0 | 0 | 0 | 125 |
| Lane Group Flow (vph) | 462 | 19 | 14 | 0 | 82 | 0 | 0 | 1151 | 0 | 29 | 614 | 138 |
| Confl. Peds. (#/hr) | | | 23 | 12 | | 15 | 11 | | 27 | 15 | | |
| Confl. Bikes (#/hr) | | | 2 | | | 5 | | | 3 | | | |
| Turn Type | Perm | | Perm | Perm | | | | | | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | 6 | | 6 |
| Actuated Green, G (s) | 52.8 | 52.8 | 52.8 | | 52.8 | | | 67.2 | | 67.2 | 67.2 | 67.2 |
| Effective Green, g (s) | 52.8 | 52.8 | 52.8 | | 52.8 | | | 67.2 | | 67.2 | 67.2 | 67.2 |
| Actuated g/C Ratio | 0.41 | 0.41 | 0.41 | | 0.41 | | | 0.52 | | 0.52 | 0.52 | 0.52 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 534 | 768 | 609 | | 646 | | | 1847 | | 144 | 1858 | 831 |
| v/s Ratio Prot | | 0.01 | | | | | | c0.33 | | | 0.17 | |
| v/s Ratio Perm | c0.36 | | 0.01 | 0.05 | | | | | | 0.11 | | 0.09 |
| v/c Ratio | 0.87 | 0.02 | 0.02 | 0.13 | | | | 0.62 | | 0.20 | 0.33 | 0.17 |
| Uniform Delay, d1 | 34.3 | 22.3 | 22.3 | 23.3 | | | | 21.5 | | 16.1 | 17.5 | 15.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | | | 0.45 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 13.7 | 0.0 | 0.0 | 0.1 | | | | 0.9 | | 3.1 | 0.5 | 0.4 |
| Delay (s) | 48.0 | 22.3 | 22.3 | 23.4 | | | | 10.5 | | 19.3 | 17.9 | 16.3 |
| Level of Service | D | C | C | C | | | | B | | B | B | B |
| Approach Delay (s) | | 45.4 | | 23.4 | | | | 10.5 | | | 17.5 | |
| Approach LOS | | D | | C | | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 20.1 | | HCM Level of Service | | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.73 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 128.0 | | Sum of lost time (s) | | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 67.5% | | ICU Level of Service | | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Market Ave & Rumrill Blvd

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|----------------------|------|------|------|-------|------|-------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | |
| Volume (vph) | 76 | 115 | 51 | 136 | 108 | 71 | 75 | 640 | 224 | 71 | 398 | 56 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.95 | | 1.00 | 0.94 | | 1.00 | 0.96 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1762 | 1758 | | 1770 | 1736 | | 1770 | 3367 | | 1770 | 3454 | |
| Flt Permitted | 0.58 | 1.00 | | 0.61 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1071 | 1758 | | 1134 | 1736 | | 1770 | 3367 | | 1770 | 3454 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 90 | 137 | 61 | 162 | 128 | 84 | 89 | 760 | 266 | 84 | 473 | 66 |
| RTOR Reduction (vph) | 0 | 32 | 0 | 0 | 48 | 0 | 0 | 56 | 0 | 0 | 18 | 0 |
| Lane Group Flow (vph) | 90 | 166 | 0 | 162 | 164 | 0 | 89 | 970 | 0 | 84 | 521 | 0 |
| Confl. Peds. (#/hr) | 7 | | 18 | | | 13 | | | 13 | 6 | | 18 |
| Confl. Bikes (#/hr) | | | 7 | | | 1 | | | 2 | | | 2 |
| Turn Type | Perm | | Perm | | | Prot | | | Prot | | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | | | | | | | |
| Actuated Green, G (s) | 9.3 | 9.3 | | 9.3 | 9.3 | | 5.0 | 20.9 | | 2.4 | 18.3 | |
| Effective Green, g (s) | 9.3 | 9.3 | | 9.3 | 9.3 | | 5.0 | 20.9 | | 2.4 | 18.3 | |
| Actuated g/C Ratio | 0.21 | 0.21 | | 0.21 | 0.21 | | 0.11 | 0.47 | | 0.05 | 0.41 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 223 | 367 | | 236 | 362 | | 198 | 1578 | | 95 | 1417 | |
| v/s Ratio Prot | | 0.09 | | | 0.09 | | 0.05 | c0.29 | | c0.05 | 0.15 | |
| v/s Ratio Perm | 0.08 | | c0.14 | | | | | | | | | |
| v/c Ratio | 0.40 | 0.45 | | 0.69 | 0.45 | | 0.45 | 0.61 | | 0.88 | 0.37 | |
| Uniform Delay, d1 | 15.3 | 15.4 | | 16.3 | 15.4 | | 18.5 | 8.8 | | 21.0 | 9.1 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.2 | 0.9 | | 8.0 | 0.9 | | 1.6 | 0.7 | | 56.2 | 0.2 | |
| Delay (s) | 16.4 | 16.3 | | 24.3 | 16.3 | | 20.1 | 9.6 | | 77.2 | 9.3 | |
| Level of Service | B | B | | C | B | | C | A | | E | A | |
| Approach Delay (s) | | 16.3 | | | 19.8 | | | 10.4 | | | 18.4 | |
| Approach LOS | | B | | | B | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 14.7 | | HCM Level of Service | | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.65 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 44.6 | | Sum of lost time (s) | | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 67.1% | | ICU Level of Service | | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Pennsylvania Ave & Harbour Way-10th St

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|----------------------|------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 5 | 256 | 44 | 252 | 252 | 32 | 26 | 56 | 444 | 20 | 29 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.96 | 1.00 | 1.00 | | | | 1.00 | 0.98 | | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.98 | | | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Fl _t Protected | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.98 | 1.00 | | 0.98 | 1.00 |
| Satd. Flow (prot) | 1861 | 1514 | 1770 | 3469 | | | | 1829 | 1556 | | 1825 | 1545 |
| Fl _t Permitted | 0.99 | 1.00 | 0.95 | 1.00 | | | | 0.90 | 1.00 | | 0.87 | 1.00 |
| Satd. Flow (perm) | 1846 | 1514 | 1770 | 3469 | | | | 1670 | 1556 | | 1616 | 1545 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 6 | 314 | 54 | 309 | 309 | 39 | 32 | 69 | 544 | 25 | 36 | 6 |
| RTOR Reduction (vph) | 0 | 0 | 40 | 0 | 15 | 0 | 0 | 0 | 428 | 0 | 0 | 5 |
| Lane Group Flow (vph) | 0 | 320 | 14 | 309 | 333 | 0 | 0 | 101 | 116 | 0 | 61 | 1 |
| Confl. Peds. (#/hr) | 5 | | 15 | | | 5 | 9 | | 6 | | | 14 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Turn Type | Perm | | Perm | Prot | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | 3 | | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 12.8 | 12.8 | 13.2 | 30.0 | | | | 10.3 | 10.3 | | 10.3 | 10.3 |
| Effective Green, g (s) | 12.8 | 12.8 | 13.2 | 30.0 | | | | 10.3 | 10.3 | | 10.3 | 10.3 |
| Actuated g/C Ratio | 0.27 | 0.27 | 0.27 | 0.62 | | | | 0.21 | 0.21 | | 0.21 | 0.21 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 489 | 401 | 484 | 2155 | | | | 356 | 332 | | 345 | 329 |
| v/s Ratio Prot | | | c0.17 | | | | | | | | | |
| v/s Ratio Perm | c0.17 | 0.01 | | 0.10 | | | | 0.06 | c0.07 | | 0.04 | 0.00 |
| v/c Ratio | 0.65 | 0.04 | 0.64 | 0.15 | | | | 0.28 | 0.35 | | 0.18 | 0.00 |
| Uniform Delay, d1 | 15.8 | 13.2 | 15.4 | 3.8 | | | | 15.9 | 16.2 | | 15.5 | 15.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.1 | 0.0 | 2.8 | 0.0 | | | | 0.4 | 0.6 | | 0.2 | 0.0 |
| Delay (s) | 18.9 | 13.2 | 18.2 | 3.9 | | | | 16.4 | 16.8 | | 15.8 | 15.0 |
| Level of Service | B | B | B | A | | | | B | B | | B | B |
| Approach Delay (s) | 18.1 | | | 10.6 | | | | 16.7 | | | 15.7 | |
| Approach LOS | B | | | B | | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 14.7 | | | HCM Level of Service | | | | B | | | | |
| HCM Volume to Capacity ratio | 0.56 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 48.3 | | | Sum of lost time (s) | | | | 12.0 | | | | |
| Intersection Capacity Utilization | 64.7% | | | ICU Level of Service | | | | C | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Macdonald Ave & Harbour Way

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|-------|------|-------|----------------------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↔ | ↔ | ↔ |
| Volume (vph) | 26 | 180 | 33 | 73 | 236 | 120 | 64 | 326 | 128 | 112 | 283 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.92 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.92 | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 1.00 | 0.85 | | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.99 | |
| Satd. Flow (prot) | 1770 | 1863 | 1450 | 1770 | 1712 | | 1770 | 1863 | 1450 | | 3455 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.99 | |
| Satd. Flow (perm) | 1770 | 1863 | 1450 | 1770 | 1712 | | 1770 | 1863 | 1450 | | 3455 | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | | 0.93 | 0.93 | 0.93 | | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | | 114% | 114% | 114% | | 114% | 114% |
| Adj. Flow (vph) | 32 | 221 | 40 | 89 | 289 | 147 | 78 | 400 | 157 | 137 | 347 | 21 |
| RTOR Reduction (vph) | 0 | 0 | 32 | 0 | 23 | 0 | 0 | 0 | 117 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 32 | 221 | 8 | 89 | 413 | 0 | 78 | 400 | 40 | 0 | 501 | 0 |
| Confl. Peds. (#/hr) | | | 56 | | | 34 | 12 | | 52 | | | 38 |
| Confl. Bikes (#/hr) | | | | | | 1 | | | 7 | | | 3 |
| Turn Type | Prot | | Perm | Prot | | | Split | | Perm | Split | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | | | | 4 | | | | | 2 | | | |
| Actuated Green, G (s) | 1.4 | 14.7 | 14.7 | 7.4 | 20.7 | | 17.8 | 17.8 | 17.8 | | 14.2 | |
| Effective Green, g (s) | 1.4 | 14.7 | 14.7 | 7.4 | 20.7 | | 17.8 | 17.8 | 17.8 | | 14.2 | |
| Actuated g/C Ratio | 0.02 | 0.21 | 0.21 | 0.11 | 0.30 | | 0.25 | 0.25 | 0.25 | | 0.20 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 35 | 391 | 304 | 187 | 506 | | 449 | 473 | 368 | | 700 | |
| v/s Ratio Prot | 0.02 | c0.12 | | 0.05 | c0.24 | | 0.04 | c0.21 | | | c0.15 | |
| v/s Ratio Perm | | | | 0.01 | | | | | 0.03 | | | |
| v/c Ratio | 0.91 | 0.57 | 0.03 | 0.48 | 0.82 | | 0.17 | 0.85 | 0.11 | | 0.72 | |
| Uniform Delay, d1 | 34.3 | 24.8 | 22.0 | 29.5 | 22.9 | | 20.4 | 24.8 | 20.1 | | 26.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 116.7 | 1.9 | 0.0 | 1.9 | 9.8 | | 0.2 | 13.1 | 0.1 | | 3.5 | |
| Delay (s) | 151.0 | 26.7 | 22.1 | 31.4 | 32.7 | | 20.6 | 37.9 | 20.2 | | 29.6 | |
| Level of Service | F | C | C | C | C | | C | D | C | | C | |
| Approach Delay (s) | | 39.6 | | | 32.5 | | | 31.4 | | | 29.6 | |
| Approach LOS | | D | | | C | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 32.5 | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | | 0.81 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.1 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 73.1% | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Macdonald Ave & 22nd St SB

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 372 | 88 | 115 | 426 | 0 | 0 | 0 | 0 | 98 | 883 | 85 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | | 0.95 | |
| Fr _t | | 0.97 | | | 1.00 | | | | | | 0.99 | |
| Flt Protected | | 1.00 | | | 0.99 | | | | | | 1.00 | |
| Satd. Flow (prot) | | 3438 | | | 3502 | | | | | | 3481 | |
| Flt Permitted | | 1.00 | | | 0.72 | | | | | | 1.00 | |
| Satd. Flow (perm) | | 3438 | | | 2533 | | | | | | 3481 | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 0 | 433 | 102 | 134 | 496 | 0 | 0 | 0 | 0 | 114 | 1027 | 99 |
| RTOR Reduction (vph) | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 |
| Lane Group Flow (vph) | 0 | 497 | 0 | 0 | 630 | 0 | 0 | 0 | 0 | 0 | 1226 | 0 |
| Turn Type | | | | | Perm | | | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | | | | 6 | |
| Permitted Phases | | | | | 8 | | | | | | 6 | |
| Actuated Green, G (s) | | 14.4 | | | 14.4 | | | | | | 21.1 | |
| Effective Green, g (s) | | 14.4 | | | 14.4 | | | | | | 21.1 | |
| Actuated g/C Ratio | | 0.33 | | | 0.33 | | | | | | 0.49 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | |
| Lane Grp Cap (vph) | | 1138 | | | 839 | | | | | | 1688 | |
| v/s Ratio Prot | | 0.14 | | | | | | | | | | |
| v/s Ratio Perm | | | | | c0.25 | | | | | | 0.35 | |
| v/c Ratio | | 0.44 | | | 0.75 | | | | | | 0.73 | |
| Uniform Delay, d1 | | 11.4 | | | 13.0 | | | | | | 8.9 | |
| Progression Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | |
| Incremental Delay, d2 | | 0.3 | | | 3.8 | | | | | | 2.8 | |
| Delay (s) | | 11.6 | | | 16.8 | | | | | | 11.7 | |
| Level of Service | | B | | | B | | | | | | B | |
| Approach Delay (s) | | 11.6 | | | 16.8 | | | 0.0 | | | 11.7 | |
| Approach LOS | | B | | | B | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 13.0 | | | HCM Level of Service | | | | | B | | |
| HCM Volume to Capacity ratio | | 0.74 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 43.5 | | | Sum of lost time (s) | | | | | 8.0 | | |
| Intersection Capacity Utilization | | 76.3% | | | ICU Level of Service | | | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

1: 23rd St & San Pablo Ave

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|----------------------|------|-------|------|------|------|------|-------|------|
| Lane Configurations | 4 | 7 | 7 | 8 | 4 | 7 | 7 | 10 | 7 | 7 | 10 | 7 |
| Volume (vph) | 362 | 316 | 74 | 8 | 238 | 15 | 82 | 224 | 53 | 25 | 386 | 343 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 | |
| Fr _t | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 0.97 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1814 | 1583 | | 1860 | 1583 | 1770 | 3438 | | 1770 | 3539 | 1583 | |
| Flt Permitted | 0.97 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 1814 | 1583 | | 1860 | 1583 | 1770 | 3438 | | 1770 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 430 | 375 | 88 | 10 | 283 | 18 | 97 | 266 | 63 | 30 | 458 | 407 |
| RTOR Reduction (vph) | 0 | 0 | 54 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 805 | 34 | 0 | 293 | 3 | 97 | 329 | 0 | 30 | 458 | 407 |
| Turn Type | Split | | Perm | Split | | Perm | Prot | | Prot | | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 3 | | | | | 6 | |
| Actuated Green, G (s) | 24.9 | 24.9 | | 15.1 | 15.1 | 4.0 | 20.0 | | 2.0 | 18.0 | 18.0 | |
| Effective Green, g (s) | 24.9 | 24.9 | | 15.1 | 15.1 | 4.0 | 20.0 | | 2.0 | 18.0 | 18.0 | |
| Actuated g/C Ratio | 0.32 | 0.32 | | 0.19 | 0.19 | 0.05 | 0.26 | | 0.03 | 0.23 | 0.23 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 579 | 505 | | 360 | 306 | 91 | 882 | | 45 | 817 | 365 | |
| v/s Ratio Prot | c0.44 | | | c0.16 | | c0.05 | 0.10 | | 0.02 | 0.13 | | |
| v/s Ratio Perm | | | 0.02 | | | 0.00 | | | | | c0.26 | |
| v/c Ratio | 1.39 | 0.07 | | 0.81 | 0.01 | 1.07 | 0.37 | | 0.67 | 0.56 | 1.12 | |
| Uniform Delay, d1 | 26.6 | 18.5 | | 30.1 | 25.4 | 37.0 | 23.8 | | 37.7 | 26.5 | 30.0 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 0.70 | 0.69 | 0.73 | |
| Incremental Delay, d2 | 186.1 | 0.1 | | 13.2 | 0.0 | 113.4 | 1.2 | | 30.5 | 2.7 | 81.2 | |
| Delay (s) | 212.6 | 18.5 | | 43.3 | 25.4 | 150.4 | 25.1 | | 57.0 | 20.9 | 103.0 | |
| Level of Service | F | B | | D | C | F | C | | E | C | F | |
| Approach Delay (s) | 193.5 | | | 42.2 | | | 53.6 | | | 59.5 | | |
| Approach LOS | F | | | D | | | D | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 103.8 | | | HCM Level of Service | | | | | F | | | |
| HCM Volume to Capacity ratio | 1.15 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 78.0 | | | Sum of lost time (s) | | | | | 16.0 | | | |
| Intersection Capacity Utilization | 87.3% | | | ICU Level of Service | | | | | E | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Market Ave & 23rd St

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|--------|-------|------|----------------------|-------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | | ↔ | ↔ | | ↔ | ↔ | ↔ |
| Volume (vph) | 142 | 196 | 93 | 208 | 165 | 27 | 102 | 318 | 95 | 29 | 527 | 75 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | | 0.98 | | | 0.98 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.99 | | | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1824 | | | 1798 | | | 1829 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.68 | | | 0.96 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1824 | | | 1238 | | | 1752 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 176 | 243 | 115 | 258 | 204 | 33 | 126 | 394 | 118 | 36 | 653 | 93 |
| RTOR Reduction (vph) | 0 | 0 | 96 | 0 | 7 | 0 | 0 | 9 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 176 | 243 | 19 | 258 | 230 | 0 | 0 | 629 | 0 | 0 | 777 | 0 |
| Confl. Peds. (#/hr) | | | | 27 | | | | | | | | |
| Turn Type | Split | | Perm | Split | | | Perm | | Perm | | Perm | |
| Protected Phases | 4 | 4 | | 8 | 8 | | | 2 | | 6 | | |
| Permitted Phases | | | 4 | | | | 2 | | 6 | | | |
| Actuated Green, G (s) | 14.6 | 14.6 | 14.6 | 15.2 | 15.2 | | | 46.1 | | | 46.1 | |
| Effective Green, g (s) | 14.6 | 14.6 | 14.6 | 15.2 | 15.2 | | | 46.1 | | | 46.1 | |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | | | 0.52 | | | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 294 | 309 | 263 | 306 | 315 | | | 649 | | | 919 | |
| v/s Ratio Prot | 0.10 | c0.13 | | c0.15 | 0.13 | | | | | | | |
| v/s Ratio Perm | | | 0.01 | | | | c0.51 | | | 0.44 | | |
| v/c Ratio | 0.60 | 0.79 | 0.07 | 0.84 | 0.73 | | | 0.97 | | | 0.85 | |
| Uniform Delay, d1 | 33.9 | 35.2 | 30.9 | 35.2 | 34.4 | | | 20.2 | | | 17.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 3.3 | 12.4 | 0.1 | 18.6 | 8.5 | | | 27.4 | | | 7.2 | |
| Delay (s) | 37.2 | 47.5 | 31.1 | 53.8 | 42.9 | | | 47.6 | | | 25.1 | |
| Level of Service | D | D | C | D | D | | | D | | | C | |
| Approach Delay (s) | | 40.6 | | | 48.6 | | | 47.6 | | | 25.1 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 39.1 | | | HCM Level of Service | | | D | | | |
| HCM Volume to Capacity ratio | | | 0.91 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 87.9 | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 108.5% | | | ICU Level of Service | | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Rheem Ave & 23rd St

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↔ | ↔ | ↔ | ↔ | ↔ | ↑ | ↑ | ↓ | ↔ |
| Volume (vph) | 80 | 181 | 128 | 127 | 157 | 35 | 60 | 464 | 138 | 33 | 551 | 43 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.92 | | 0.99 | | | 0.98 | | | 0.99 | |
| Flpb, ped/bikes | 0.98 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.99 | | | 0.97 | | | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1739 | 1863 | 1459 | | 1766 | | | 1763 | | | 1827 | |
| Flt Permitted | 0.54 | 1.00 | 1.00 | | 0.78 | | | 0.90 | | | 0.95 | |
| Satd. Flow (perm) | 996 | 1863 | 1459 | | 1405 | | | 1595 | | | 1745 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 95 | 215 | 152 | 151 | 186 | 42 | 71 | 551 | 164 | 39 | 654 | 51 |
| RTOR Reduction (vph) | 0 | 0 | 52 | 0 | 12 | 0 | 0 | 23 | 0 | 0 | 6 | 0 |
| Lane Group Flow (vph) | 95 | 215 | 100 | 0 | 367 | 0 | 0 | 763 | 0 | 0 | 738 | 0 |
| Confl. Peds. (#/hr) | 29 | | 48 | 14 | | 82 | 34 | | 67 | 53 | | 63 |
| Confl. Bikes (#/hr) | | | 3 | | | 5 | | | 1 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 13.4 | 13.4 | 13.4 | | 13.4 | | | 16.6 | | | 16.6 | |
| Effective Green, g (s) | 13.4 | 13.4 | 13.4 | | 13.4 | | | 16.6 | | | 16.6 | |
| Actuated g/C Ratio | 0.35 | 0.35 | 0.35 | | 0.35 | | | 0.44 | | | 0.44 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 351 | 657 | 514 | | 495 | | | 697 | | | 762 | |
| v/s Ratio Prot | | 0.12 | | | | | | | | | | |
| v/s Ratio Perm | 0.10 | | 0.07 | | c0.26 | | | c0.48 | | | 0.42 | |
| v/c Ratio | 0.27 | 0.33 | 0.19 | | 0.74 | | | 1.10 | | | 0.97 | |
| Uniform Delay, d1 | 8.8 | 9.0 | 8.5 | | 10.8 | | | 10.7 | | | 10.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.3 | 0.2 | | 5.9 | | | 63.1 | | | 25.7 | |
| Delay (s) | 9.2 | 9.3 | 8.7 | | 16.7 | | | 73.8 | | | 36.2 | |
| Level of Service | A | A | A | | B | | | E | | | D | |
| Approach Delay (s) | | 9.1 | | | 16.7 | | | 73.8 | | | 36.2 | |
| Approach LOS | | A | | | B | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 40.2 | | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | 0.94 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 38.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 105.7% | | | ICU Level of Service | | | G | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Barrett Ave & 23rd St NB

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | | | ↑↑ | | | ↑↑ | | | | |
| Volume (vph) | 107 | 395 | 0 | 0 | 447 | 102 | 111 | 461 | 64 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | | | 0.95 | | | | |
| Fr _t | 1.00 | 1.00 | | | 0.97 | | | 0.98 | | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | | | 0.99 | | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3440 | | | 3456 | | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | | | 0.99 | | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3440 | | | 3456 | | | | |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 140 | 518 | 0 | 0 | 586 | 134 | 145 | 604 | 84 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 41 | 0 | 0 | 16 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 140 | 518 | 0 | 0 | 679 | 0 | 0 | 817 | 0 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | | | Perm | | | | |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | | | | | | | | 2 | | | | |
| Actuated Green, G (s) | 4.5 | 22.4 | | | 13.9 | | | 16.4 | | | | |
| Effective Green, g (s) | 4.5 | 22.4 | | | 13.9 | | | 16.4 | | | | |
| Actuated g/C Ratio | 0.10 | 0.48 | | | 0.30 | | | 0.35 | | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | 170 | 1694 | | | 1022 | | | 1211 | | | | |
| v/s Ratio Prot | c0.08 | 0.15 | | | c0.20 | | | | | | | |
| v/s Ratio Perm | | | | | | | | 0.24 | | | | |
| v/c Ratio | 0.82 | 0.31 | | | 0.66 | | | 0.67 | | | | |
| Uniform Delay, d1 | 20.8 | 7.5 | | | 14.4 | | | 12.9 | | | | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | 26.4 | 0.1 | | | 1.6 | | | 3.0 | | | | |
| Delay (s) | 47.2 | 7.6 | | | 16.1 | | | 15.9 | | | | |
| Level of Service | D | A | | | B | | | B | | | | |
| Approach Delay (s) | | 16.0 | | | 16.1 | | | 15.9 | | | 0.0 | |
| Approach LOS | | B | | | B | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 16.0 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.69 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 46.8 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 55.1% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Macdonald Ave & 23rd St NB

5/23/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↑↑ | | | ↑↑ | ↑ | | ↑↑ | ↑ | | | |
| Volume (vph) | 64 | 241 | 0 | 0 | 265 | 59 | 70 | 589 | 148 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 0.95 | | | 0.95 | 1.00 | | 0.95 | 1.00 | | | |
| Fr _t | | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | | |
| Flt Protected | | 0.99 | | | 1.00 | 1.00 | | 0.99 | 1.00 | | | |
| Satd. Flow (prot) | | 3502 | | | 3539 | 1583 | | 3520 | 1583 | | | |
| Flt Permitted | | 0.81 | | | 1.00 | 1.00 | | 0.99 | 1.00 | | | |
| Satd. Flow (perm) | | 2882 | | | 3539 | 1583 | | 3520 | 1583 | | | |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 85 | 319 | 0 | 0 | 351 | 78 | 93 | 781 | 196 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 55 | 0 | 0 | 104 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 404 | 0 | 0 | 351 | 23 | 0 | 874 | 92 | 0 | 0 | 0 |
| Turn Type | Perm | | | | Perm | Perm | | Perm | | | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | 4 | | | | | 8 | 2 | | 2 | | | |
| Actuated Green, G (s) | | 10.3 | | | 10.3 | 10.3 | | 16.1 | 16.1 | | | |
| Effective Green, g (s) | | 10.3 | | | 10.3 | 10.3 | | 16.1 | 16.1 | | | |
| Actuated g/C Ratio | | 0.30 | | | 0.30 | 0.30 | | 0.47 | 0.47 | | | |
| Clearance Time (s) | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 863 | | | 1060 | 474 | | 1647 | 741 | | | |
| v/s Ratio Prot | | | | | 0.10 | | | | | | | |
| v/s Ratio Perm | | c0.14 | | | | 0.01 | | 0.25 | 0.06 | | | |
| v/c Ratio | | 0.47 | | | 0.33 | 0.05 | | 0.53 | 0.12 | | | |
| Uniform Delay, d1 | | 9.8 | | | 9.4 | 8.6 | | 6.5 | 5.2 | | | |
| Progression Factor | | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.4 | | | 0.2 | 0.0 | | 1.2 | 0.3 | | | |
| Delay (s) | | 10.2 | | | 9.6 | 8.6 | | 7.7 | 5.5 | | | |
| Level of Service | | B | | | A | A | | A | A | | | |
| Approach Delay (s) | | 10.2 | | | 9.4 | | | 7.3 | | 0.0 | | |
| Approach LOS | | B | | | A | | | A | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 8.4 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.51 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 34.4 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 48.9% | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: 23rd St & San Pablo Ave

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|------|-------|-------|------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 695 | 174 | 103 | 31 | 201 | 33 | 113 | 607 | 47 | 36 | 378 | 592 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 0.99 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.96 | 1.00 | | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1791 | 1583 | | 1850 | 1583 | 1770 | 3501 | 3501 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.96 | 1.00 | | 0.99 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1791 | 1583 | | 1850 | 1583 | 1770 | 3501 | 3501 | | 1770 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 808 | 202 | 120 | 36 | 234 | 38 | 131 | 706 | 55 | 42 | 440 | 689 |
| RTOR Reduction (vph) | 0 | 0 | 37 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1010 | 83 | 0 | 270 | 18 | 131 | 761 | 0 | 42 | 440 | 689 |
| Turn Type | Split | | Perm | Split | | Perm | Prot | | Prot | | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 3 | | | | | 6 | |
| Actuated Green, G (s) | 35.0 | 35.0 | | 17.0 | 17.0 | 9.0 | 54.4 | | | 5.6 | 51.0 | 51.0 |
| Effective Green, g (s) | 35.0 | 35.0 | | 17.0 | 17.0 | 9.0 | 54.4 | | | 5.6 | 51.0 | 51.0 |
| Actuated g/C Ratio | 0.27 | 0.27 | | 0.13 | 0.13 | 0.07 | 0.42 | | | 0.04 | 0.40 | 0.40 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 490 | 433 | | 246 | 210 | 124 | 1488 | | | 77 | 1410 | 631 |
| v/s Ratio Prot | c0.56 | | | c0.15 | | c0.07 | c0.22 | | | 0.02 | 0.12 | |
| v/s Ratio Perm | | 0.05 | | | | 0.01 | | | | | c0.44 | |
| v/c Ratio | 2.06 | 0.19 | | 1.10 | 0.09 | 1.06 | 0.51 | | | 0.55 | 0.31 | 1.09 |
| Uniform Delay, d1 | 46.5 | 35.7 | | 55.5 | 48.7 | 59.5 | 27.0 | | | 60.0 | 26.4 | 38.5 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.20 | 0.74 | 0.76 |
| Incremental Delay, d2 | 484.6 | 0.2 | | 85.9 | 0.2 | 96.7 | 1.3 | | | 7.6 | 0.1 | 63.3 |
| Delay (s) | 531.1 | 35.9 | | 141.4 | 48.9 | 156.2 | 28.3 | | | 79.5 | 19.6 | 92.5 |
| Level of Service | F | D | | F | D | F | C | | | E | B | F |
| Approach Delay (s) | 478.5 | | | 130.0 | | | 47.1 | | | | 64.6 | |
| Approach LOS | F | | | F | | | D | | | | E | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|------|
| HCM Average Control Delay | 199.5 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.43 | | |
| Actuated Cycle Length (s) | 128.0 | Sum of lost time (s) | 20.0 |
| Intersection Capacity Utilization | 105.8% | ICU Level of Service | G |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

2: Market Ave & 23rd St

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|-------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ |
| Volume (vph) | 89 | 201 | 121 | 159 | 168 | 23 | 94 | 632 | 80 | 17 | 328 | 62 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | | 0.99 | | | 0.98 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.99 | | | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1830 | | | 1827 | | | 1821 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.88 | | | 0.95 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1830 | | | 1624 | | | 1735 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 106 | 239 | 144 | 189 | 200 | 27 | 112 | 750 | 95 | 20 | 390 | 74 |
| RTOR Reduction (vph) | 0 | 0 | 120 | 0 | 6 | 0 | 0 | 4 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 106 | 239 | 24 | 189 | 221 | 0 | 0 | 953 | 0 | 0 | 477 | 0 |
| Confl. Peds. (#/hr) | | | | | 27 | | | | | | | |
| Turn Type | Split | | Perm | Split | | | Perm | | Perm | | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 14.5 | 14.5 | 14.5 | 14.1 | 14.1 | | | 46.1 | | | 46.1 | |
| Effective Green, g (s) | 14.5 | 14.5 | 14.5 | 14.1 | 14.1 | | | 46.1 | | | 46.1 | |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 | 0.16 | 0.16 | | | 0.53 | | | 0.53 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 296 | 312 | 265 | 288 | 298 | | | 864 | | | 923 | |
| v/s Ratio Prot | 0.06 | c0.13 | | 0.11 | c0.12 | | | | | | | |
| v/s Ratio Perm | | | 0.02 | | | | | c0.59 | | | 0.27 | |
| v/c Ratio | 0.36 | 0.77 | 0.09 | 0.66 | 0.74 | | | 1.10 | | | 0.52 | |
| Uniform Delay, d1 | 32.0 | 34.5 | 30.5 | 34.0 | 34.6 | | | 20.3 | | | 13.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.7 | 10.7 | 0.1 | 5.3 | 9.6 | | | 62.7 | | | 0.5 | |
| Delay (s) | 32.7 | 45.2 | 30.7 | 39.3 | 44.1 | | | 83.0 | | | 13.6 | |
| Level of Service | C | D | C | D | D | | | F | | | B | |
| Approach Delay (s) | | 38.2 | | | 42.0 | | | 83.0 | | | 13.6 | |
| Approach LOS | | D | | | D | | | F | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|------|
| HCM Average Control Delay | 52.1 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.97 | | |
| Actuated Cycle Length (s) | 86.7 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 109.9% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

3: Rheem Ave & 23rd St

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 44 | 143 | 91 | 116 | 155 | 64 | 55 | 909 | 178 | 31 | 624 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.91 | | 0.98 | | | 0.99 | | | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.97 | | | 0.98 | | | 0.99 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1751 | 1863 | 1436 | | 1739 | | | 1791 | | | 1838 | |
| Fl _t Permitted | 0.47 | 1.00 | 1.00 | | 0.82 | | | 0.94 | | | 0.93 | |
| Satd. Flow (perm) | 861 | 1863 | 1436 | | 1448 | | | 1690 | | | 1705 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 53 | 172 | 109 | 139 | 186 | 77 | 66 | 1091 | 214 | 37 | 749 | 41 |
| RTOR Reduction (vph) | 0 | 0 | 75 | 0 | 17 | 0 | 0 | 13 | 0 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 53 | 172 | 34 | 0 | 385 | 0 | 0 | 1358 | 0 | 0 | 823 | 0 |
| Confl. Peds. (#/hr) | 16 | | 38 | 9 | | 55 | 29 | | 48 | 39 | | 45 |
| Confl. Bikes (#/hr) | | | 14 | | | 9 | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 15.2 | 15.2 | 15.2 | | 15.2 | | | 26.1 | | | 26.1 | |
| Effective Green, g (s) | 15.2 | 15.2 | 15.2 | | 15.2 | | | 26.1 | | | 26.1 | |
| Actuated g/C Ratio | 0.31 | 0.31 | 0.31 | | 0.31 | | | 0.53 | | | 0.53 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 265 | 574 | 443 | | 446 | | | 895 | | | 903 | |
| v/s Ratio Prot | | 0.09 | | | | | | | | | | |
| v/s Ratio Perm | 0.06 | | 0.02 | | c0.27 | | | c0.80 | | | 0.48 | |
| v/c Ratio | 0.20 | 0.30 | 0.08 | | 0.86 | | | 1.52 | | | 0.91 | |
| Uniform Delay, d1 | 12.6 | 13.0 | 12.1 | | 16.1 | | | 11.6 | | | 10.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.4 | 0.3 | 0.1 | | 15.7 | | | 238.5 | | | 15.0 | |
| Delay (s) | 12.9 | 13.3 | 12.1 | | 31.7 | | | 250.1 | | | 25.5 | |
| Level of Service | B | B | B | | C | | | F | | | C | |
| Approach Delay (s) | | 12.9 | | | 31.7 | | | 250.1 | | | 25.5 | |
| Approach LOS | | B | | | C | | | F | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 129.9 | | | HCM Level of Service | | | F | | | | |
| HCM Volume to Capacity ratio | | 1.28 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 49.3 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 134.2% | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Barrett Ave & 23rd St NB

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | | 0 | 0 | ↑↑ | | ↑↑ | | 0 | 0 | 0 |
| Volume (vph) | 153 | 767 | 0 | 0 | 424 | 66 | 107 | 1131 | 94 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | | | 0.95 | | | | |
| Fr _t | 1.00 | 1.00 | | | 0.98 | | | 0.99 | | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3468 | | | 3488 | | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3468 | | | 3488 | | | | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 188 | 940 | 0 | 0 | 520 | 81 | 131 | 1386 | 115 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 9 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 188 | 940 | 0 | 0 | 580 | 0 | 0 | 1623 | 0 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | | | Perm | | | | |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | | | | | | | | 2 | | | | |
| Actuated Green, G (s) | 6.1 | 24.4 | | | 14.3 | | | 26.0 | | | | |
| Effective Green, g (s) | 6.1 | 24.4 | | | 14.3 | | | 26.0 | | | | |
| Actuated g/C Ratio | 0.10 | 0.42 | | | 0.24 | | | 0.45 | | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | 185 | 1479 | | | 849 | | | 1553 | | | | |
| v/s Ratio Prot | c0.11 | c0.27 | | | 0.17 | | | | | | | |
| v/s Ratio Perm | | | | | | | | 0.47 | | | | |
| v/c Ratio | 1.02 | 0.64 | | | 0.68 | | | 1.05 | | | | |
| Uniform Delay, d1 | 26.2 | 13.5 | | | 20.0 | | | 16.2 | | | | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | 70.5 | 0.9 | | | 2.3 | | | 35.6 | | | | |
| Delay (s) | 96.6 | 14.4 | | | 22.3 | | | 51.8 | | | | |
| Level of Service | F | B | | | C | | | D | | | | |
| Approach Delay (s) | | 28.1 | | | 22.3 | | | 51.8 | | 0.0 | | |
| Approach LOS | | C | | | C | | | D | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 38.6 | | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | 0.94 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 58.4 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 78.0% | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Macdonald Ave & 23rd St NB

5/25/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 99 | 355 | 0 | 0 | 384 | 147 | 150 | 1156 | 163 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | | | | | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | | | |
| Fr _t | | | | | 1.00 | 1.00 | 0.85 | 1.00 | 0.85 | | | |
| Flt Protected | | | | | 0.99 | 1.00 | 1.00 | 0.99 | 1.00 | | | |
| Satd. Flow (prot) | | | | | 3501 | 3539 | 1583 | 3519 | 1583 | | | |
| Flt Permitted | | | | | 0.77 | 1.00 | 1.00 | 0.99 | 1.00 | | | |
| Satd. Flow (perm) | | | | | 2738 | 3539 | 1583 | 3519 | 1583 | | | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 118 | 422 | 0 | 0 | 456 | 175 | 178 | 1373 | 194 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 109 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 540 | 0 | 0 | 456 | 168 | 0 | 1551 | 85 | 0 | 0 | 0 |
| Turn Type | Perm | | | | | Perm | Perm | | Perm | | | |
| Protected Phases | | 4 | | | | 8 | | | 2 | | | |
| Permitted Phases | 4 | | | | | | 8 | 2 | | 2 | | |
| Actuated Green, G (s) | | 12.5 | | | | 12.5 | 12.5 | | 16.1 | 16.1 | | |
| Effective Green, g (s) | | 12.5 | | | | 12.5 | 12.5 | | 16.1 | 16.1 | | |
| Actuated g/C Ratio | | 0.34 | | | | 0.34 | 0.34 | | 0.44 | 0.44 | | |
| Clearance Time (s) | | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 | | |
| Vehicle Extension (s) | | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 935 | | | | 1209 | 541 | | 1548 | 696 | | | |
| v/s Ratio Prot | | | | | 0.13 | | | | | | | |
| v/s Ratio Perm | c0.20 | | | | | 0.11 | | 0.44 | 0.05 | | | |
| v/c Ratio | 0.58 | | | | 0.38 | 0.31 | | 1.00 | 0.12 | | | |
| Uniform Delay, d1 | 9.9 | | | | 9.1 | 8.9 | | 10.2 | 6.1 | | | |
| Progression Factor | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 0.9 | | | | 0.2 | 0.3 | | 23.3 | 0.4 | | | |
| Delay (s) | 10.8 | | | | 9.3 | 9.2 | | 33.6 | 6.4 | | | |
| Level of Service | B | | | | A | A | | C | A | | | |
| Approach Delay (s) | 10.8 | | | | 9.3 | | | 30.6 | | 0.0 | | |
| Approach LOS | B | | | | A | | | C | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 22.3 | | | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | 0.82 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 36.6 | | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | 78.0% | | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: 23rd St & San Pablo Ave

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|------|-------|------|------|------|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 302 | 316 | 74 | 8 | 238 | 15 | 82 | 224 | 53 | 25 | 386 | 243 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 | |
| Fr _t | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 0.98 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1818 | 1583 | | 1860 | 1583 | 1770 | 3438 | | 1770 | 3539 | 1583 | |
| Flt Permitted | 0.98 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 1818 | 1583 | | 1860 | 1583 | 1770 | 3438 | | 1770 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 359 | 375 | 88 | 10 | 283 | 18 | 97 | 266 | 63 | 30 | 458 | 289 |
| RTOR Reduction (vph) | 0 | 0 | 49 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 734 | 39 | 0 | 293 | 6 | 97 | 329 | 0 | 30 | 458 | 289 |
| Turn Type | Split | | Perm | Split | | Perm | Prot | | Prot | | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 3 | | | | | 6 | |
| Actuated Green, G (s) | 39.0 | 39.0 | | 16.0 | 16.0 | 7.6 | 22.0 | | 3.0 | 17.4 | 17.4 | |
| Effective Green, g (s) | 39.0 | 39.0 | | 16.0 | 16.0 | 7.6 | 22.0 | | 3.0 | 17.4 | 17.4 | |
| Actuated g/C Ratio | 0.41 | 0.41 | | 0.17 | 0.17 | 0.08 | 0.23 | | 0.03 | 0.18 | 0.18 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 739 | 643 | | 310 | 264 | 140 | 788 | | 55 | 641 | 287 | |
| v/s Ratio Prot | c0.40 | | | c0.16 | | c0.05 | 0.10 | | 0.02 | 0.13 | | |
| v/s Ratio Perm | | 0.02 | | | 0.00 | | | | | | c0.18 | |
| v/c Ratio | 0.99 | 0.06 | | 0.95 | 0.02 | 0.69 | 0.42 | | 0.55 | 0.71 | 1.01 | |
| Uniform Delay, d1 | 28.4 | 17.3 | | 39.6 | 33.5 | 43.1 | 31.5 | | 45.8 | 37.0 | 39.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 0.70 | 0.68 | 0.70 | |
| Incremental Delay, d2 | 31.2 | 0.0 | | 36.5 | 0.0 | 13.8 | 1.6 | | 10.4 | 6.5 | 54.2 | |
| Delay (s) | 59.6 | 17.4 | | 76.1 | 33.5 | 56.9 | 33.2 | | 42.2 | 31.6 | 81.7 | |
| Level of Service | E | B | | E | C | E | C | | D | C | F | |
| Approach Delay (s) | 55.1 | | | 73.6 | | 38.6 | | | | 50.7 | | |
| Approach LOS | E | | | E | | D | | | | D | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 53.1 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.96 | | |
| Actuated Cycle Length (s) | 96.0 | Sum of lost time (s) | 16.0 |
| Intersection Capacity Utilization | 83.5% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |

c = Critical Lane Group

HCM Signalized Intersection Capacity Analysis

2: Market Ave & 23rd St

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|-------|-------|------|-------|------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 142 | 196 | 93 | 208 | 165 | 27 | 102 | 258 | 95 | 29 | 427 | 75 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | | 0.97 | | | 0.98 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.99 | | | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1824 | | | 1790 | | | 1822 | |
| Fl _t Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.69 | | | 0.95 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1824 | | | 1248 | | | 1743 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 176 | 243 | 115 | 258 | 204 | 33 | 126 | 320 | 118 | 36 | 529 | 93 |
| RTOR Reduction (vph) | 0 | 0 | 94 | 0 | 7 | 0 | 0 | 12 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 176 | 243 | 21 | 258 | 230 | 0 | 0 | 552 | 0 | 0 | 651 | 0 |
| Confl. Peds. (#/hr) | | | | 27 | | | | | | | | |
| Turn Type | Split | | Perm | Split | | | Perm | | Perm | | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 13.9 | 13.9 | 13.9 | 14.4 | 14.4 | | | 36.2 | | | 36.2 | |
| Effective Green, g (s) | 13.9 | 13.9 | 13.9 | 14.4 | 14.4 | | | 36.2 | | | 36.2 | |
| Actuated g/C Ratio | 0.18 | 0.18 | 0.18 | 0.19 | 0.19 | | | 0.47 | | | 0.47 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 322 | 339 | 288 | 333 | 343 | | | 591 | | | 825 | |
| v/s Ratio Prot | 0.10 | c0.13 | | c0.15 | 0.13 | | | | | | | |
| v/s Ratio Perm | | | 0.01 | | | | c0.44 | | | 0.37 | | |
| v/c Ratio | 0.55 | 0.72 | 0.07 | 0.77 | 0.67 | | | 0.93 | | | 0.79 | |
| Uniform Delay, d1 | 28.4 | 29.4 | 26.0 | 29.5 | 28.8 | | | 19.0 | | | 16.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 1.9 | 7.1 | 0.1 | 10.7 | 4.9 | | | 22.1 | | | 5.1 | |
| Delay (s) | 30.3 | 36.5 | 26.1 | 40.2 | 33.7 | | | 41.1 | | | 22.0 | |
| Level of Service | C | D | C | D | C | | | D | | | C | |
| Approach Delay (s) | | 32.2 | | | 37.1 | | | 41.1 | | | 22.0 | |
| Approach LOS | | C | | | D | | | D | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 32.5 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.85 | | |
| Actuated Cycle Length (s) | 76.5 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 99.4% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

3: Rheem Ave & 23rd St

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | | ↑ | | | ↑ | | | ↑ | |
| Volume (vph) | 80 | 181 | 128 | 127 | 157 | 35 | 60 | 404 | 138 | 33 | 451 | 43 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.90 | | 0.98 | | | 0.97 | | | 0.99 | |
| Flpb, ped/bikes | 0.98 | 1.00 | 1.00 | | 0.99 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.99 | | | 0.97 | | | 0.99 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1734 | 1863 | 1432 | | 1758 | | | 1743 | | | 1817 | |
| Fl _t Permitted | 0.50 | 1.00 | 1.00 | | 0.74 | | | 0.90 | | | 0.94 | |
| Satd. Flow (perm) | 913 | 1863 | 1432 | | 1336 | | | 1582 | | | 1711 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 95 | 215 | 152 | 151 | 186 | 42 | 71 | 480 | 164 | 39 | 536 | 51 |
| RTOR Reduction (vph) | 0 | 0 | 105 | 0 | 9 | 0 | 0 | 21 | 0 | 0 | 6 | 0 |
| Lane Group Flow (vph) | 95 | 215 | 47 | 0 | 370 | 0 | 0 | 694 | 0 | 0 | 620 | 0 |
| Confl. Peds. (#/hr) | 29 | | 48 | 14 | | 82 | 34 | | 67 | 53 | | 63 |
| Confl. Bikes (#/hr) | | | 3 | | | 5 | | | 1 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 15.3 | 15.3 | 15.3 | | 15.3 | | | 26.0 | | | 26.0 | |
| Effective Green, g (s) | 15.3 | 15.3 | 15.3 | | 15.3 | | | 26.0 | | | 26.0 | |
| Actuated g/C Ratio | 0.31 | 0.31 | 0.31 | | 0.31 | | | 0.53 | | | 0.53 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 283 | 578 | 444 | | 415 | | | 834 | | | 902 | |
| v/s Ratio Prot | | 0.12 | | | | | | | | | | |
| v/s Ratio Perm | 0.10 | | 0.03 | | c0.28 | | | c0.44 | | | 0.36 | |
| v/c Ratio | 0.34 | 0.37 | 0.11 | | 0.89 | | | 0.83 | | | 0.69 | |
| Uniform Delay, d1 | 13.1 | 13.3 | 12.1 | | 16.2 | | | 9.8 | | | 8.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.7 | 0.4 | 0.1 | | 20.7 | | | 9.5 | | | 4.3 | |
| Delay (s) | 13.8 | 13.7 | 12.2 | | 36.9 | | | 19.3 | | | 12.9 | |
| Level of Service | B | B | B | | D | | | B | | | B | |
| Approach Delay (s) | | 13.2 | | | 36.9 | | | 19.3 | | | 12.9 | |
| Approach LOS | | B | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 19.2 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.85 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 49.3 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 100.0% | | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Barrett Ave & 23rd St NB

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | | | ↑↑ | | | ↑↑ | | | | |
| Volume (vph) | 107 | 395 | 0 | 0 | 447 | 102 | 111 | 401 | 64 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | | | 0.95 | | | | |
| Fr _t | 1.00 | 1.00 | | | 0.97 | | | 0.98 | | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | | | 0.99 | | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3440 | | | 3447 | | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | | | 0.99 | | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3440 | | | 3447 | | | | |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 140 | 518 | 0 | 0 | 586 | 134 | 145 | 525 | 84 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 41 | 0 | 0 | 18 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 140 | 518 | 0 | 0 | 679 | 0 | 0 | 736 | 0 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | | | Perm | | | | |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | | | | | | | | 2 | | | | |
| Actuated Green, G (s) | 4.5 | 22.4 | | | 13.9 | | | 16.4 | | | | |
| Effective Green, g (s) | 4.5 | 22.4 | | | 13.9 | | | 16.4 | | | | |
| Actuated g/C Ratio | 0.10 | 0.48 | | | 0.30 | | | 0.35 | | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | 170 | 1694 | | | 1022 | | | 1208 | | | | |
| v/s Ratio Prot | c0.08 | 0.15 | | | c0.20 | | | | | | | |
| v/s Ratio Perm | | | | | | | | 0.21 | | | | |
| v/c Ratio | 0.82 | 0.31 | | | 0.66 | | | 0.61 | | | | |
| Uniform Delay, d1 | 20.8 | 7.5 | | | 14.4 | | | 12.6 | | | | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | 26.4 | 0.1 | | | 1.6 | | | 2.3 | | | | |
| Delay (s) | 47.2 | 7.6 | | | 16.1 | | | 14.8 | | | | |
| Level of Service | D | A | | | B | | | B | | | | |
| Approach Delay (s) | | 16.0 | | | 16.1 | | | 14.8 | | | 0.0 | |
| Approach LOS | | B | | | B | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 15.6 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.66 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 46.8 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 53.2% | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Macdonald Ave & 23rd St NB

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↑↑ | | | ↑↑ | ↑ | | ↑↑ | ↑ | | | |
| Volume (vph) | 64 | 241 | 0 | 0 | 265 | 59 | 130 | 529 | 148 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 0.95 | | | 0.95 | 1.00 | | 0.95 | 1.00 | | | |
| Fr _t | | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | | |
| Flt Protected | | 0.99 | | | 1.00 | 1.00 | | 0.99 | 1.00 | | | |
| Satd. Flow (prot) | | 3502 | | | 3539 | 1583 | | 3505 | 1583 | | | |
| Flt Permitted | | 0.81 | | | 1.00 | 1.00 | | 0.99 | 1.00 | | | |
| Satd. Flow (perm) | | 2882 | | | 3539 | 1583 | | 3505 | 1583 | | | |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 85 | 319 | 0 | 0 | 351 | 78 | 172 | 701 | 196 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 55 | 0 | 0 | 104 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 404 | 0 | 0 | 351 | 23 | 0 | 873 | 92 | 0 | 0 | 0 |
| Turn Type | Perm | | | | Perm | Perm | | Perm | | | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | 4 | | | | | 8 | 2 | | 2 | | | |
| Actuated Green, G (s) | 10.3 | | | | 10.3 | 10.3 | | 16.1 | 16.1 | | | |
| Effective Green, g (s) | 10.3 | | | | 10.3 | 10.3 | | 16.1 | 16.1 | | | |
| Actuated g/C Ratio | 0.30 | | | | 0.30 | 0.30 | | 0.47 | 0.47 | | | |
| Clearance Time (s) | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | 863 | | | | 1060 | 474 | | 1640 | 741 | | | |
| v/s Ratio Prot | | | | | 0.10 | | | | | | | |
| v/s Ratio Perm | c0.14 | | | | | 0.01 | | 0.25 | 0.06 | | | |
| v/c Ratio | 0.47 | | | | 0.33 | 0.05 | | 0.53 | 0.12 | | | |
| Uniform Delay, d1 | 9.8 | | | | 9.4 | 8.6 | | 6.5 | 5.2 | | | |
| Progression Factor | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 0.4 | | | | 0.2 | 0.0 | | 1.2 | 0.3 | | | |
| Delay (s) | 10.2 | | | | 9.6 | 8.6 | | 7.7 | 5.5 | | | |
| Level of Service | B | | | | A | A | | A | A | | | |
| Approach Delay (s) | 10.2 | | | | 9.4 | | | 7.3 | | 0.0 | | |
| Approach LOS | B | | | | A | | | A | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 8.4 | | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | 0.51 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 34.4 | | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | 49.0% | | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Rumrill Blvd & San Pablo Ave

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|------|------|------|-------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↗ ↖ | | ↖ ↗ | | | ↑ ↗ | ↑ ↘ | ↗ ↖ | ↑ ↗ | ↑ ↘ |
| Volume (vph) | 325 | 25 | 6 | 28 | 28 | 24 | 0 | 324 | 11 | 33 | 511 | 350 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.97 | | 0.99 | | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | 0.99 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.96 | | | 0.99 | | 1.00 | 1.00 | 0.85 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1534 | | 1734 | | | 3513 | | 1745 | 3539 | 1583 |
| Fl _t Permitted | 0.71 | 1.00 | 1.00 | | 0.91 | | | 1.00 | | 0.49 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1314 | 1863 | 1534 | | 1612 | | | 3513 | | 895 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 403 | 31 | 7 | 35 | 35 | 30 | 0 | 401 | 14 | 41 | 633 | 434 |
| RTOR Reduction (vph) | 0 | 0 | 4 | 0 | 19 | 0 | 0 | 2 | 0 | 0 | 0 | 202 |
| Lane Group Flow (vph) | 403 | 31 | 3 | 0 | 81 | 0 | 0 | 413 | 0 | 41 | 633 | 232 |
| Confl. Peds. (#/hr) | | | 11 | 7 | | 9 | 9 | | 16 | 9 | | |
| Confl. Bikes (#/hr) | | | | | | 1 | | | 1 | | | |
| Turn Type | Perm | | Perm | Perm | | | | | | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | 6 | | 6 |
| Actuated Green, G (s) | 36.6 | 36.6 | 36.6 | | 36.6 | | | 51.4 | | 51.4 | 51.4 | 51.4 |
| Effective Green, g (s) | 36.6 | 36.6 | 36.6 | | 36.6 | | | 51.4 | | 51.4 | 51.4 | 51.4 |
| Actuated g/C Ratio | 0.38 | 0.38 | 0.38 | | 0.38 | | | 0.54 | | 0.54 | 0.54 | 0.54 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 501 | 710 | 585 | | 615 | | | 1881 | | 479 | 1895 | 848 |
| v/s Ratio Prot | | 0.02 | | | | | | 0.12 | | | c0.18 | |
| v/s Ratio Perm | c0.31 | | 0.00 | | 0.05 | | | | | 0.05 | | 0.15 |
| v/c Ratio | 0.80 | 0.04 | 0.00 | | 0.13 | | | 0.22 | | 0.09 | 0.33 | 0.27 |
| Uniform Delay, d1 | 26.5 | 18.7 | 18.4 | | 19.4 | | | 11.7 | | 10.9 | 12.6 | 12.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 0.23 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 9.1 | 0.0 | 0.0 | | 0.1 | | | 0.2 | | 0.4 | 0.5 | 0.8 |
| Delay (s) | 35.6 | 18.7 | 18.4 | | 19.5 | | | 2.9 | | 11.2 | 13.1 | 12.9 |
| Level of Service | D | B | B | | B | | | A | | B | B | B |
| Approach Delay (s) | | 34.1 | | | 19.5 | | | 2.9 | | | 13.0 | |
| Approach LOS | | C | | | B | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 15.8 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.53 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 96.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 53.9% | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Market Ave & Rumrill Blvd

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|----------------------|------|------|------|------|------|-------|-------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | |
| Volume (vph) | 31 | 92 | 32 | 160 | 78 | 64 | 42 | 505 | 145 | 56 | 725 | 42 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.99 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.96 | | 1.00 | 0.93 | | 1.00 | 0.97 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1759 | 1782 | | 1770 | 1720 | | 1770 | 3400 | | 1770 | 3503 | |
| Flt Permitted | 0.62 | 1.00 | | 0.65 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1149 | 1782 | | 1206 | 1720 | | 1770 | 3400 | | 1770 | 3503 | |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 44 | 129 | 45 | 225 | 110 | 90 | 59 | 711 | 204 | 79 | 1020 | 59 |
| RTOR Reduction (vph) | 0 | 23 | 0 | 0 | 55 | 0 | 0 | 48 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 44 | 151 | 0 | 225 | 145 | 0 | 59 | 867 | 0 | 79 | 1071 | 0 |
| Confl. Peds. (#/hr) | 9 | | 6 | | | 11 | | | 5 | 2 | | 12 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Turn Type | Perm | | Perm | | | Prot | | | Prot | | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | | | | | | | |
| Actuated Green, G (s) | 13.3 | 13.3 | | 13.3 | 13.3 | | 2.0 | 20.0 | | 2.0 | 20.0 | |
| Effective Green, g (s) | 13.3 | 13.3 | | 13.3 | 13.3 | | 2.0 | 20.0 | | 2.0 | 20.0 | |
| Actuated g/C Ratio | 0.28 | 0.28 | | 0.28 | 0.28 | | 0.04 | 0.42 | | 0.04 | 0.42 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 323 | 501 | | 339 | 484 | | 75 | 1438 | | 75 | 1481 | |
| v/s Ratio Prot | | 0.08 | | | 0.08 | | 0.03 | 0.26 | | c0.04 | c0.31 | |
| v/s Ratio Perm | 0.04 | | c0.19 | | | | | | | | | |
| v/c Ratio | 0.14 | 0.30 | | 0.66 | 0.30 | | 0.79 | 0.60 | | 1.05 | 0.72 | |
| Uniform Delay, d1 | 12.7 | 13.4 | | 15.0 | 13.3 | | 22.4 | 10.6 | | 22.6 | 11.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.2 | 0.3 | | 4.8 | 0.4 | | 40.6 | 0.7 | | 119.3 | 1.8 | |
| Delay (s) | 12.9 | 13.7 | | 19.9 | 13.7 | | 63.0 | 11.3 | | 142.0 | 13.1 | |
| Level of Service | B | B | | B | B | | E | B | | F | B | |
| Approach Delay (s) | | 13.5 | | | 17.0 | | | 14.4 | | | 21.9 | |
| Approach LOS | | B | | | B | | | B | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 17.9 | | HCM Level of Service | | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.72 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 47.3 | | Sum of lost time (s) | | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 60.1% | | ICU Level of Service | | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Pennsylvania Ave & Harbour Way-10th St

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 1 | 249 | 45 | 484 | 353 | 24 | 35 | 34 | 281 | 21 | 26 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.94 | 1.00 | 1.00 | | | | 1.00 | 0.97 | | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.99 | | | | 1.00 | 0.85 | | 1.00 | 0.85 |
| Fl _t Protected | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.98 | 1.00 | | 0.98 | 1.00 |
| Satd. Flow (prot) | 1862 | 1493 | 1770 | 3500 | | | | 1812 | 1538 | | 1822 | 1553 |
| Fl _t Permitted | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.82 | 1.00 | | 0.84 | 1.00 |
| Satd. Flow (perm) | 1860 | 1493 | 1770 | 3500 | | | | 1524 | 1538 | | 1571 | 1553 |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 1 | 330 | 60 | 642 | 468 | 32 | 46 | 45 | 372 | 28 | 34 | 5 |
| RTOR Reduction (vph) | 0 | 0 | 46 | 0 | 6 | 0 | 0 | 0 | 315 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 0 | 331 | 14 | 642 | 494 | 0 | 0 | 91 | 57 | 0 | 62 | 1 |
| Confl. Peds. (#/hr) | 1 | | 18 | 13 | | 1 | 5 | | 13 | | | 6 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | |
| Turn Type | Perm | | Perm | | Prot | | | Perm | | Perm | | Perm |
| Protected Phases | | 4 | | 3 | | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 15.1 | 15.1 | 27.1 | 46.2 | | | | 9.9 | 9.9 | | 9.9 | 9.9 |
| Effective Green, g (s) | 15.1 | 15.1 | 27.1 | 46.2 | | | | 9.9 | 9.9 | | 9.9 | 9.9 |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.42 | 0.72 | | | | 0.15 | 0.15 | | 0.15 | 0.15 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 438 | 352 | 748 | 2523 | | | | 235 | 238 | | 243 | 240 |
| v/s Ratio Prot | | | c0.36 | | | | | | | | | |
| v/s Ratio Perm | c0.18 | 0.01 | | 0.14 | | | | c0.06 | 0.04 | | 0.04 | 0.00 |
| v/c Ratio | 0.76 | 0.04 | 0.86 | 0.20 | | | | 0.39 | 0.24 | | 0.26 | 0.00 |
| Uniform Delay, d1 | 22.8 | 18.9 | 16.8 | 2.9 | | | | 24.4 | 23.8 | | 23.9 | 22.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 7.3 | 0.0 | 9.6 | 0.0 | | | | 1.1 | 0.5 | | 0.6 | 0.0 |
| Delay (s) | 30.1 | 19.0 | 26.4 | 2.9 | | | | 25.4 | 24.3 | | 24.4 | 22.9 |
| Level of Service | C | B | C | A | | | | C | C | | C | C |
| Approach Delay (s) | 28.4 | | | 16.1 | | | | 24.5 | | | 24.3 | |
| Approach LOS | C | | | B | | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 20.6 | | | | HCM Level of Service | | | | C | | | |
| HCM Volume to Capacity ratio | 0.74 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 64.1 | | | | Sum of lost time (s) | | | | 12.0 | | | |
| Intersection Capacity Utilization | 67.3% | | | | ICU Level of Service | | | | C | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Macdonald Ave & Harbour Way

5/29/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|-------|----------------------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 23 | 149 | 31 | 63 | 161 | 108 | 130 | 256 | 98 | 179 | 327 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.94 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.94 | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 1.00 | 0.85 | | 1.00 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.98 | |
| Satd. Flow (prot) | 1770 | 1863 | 1488 | 1770 | 1710 | | 1770 | 1863 | 1484 | | 3470 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.98 | |
| Satd. Flow (perm) | 1770 | 1863 | 1488 | 1770 | 1710 | | 1770 | 1863 | 1484 | | 3470 | |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 30 | 193 | 40 | 82 | 209 | 140 | 168 | 332 | 127 | 232 | 424 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 31 | 0 | 33 | 0 | 0 | 0 | 97 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 30 | 193 | 9 | 82 | 316 | 0 | 168 | 332 | 30 | 0 | 662 | 0 |
| Confl. Peds. (#/hr) | | | 41 | | | 18 | | | 40 | | | 19 |
| Confl. Bikes (#/hr) | | | | | | 2 | | | 4 | | | 3 |
| Turn Type | Prot | | Perm | Prot | | | Split | | Perm | Split | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | | | | 4 | | | | | | 2 | | |
| Actuated Green, G (s) | 1.4 | 14.3 | 14.3 | 3.7 | 16.6 | | 14.9 | 14.9 | 14.9 | | 15.2 | |
| Effective Green, g (s) | 1.4 | 14.3 | 14.3 | 3.7 | 16.6 | | 14.9 | 14.9 | 14.9 | | 15.2 | |
| Actuated g/C Ratio | 0.02 | 0.22 | 0.22 | 0.06 | 0.26 | | 0.23 | 0.23 | 0.23 | | 0.24 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 39 | 416 | 332 | 102 | 443 | | 411 | 433 | 345 | | 823 | |
| v/s Ratio Prot | 0.02 | 0.10 | | c0.05 | c0.18 | | 0.09 | c0.18 | | | c0.19 | |
| v/s Ratio Perm | | | | 0.01 | | | | | | 0.02 | | |
| v/c Ratio | 0.77 | 0.46 | 0.03 | 0.80 | 0.71 | | 0.41 | 0.77 | 0.09 | | 0.80 | |
| Uniform Delay, d1 | 31.2 | 21.6 | 19.5 | 29.8 | 21.6 | | 20.9 | 23.0 | 19.3 | | 23.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 60.6 | 0.8 | 0.0 | 35.2 | 5.4 | | 0.7 | 7.9 | 0.1 | | 5.8 | |
| Delay (s) | 91.8 | 22.4 | 19.5 | 65.0 | 26.9 | | 21.5 | 30.9 | 19.4 | | 28.8 | |
| Level of Service | F | C | B | E | C | | C | C | B | | C | |
| Approach Delay (s) | | 29.9 | | | 34.2 | | | 26.1 | | | 28.8 | |
| Approach LOS | | C | | | C | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 29.2 | | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | 0.73 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 64.1 | | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | 66.4% | | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Macdonald Ave & 22nd St SB

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 224 | 160 | 142 | 367 | 0 | 0 | 0 | 0 | 125 | 949 | 77 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | | 0.95 | |
| Fr _t | | 0.94 | | | 1.00 | | | | | | 0.99 | |
| Flt Protected | | 1.00 | | | 0.99 | | | | | | 0.99 | |
| Satd. Flow (prot) | | 3318 | | | 3491 | | | | | | 3485 | |
| Flt Permitted | | 1.00 | | | 0.70 | | | | | | 0.99 | |
| Satd. Flow (perm) | | 3318 | | | 2477 | | | | | | 3485 | |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 0 | 272 | 194 | 172 | 445 | 0 | 0 | 0 | 0 | 152 | 1151 | 93 |
| RTOR Reduction (vph) | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 0 | 432 | 0 | 0 | 617 | 0 | 0 | 0 | 0 | 0 | 1386 | 0 |
| Turn Type | | | | | Perm | | | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | | | | 6 | |
| Permitted Phases | | | | | 8 | | | | | | 6 | |
| Actuated Green, G (s) | | 15.6 | | | 15.6 | | | | | | 25.1 | |
| Effective Green, g (s) | | 15.6 | | | 15.6 | | | | | | 25.1 | |
| Actuated g/C Ratio | | 0.32 | | | 0.32 | | | | | | 0.52 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | |
| Lane Grp Cap (vph) | | 1063 | | | 793 | | | | | | 1796 | |
| v/s Ratio Prot | | 0.13 | | | | | | | | | | |
| v/s Ratio Perm | | | | | c0.25 | | | | | | 0.40 | |
| v/c Ratio | | 0.41 | | | 0.78 | | | | | | 0.77 | |
| Uniform Delay, d1 | | 12.9 | | | 15.0 | | | | | | 9.5 | |
| Progression Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | |
| Incremental Delay, d2 | | 0.3 | | | 4.8 | | | | | | 3.3 | |
| Delay (s) | | 13.2 | | | 19.8 | | | | | | 12.8 | |
| Level of Service | | B | | | B | | | | | | B | |
| Approach Delay (s) | | 13.2 | | | 19.8 | | | 0.0 | | | 12.8 | |
| Approach LOS | | B | | | B | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 14.6 | | | HCM Level of Service | | | | | B | | |
| HCM Volume to Capacity ratio | | 0.77 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 48.7 | | | Sum of lost time (s) | | | | | 8.0 | | |
| Intersection Capacity Utilization | | 76.0% | | | ICU Level of Service | | | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

1: 23rd St & San Pablo Ave

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|------|-------|------|------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 565 | 174 | 103 | 31 | 201 | 33 | 113 | 607 | 47 | 36 | 378 | 532 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 | |
| Fr _t | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.96 | 1.00 | | 0.99 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1794 | 1583 | | 1850 | 1583 | 1770 | 3501 | | 1770 | 3539 | 1583 | |
| Flt Permitted | 0.96 | 1.00 | | 0.99 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 1794 | 1583 | | 1850 | 1583 | 1770 | 3501 | | 1770 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 657 | 202 | 120 | 36 | 234 | 38 | 131 | 706 | 55 | 42 | 440 | 619 |
| RTOR Reduction (vph) | 0 | 0 | 46 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 859 | 74 | 0 | 270 | 17 | 131 | 761 | 0 | 42 | 440 | 619 |
| Turn Type | Split | | Perm | Split | | Perm | Prot | | Prot | | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 3 | | | | | 6 | |
| Actuated Green, G (s) | 43.0 | 43.0 | | 16.0 | 16.0 | 7.8 | 39.4 | | 5.6 | 37.2 | 37.2 | |
| Effective Green, g (s) | 43.0 | 43.0 | | 16.0 | 16.0 | 7.8 | 39.4 | | 5.6 | 37.2 | 37.2 | |
| Actuated g/C Ratio | 0.36 | 0.36 | | 0.13 | 0.13 | 0.06 | 0.33 | | 0.05 | 0.31 | 0.31 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 643 | 567 | | 247 | 211 | 115 | 1149 | | 83 | 1097 | 491 | |
| v/s Ratio Prot | c0.48 | | | c0.15 | | c0.07 | 0.22 | | 0.02 | 0.12 | | |
| v/s Ratio Perm | | 0.05 | | | 0.01 | | | | | c0.39 | | |
| v/c Ratio | 1.34 | 0.13 | | 1.09 | 0.08 | 1.14 | 0.66 | | 0.51 | 0.40 | 1.26 | |
| Uniform Delay, d1 | 38.5 | 25.9 | | 52.0 | 45.6 | 56.1 | 34.6 | | 55.8 | 32.6 | 41.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 0.92 | 0.71 | 0.80 | |
| Incremental Delay, d2 | 161.6 | 0.1 | | 84.4 | 0.2 | 126.2 | 3.0 | | 4.7 | 0.2 | 132.8 | |
| Delay (s) | 200.1 | 26.0 | | 136.4 | 45.7 | 182.3 | 37.6 | | 56.0 | 23.6 | 166.1 | |
| Level of Service | F | C | | F | D | F | D | | E | C | F | |
| Approach Delay (s) | 178.7 | | | 125.2 | | | 58.9 | | | 104.9 | | |
| Approach LOS | F | | | F | | | E | | | F | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 116.3 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.21 | | |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 97.6% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

2: Market Ave & 23rd St

5/29/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|----------------------|-------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 89 | 201 | 121 | 159 | 168 | 23 | 94 | 502 | 80 | 17 | 268 | 62 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | | 0.98 | | | 0.98 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.99 | | | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1830 | | | 1820 | | | 1813 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.88 | | | 0.95 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1830 | | | 1621 | | | 1733 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 106 | 239 | 144 | 189 | 200 | 27 | 112 | 596 | 95 | 20 | 318 | 74 |
| RTOR Reduction (vph) | 0 | 0 | 120 | 0 | 6 | 0 | 0 | 5 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 106 | 239 | 24 | 189 | 221 | 0 | 0 | 798 | 0 | 0 | 403 | 0 |
| Confl. Peds. (#/hr) | | | | 27 | | | | | | | | |
| Turn Type | Split | | Perm | Split | | | Perm | | Perm | | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 14.4 | 14.4 | 14.4 | 14.1 | 14.1 | | | 44.3 | | | 44.3 | |
| Effective Green, g (s) | 14.4 | 14.4 | 14.4 | 14.1 | 14.1 | | | 44.3 | | | 44.3 | |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | | | 0.52 | | | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 301 | 316 | 269 | 294 | 304 | | | 847 | | | 905 | |
| v/s Ratio Prot | 0.06 | c0.13 | | 0.11 | c0.12 | | | | | | | |
| v/s Ratio Perm | | | 0.02 | | | | | c0.49 | | | 0.23 | |
| v/c Ratio | 0.35 | 0.76 | 0.09 | 0.64 | 0.73 | | | 0.94 | | | 0.45 | |
| Uniform Delay, d1 | 31.1 | 33.5 | 29.7 | 33.0 | 33.5 | | | 19.0 | | | 12.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.7 | 9.9 | 0.1 | 4.8 | 8.4 | | | 18.3 | | | 0.4 | |
| Delay (s) | 31.8 | 43.4 | 29.8 | 37.8 | 41.9 | | | 37.3 | | | 13.0 | |
| Level of Service | C | D | C | D | D | | | D | | | B | |
| Approach Delay (s) | | 36.9 | | | 40.0 | | | 37.3 | | | 13.0 | |
| Approach LOS | | D | | | D | | | D | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 33.0 | | HCM Level of Service | | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.86 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 84.8 | | Sum of lost time (s) | | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 98.5% | | ICU Level of Service | | | | F | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Rheem Ave & 23rd St

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|--------|------|------|----------------------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | | ↑ | | | ↑ | | | ↑ | |
| Volume (vph) | 44 | 143 | 91 | 116 | 155 | 64 | 55 | 779 | 178 | 31 | 564 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.88 | | 0.97 | | | 0.98 | | | 0.99 | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | | 0.99 | | | 1.00 | | | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | | 0.97 | | | 0.98 | | | 0.99 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | 1749 | 1863 | 1392 | | 1724 | | | 1772 | | | 1832 | |
| Fl _t Permitted | 0.40 | 1.00 | 1.00 | | 0.74 | | | 0.93 | | | 0.91 | |
| Satd. Flow (perm) | 732 | 1863 | 1392 | | 1297 | | | 1654 | | | 1674 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 53 | 172 | 109 | 139 | 186 | 77 | 66 | 935 | 214 | 37 | 677 | 41 |
| RTOR Reduction (vph) | 0 | 0 | 83 | 0 | 12 | 0 | 0 | 11 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 53 | 172 | 26 | 0 | 390 | 0 | 0 | 1204 | 0 | 0 | 752 | 0 |
| Confl. Peds. (#/hr) | 16 | | 38 | 9 | | 55 | 29 | | 48 | 39 | | 45 |
| Confl. Bikes (#/hr) | | | 14 | | | 9 | | | 3 | | | 1 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | | Perm | | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 17.0 | 17.0 | 17.0 | | 17.0 | | | 45.0 | | | 45.0 | |
| Effective Green, g (s) | 17.0 | 17.0 | 17.0 | | 17.0 | | | 45.0 | | | 45.0 | |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | | 0.24 | | | 0.64 | | | 0.64 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 178 | 452 | 338 | | 315 | | | 1063 | | | 1076 | |
| v/s Ratio Prot | | 0.09 | | | | | | | | | | |
| v/s Ratio Perm | 0.07 | | 0.02 | | c0.30 | | | c0.73 | | | 0.45 | |
| v/c Ratio | 0.30 | 0.38 | 0.08 | | 1.24 | | | 1.13 | | | 0.70 | |
| Uniform Delay, d1 | 21.6 | 22.1 | 20.5 | | 26.5 | | | 12.5 | | | 8.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.9 | 0.5 | 0.1 | | 131.2 | | | 71.7 | | | 3.8 | |
| Delay (s) | 22.6 | 22.6 | 20.6 | | 157.7 | | | 84.2 | | | 11.9 | |
| Level of Service | C | C | C | | F | | | F | | | B | |
| Approach Delay (s) | | 21.9 | | | 157.7 | | | 84.2 | | | 11.9 | |
| Approach LOS | | C | | | F | | | F | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 67.3 | | | HCM Level of Service | | | E | | | | |
| HCM Volume to Capacity ratio | | 1.16 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 70.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 125.5% | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Barrett Ave & 23rd St NB

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | | | ↑↑ | | | ↑↑ | | | | |
| Volume (vph) | 153 | 767 | 0 | 0 | 424 | 66 | 107 | 1001 | 94 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | | | 0.95 | | | | |
| Fr _t | 1.00 | 1.00 | | | 0.98 | | | 0.99 | | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3468 | | | 3482 | | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3468 | | | 3482 | | | | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 188 | 940 | 0 | 0 | 520 | 81 | 131 | 1227 | 115 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 9 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 188 | 940 | 0 | 0 | 582 | 0 | 0 | 1464 | 0 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | | | Perm | | | | |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | | |
| Permitted Phases | | | | | | | | 2 | | | | |
| Actuated Green, G (s) | 8.0 | 26.7 | | | 14.7 | | | 29.0 | | | | |
| Effective Green, g (s) | 8.0 | 26.7 | | | 14.7 | | | 29.0 | | | | |
| Actuated g/C Ratio | 0.13 | 0.42 | | | 0.23 | | | 0.46 | | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | | | 4.0 | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | | | 3.0 | | | | |
| Lane Grp Cap (vph) | 222 | 1483 | | | 800 | | | 1585 | | | | |
| v/s Ratio Prot | c0.11 | 0.27 | | | c0.17 | | | | | | | |
| v/s Ratio Perm | | | | | | | | 0.42 | | | | |
| v/c Ratio | 0.85 | 0.63 | | | 0.73 | | | 0.92 | | | | |
| Uniform Delay, d1 | 27.3 | 14.6 | | | 22.6 | | | 16.3 | | | | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | | | 1.00 | | | | |
| Incremental Delay, d2 | 24.6 | 0.9 | | | 3.3 | | | 10.5 | | | | |
| Delay (s) | 51.8 | 15.5 | | | 26.0 | | | 26.8 | | | | |
| Level of Service | D | B | | | C | | | C | | | | |
| Approach Delay (s) | | 21.6 | | | 26.0 | | | 26.8 | | | 0.0 | |
| Approach LOS | | C | | | C | | | C | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 24.8 | | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.86 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 63.7 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 73.9% | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Macdonald Ave & 23rd St NB

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 99 | 355 | 0 | 0 | 384 | 147 | 280 | 1026 | 163 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | | | | | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | | | |
| Fr _t | | | | | 1.00 | 1.00 | 0.85 | 1.00 | 0.85 | | | |
| Flt Protected | | | | | 0.99 | 1.00 | 1.00 | 0.99 | 1.00 | | | |
| Satd. Flow (prot) | | | | | 3501 | 3539 | 1583 | 3502 | 1583 | | | |
| Flt Permitted | | | | | 0.71 | 1.00 | 1.00 | 0.99 | 1.00 | | | |
| Satd. Flow (perm) | | | | | 2519 | 3539 | 1583 | 3502 | 1583 | | | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 118 | 422 | 0 | 0 | 456 | 175 | 332 | 1218 | 194 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 44 | 0 | 0 | 68 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 540 | 0 | 0 | 456 | 131 | 0 | 1550 | 126 | 0 | 0 | 0 |
| Turn Type | Perm | | | | | Perm | Perm | | Perm | | | |
| Protected Phases | | 4 | | | | 8 | | | 2 | | | |
| Permitted Phases | 4 | | | | | | 8 | 2 | | 2 | | |
| Actuated Green, G (s) | | 14.7 | | | | 14.7 | 14.7 | | 31.0 | 31.0 | | |
| Effective Green, g (s) | | 14.7 | | | | 14.7 | 14.7 | | 31.0 | 31.0 | | |
| Actuated g/C Ratio | | 0.27 | | | | 0.27 | 0.27 | | 0.58 | 0.58 | | |
| Clearance Time (s) | | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 | | |
| Vehicle Extension (s) | | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 690 | | | | 969 | 433 | | 2022 | 914 | | | |
| v/s Ratio Prot | | | | | 0.13 | | | | | | | |
| v/s Ratio Perm | c0.21 | | | | | 0.08 | | 0.44 | 0.08 | | | |
| v/c Ratio | 0.78 | | | | 0.47 | 0.30 | | 0.77 | 0.14 | | | |
| Uniform Delay, d1 | 18.0 | | | | 16.3 | 15.4 | | 8.6 | 5.2 | | | |
| Progression Factor | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 5.8 | | | | 0.4 | 0.4 | | 2.8 | 0.3 | | | |
| Delay (s) | 23.8 | | | | 16.6 | 15.8 | | 11.5 | 5.5 | | | |
| Level of Service | C | | | | B | B | | B | A | | | |
| Approach Delay (s) | 23.8 | | | | 16.4 | | | 10.8 | | 0.0 | | |
| Approach LOS | C | | | | B | | | B | | A | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 14.4 | | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | 0.77 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 53.7 | | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | 78.2% | | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Rumrill Blvd & San Pablo Ave

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|----------------------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↙ | | ↗ ↖ | | | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↗ | ↑ ↘ |
| Volume (vph) | 511 | 16 | 27 | 31 | 24 | 25 | 0 | 799 | 21 | 24 | 446 | 277 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | 1.00 | | | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.94 | | 0.99 | | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | | 0.99 | | | 1.00 | | 1.00 | 1.00 | 1.00 |
| Fr | 1.00 | 1.00 | 0.85 | | 0.96 | | | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.98 | | | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 1863 | 1483 | | 1707 | | | 3515 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.71 | 1.00 | 1.00 | | 0.91 | | | 1.00 | | 0.13 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1320 | 1863 | 1483 | | 1576 | | | 3515 | | 247 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 620 | 19 | 33 | 38 | 29 | 30 | 0 | 969 | 25 | 29 | 541 | 336 |
| RTOR Reduction (vph) | 0 | 0 | 15 | 0 | 11 | 0 | 0 | 1 | 0 | 0 | 0 | 203 |
| Lane Group Flow (vph) | 620 | 19 | 18 | 0 | 86 | 0 | 0 | 993 | 0 | 29 | 541 | 133 |
| Confl. Peds. (#/hr) | | | 23 | 12 | | 15 | 11 | | 27 | 15 | | |
| Confl. Bikes (#/hr) | | | 2 | | | 5 | | | 3 | | | |
| Turn Type | Perm | | Perm | Perm | | | | | | Perm | | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | | | | 6 | | 6 |
| Actuated Green, G (s) | 64.4 | 64.4 | 64.4 | | 64.4 | | | 47.6 | | 47.6 | 47.6 | 47.6 |
| Effective Green, g (s) | 64.4 | 64.4 | 64.4 | | 64.4 | | | 47.6 | | 47.6 | 47.6 | 47.6 |
| Actuated g/C Ratio | 0.54 | 0.54 | 0.54 | | 0.54 | | | 0.40 | | 0.40 | 0.40 | 0.40 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | | | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | | | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 708 | 1000 | 796 | | 846 | | | 1394 | | 98 | 1404 | 628 |
| v/s Ratio Prot | | 0.01 | | | | | | c0.28 | | | 0.15 | |
| v/s Ratio Perm | c0.47 | | 0.01 | 0.05 | | | | | | 0.12 | | 0.08 |
| v/c Ratio | 0.88 | 0.02 | 0.02 | 0.10 | | | | 0.71 | | 0.30 | 0.39 | 0.21 |
| Uniform Delay, d1 | 24.3 | 13.0 | 13.0 | 13.6 | | | | 30.4 | | 24.7 | 25.8 | 23.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | | | 0.45 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 11.7 | 0.0 | 0.0 | 0.1 | | | | 1.0 | | 7.5 | 0.8 | 0.8 |
| Delay (s) | 36.0 | 13.0 | 13.0 | 13.7 | | | | 14.7 | | 32.3 | 26.6 | 24.6 |
| Level of Service | D | B | B | B | | | | B | | C | C | C |
| Approach Delay (s) | | 34.2 | | 13.7 | | | | 14.7 | | | 26.0 | |
| Approach LOS | | C | | B | | | | B | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 23.4 | | HCM Level of Service | | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.81 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 120.0 | | Sum of lost time (s) | | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 71.6% | | ICU Level of Service | | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Market Ave & Rumrill Blvd

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|----------------------|------|------|------|-------|------|-------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | |
| Volume (vph) | 76 | 115 | 51 | 136 | 108 | 71 | 75 | 770 | 224 | 71 | 458 | 56 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.95 | | 1.00 | 0.94 | | 1.00 | 0.97 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1761 | 1757 | | 1770 | 1734 | | 1770 | 3387 | | 1770 | 3463 | |
| Flt Permitted | 0.56 | 1.00 | | 0.58 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1033 | 1757 | | 1089 | 1734 | | 1770 | 3387 | | 1770 | 3463 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 90 | 137 | 61 | 162 | 128 | 84 | 89 | 914 | 266 | 84 | 544 | 66 |
| RTOR Reduction (vph) | 0 | 27 | 0 | 0 | 41 | 0 | 0 | 44 | 0 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 90 | 171 | 0 | 162 | 171 | 0 | 89 | 1136 | 0 | 84 | 594 | 0 |
| Confl. Peds. (#/hr) | 7 | | 18 | | | 13 | | | 13 | 6 | | 18 |
| Confl. Bikes (#/hr) | | | 7 | | | 1 | | | 2 | | | 2 |
| Turn Type | Perm | | Perm | | | Prot | | | Prot | | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | | | | | | | |
| Actuated Green, G (s) | 12.4 | 12.4 | | 12.4 | 12.4 | | 6.9 | 24.5 | | 3.6 | 21.2 | |
| Effective Green, g (s) | 12.4 | 12.4 | | 12.4 | 12.4 | | 6.9 | 24.5 | | 3.6 | 21.2 | |
| Actuated g/C Ratio | 0.24 | 0.24 | | 0.24 | 0.24 | | 0.13 | 0.47 | | 0.07 | 0.40 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 244 | 415 | | 257 | 410 | | 233 | 1581 | | 121 | 1398 | |
| v/s Ratio Prot | | 0.10 | | | 0.10 | | 0.05 | c0.34 | | c0.05 | 0.17 | |
| v/s Ratio Perm | 0.09 | | c0.15 | | | | | | | | | |
| v/c Ratio | 0.37 | 0.41 | | 0.63 | 0.42 | | 0.38 | 0.72 | | 0.69 | 0.42 | |
| Uniform Delay, d1 | 16.8 | 17.0 | | 18.0 | 17.0 | | 20.9 | 11.2 | | 23.9 | 11.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.9 | 0.7 | | 5.0 | 0.7 | | 1.0 | 1.6 | | 15.9 | 0.2 | |
| Delay (s) | 17.7 | 17.6 | | 23.0 | 17.7 | | 21.9 | 12.8 | | 39.8 | 11.5 | |
| Level of Service | B | B | | C | B | | C | B | | D | B | |
| Approach Delay (s) | | 17.7 | | | 20.0 | | | 13.5 | | | 14.9 | |
| Approach LOS | | B | | | B | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 15.2 | | HCM Level of Service | | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.69 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 52.5 | | Sum of lost time (s) | | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 71.2% | | ICU Level of Service | | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Pennsylvania Ave & Harbour Way-10th St

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|----------------------|------|------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 5 | 256 | 44 | 312 | 252 | 32 | 26 | 56 | 574 | 20 | 29 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.95 | 1.00 | 1.00 | | | | 1.00 | 0.98 | 1.00 | 0.97 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.98 | | | | 1.00 | 0.85 | 1.00 | 0.85 | |
| Fl _t Protected | 1.00 | 1.00 | 0.95 | 1.00 | | | | 0.98 | 1.00 | 0.98 | 1.00 | |
| Satd. Flow (prot) | 1861 | 1512 | 1770 | 3469 | | | | 1829 | 1555 | 1825 | 1543 | |
| Fl _t Permitted | 0.99 | 1.00 | 0.95 | 1.00 | | | | 0.90 | 1.00 | 0.87 | 1.00 | |
| Satd. Flow (perm) | 1846 | 1512 | 1770 | 3469 | | | | 1678 | 1555 | 1629 | 1543 | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 6 | 314 | 54 | 382 | 309 | 39 | 32 | 69 | 704 | 25 | 36 | 6 |
| RTOR Reduction (vph) | 0 | 0 | 40 | 0 | 15 | 0 | 0 | 0 | 498 | 0 | 0 | 5 |
| Lane Group Flow (vph) | 0 | 320 | 14 | 382 | 333 | 0 | 0 | 101 | 206 | 0 | 61 | 1 |
| Confl. Peds. (#/hr) | 5 | | 15 | | | 5 | 9 | | 6 | | | 14 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Turn Type | Perm | | Perm | Prot | | | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 4 | | 3 | | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | | 8 | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 13.2 | 13.2 | 14.6 | 31.8 | | | | 11.8 | 11.8 | | 11.8 | 11.8 |
| Effective Green, g (s) | 13.2 | 13.2 | 14.6 | 31.8 | | | | 11.8 | 11.8 | | 11.8 | 11.8 |
| Actuated g/C Ratio | 0.26 | 0.26 | 0.28 | 0.62 | | | | 0.23 | 0.23 | | 0.23 | 0.23 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | | | | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | | | | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 472 | 387 | 501 | 2138 | | | | 384 | 356 | | 373 | 353 |
| v/s Ratio Prot | | | c0.22 | | | | | | | | | |
| v/s Ratio Perm | c0.17 | 0.01 | | 0.10 | | | | 0.06 | c0.13 | | 0.04 | 0.00 |
| v/c Ratio | 0.68 | 0.04 | 0.76 | 0.16 | | | | 0.26 | 0.58 | | 0.16 | 0.00 |
| Uniform Delay, d1 | 17.3 | 14.4 | 16.9 | 4.2 | | | | 16.3 | 17.7 | | 15.9 | 15.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.8 | 0.0 | 6.8 | 0.0 | | | | 0.4 | 2.3 | | 0.2 | 0.0 |
| Delay (s) | 21.1 | 14.5 | 23.7 | 4.2 | | | | 16.7 | 20.0 | | 16.2 | 15.4 |
| Level of Service | C | B | C | A | | | | B | B | | B | B |
| Approach Delay (s) | 20.2 | | | 14.4 | | | | 19.5 | | | 16.1 | |
| Approach LOS | C | | | B | | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | 17.7 | | HCM Level of Service | | | | | B | | | | |
| HCM Volume to Capacity ratio | 0.68 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 51.6 | | Sum of lost time (s) | | | | | 12.0 | | | | |
| Intersection Capacity Utilization | 73.9% | | ICU Level of Service | | | | | D | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Macdonald Ave & Harbour Way

5/29/2012

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|------|-------|----------------------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 26 | 180 | 33 | 73 | 236 | 250 | 64 | 326 | 128 | 172 | 283 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.90 | 1.00 | 0.94 | | 1.00 | 1.00 | 0.90 | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 | | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.98 | |
| Satd. Flow (prot) | 1770 | 1863 | 1423 | 1770 | 1621 | | 1770 | 1863 | 1425 | | 3441 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | | 0.98 | |
| Satd. Flow (perm) | 1770 | 1863 | 1423 | 1770 | 1621 | | 1770 | 1863 | 1425 | | 3441 | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | | 0.93 | 0.93 | 0.93 | | 0.93 | 0.93 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | | 114% | 114% | 114% | | 114% | 114% |
| Adj. Flow (vph) | 32 | 221 | 40 | 89 | 289 | 306 | 78 | 400 | 157 | 211 | 347 | 21 |
| RTOR Reduction (vph) | 0 | 0 | 31 | 0 | 42 | 0 | 0 | 0 | 119 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 32 | 221 | 9 | 89 | 553 | 0 | 78 | 400 | 38 | 0 | 576 | 0 |
| Confl. Peds. (#/hr) | | | 56 | | | 34 | 12 | | 52 | | | 38 |
| Confl. Bikes (#/hr) | | | | | | 1 | | | 7 | | | 3 |
| Turn Type | Prot | | Perm | Prot | | | Split | | Perm | Split | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 2 | 2 | | 6 | 6 | |
| Permitted Phases | | | | 4 | | | | | | 2 | | |
| Actuated Green, G (s) | 2.3 | 20.3 | 20.3 | 13.2 | 31.2 | | 21.2 | 21.2 | 21.2 | | 16.0 | |
| Effective Green, g (s) | 2.3 | 20.3 | 20.3 | 13.2 | 31.2 | | 21.2 | 21.2 | 21.2 | | 16.0 | |
| Actuated g/C Ratio | 0.03 | 0.23 | 0.23 | 0.15 | 0.36 | | 0.24 | 0.24 | 0.24 | | 0.18 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | 47 | 436 | 333 | 269 | 583 | | 433 | 456 | 348 | | 635 | |
| v/s Ratio Prot | 0.02 | c0.12 | | 0.05 | c0.34 | | 0.04 | c0.21 | | | c0.17 | |
| v/s Ratio Perm | | | | 0.01 | | | | | | 0.03 | | |
| v/c Ratio | 0.68 | 0.51 | 0.03 | 0.33 | 0.95 | | 0.18 | 0.88 | 0.11 | | 0.91 | |
| Uniform Delay, d1 | 41.8 | 28.9 | 25.6 | 32.8 | 27.0 | | 25.9 | 31.5 | 25.4 | | 34.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 33.6 | 0.9 | 0.0 | 0.7 | 24.9 | | 0.2 | 17.1 | 0.1 | | 16.6 | |
| Delay (s) | 75.5 | 29.8 | 25.6 | 33.5 | 51.9 | | 26.1 | 48.6 | 25.6 | | 51.2 | |
| Level of Service | E | C | C | C | D | | C | D | C | | D | |
| Approach Delay (s) | | | | | 49.5 | | | 40.1 | | | 51.2 | |
| Approach LOS | | | C | | D | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 45.2 | | | HCM Level of Service | | | D | | | |
| HCM Volume to Capacity ratio | | | 0.91 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 86.7 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 84.7% | | | ICU Level of Service | | | E | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Macdonald Ave & 22nd St SB

5/29/2012



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 0 | 372 | 148 | 115 | 556 | 0 | 0 | 0 | 0 | 98 | 823 | 85 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | | 4.0 | | | | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | | | | | 0.95 | |
| Fr _t | | | | | 0.96 | | | | | | 0.99 | |
| Flt Protected | | | | | 1.00 | | | | | | 1.00 | |
| Satd. Flow (prot) | | | | | 3388 | | | | | | 3477 | |
| Flt Permitted | | | | | 1.00 | | | | | | 1.00 | |
| Satd. Flow (perm) | | | | | 3388 | | | | | | 3477 | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor (vph) | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% | 114% |
| Adj. Flow (vph) | 0 | 433 | 172 | 134 | 647 | 0 | 0 | 0 | 0 | 114 | 957 | 99 |
| RTOR Reduction (vph) | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 |
| Lane Group Flow (vph) | 0 | 578 | 0 | 0 | 781 | 0 | 0 | 0 | 0 | 0 | 1153 | 0 |
| Turn Type | | | | | Perm | | | | | Perm | | |
| Protected Phases | | | | 4 | | 8 | | | | | 6 | |
| Permitted Phases | | | | | 8 | | | | | | 6 | |
| Actuated Green, G (s) | | 14.9 | | | 14.9 | | | | | | 16.0 | |
| Effective Green, g (s) | | 14.9 | | | 14.9 | | | | | | 16.0 | |
| Actuated g/C Ratio | | 0.38 | | | 0.38 | | | | | | 0.41 | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | |
| Lane Grp Cap (vph) | | 1298 | | | 1020 | | | | | | 1430 | |
| v/s Ratio Prot | | 0.17 | | | | | | | | | | |
| v/s Ratio Perm | | | | | c0.29 | | | | | | 0.33 | |
| v/c Ratio | | 0.45 | | | 0.77 | | | | | | 0.81 | |
| Uniform Delay, d1 | | 8.9 | | | 10.5 | | | | | | 10.1 | |
| Progression Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | |
| Incremental Delay, d2 | | 0.2 | | | 3.5 | | | | | | 5.0 | |
| Delay (s) | | 9.2 | | | 14.0 | | | | | | 15.0 | |
| Level of Service | | A | | | B | | | | | | B | |
| Approach Delay (s) | | 9.2 | | | 14.0 | | | 0.0 | | | 15.0 | |
| Approach LOS | | A | | | B | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 13.3 | | | HCM Level of Service | | | | | B | | |
| HCM Volume to Capacity ratio | | 0.79 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 38.9 | | | Sum of lost time (s) | | | | | 8.0 | | |
| Intersection Capacity Utilization | | 80.7% | | | ICU Level of Service | | | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

APPENDIX N

Secondary Effects of Growth

Summary of Secondary Effects of Growth

Table N-1 summarizes the secondary effects of growth in the area served by the West of Hills Northern Pipelines Project. The information presented in Table N-1 is derived from the following environmental documents:

- City of Albany: *Albany General Plan Update and Revision Program Draft Environmental Impact Report and Final Environmental Impact Report: Response to Comments*, State Clearinghouse # 89022809, September 1992 (City of Albany, 1992)
- City of Berkeley: *City of Berkeley Draft General Plan Final Environmental Impact Report*, State Clearinghouse # 2000102107, June 2001 (City of Berkeley, 2001)
- City of El Cerrito: *City of El Cerrito: Draft Environmental Impact Report for the City of El Cerrito General Plan Update*, State Clearinghouse #99022058 (City of El Cerrito, 1999)
- City of Hercules: *City of Hercules General Plan Land Use and Circulation Elements Update and Redevelopment Plan Amendments Environmental Impact Report* (City of Hercules, 1995)
- City of Pinole: *City of Pinole General Plan Update Draft and Final Environmental Impact Report* (City of Pinole, 2010)
- City of Richmond: *Richmond General Plan Update Final Environmental Impact Report* (City of Richmond, 2011)
- City of San Pablo: *San Pablo General Plan 2030 Draft and Final Environmental Impact Report* (City of San Pablo, 2011)
- Contra Costa County: *Findings Related to Certification of the Environmental Impact Report for the General Plan and Adoption of the General Plan* (Contra Costa County, 1991), and Notice of Determination, Negative Declaration prepared for Reconsolidation of the Contra Costa County General Plan (Contra Costa County, 2005)

**TABLE N-1
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA**

| Impact / Mitigation | 2010 Census Population | City of Albany ^a | City of Berkeley ^b | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | City of San Rafael ^h | Contra Costa County ⁱ |
|--|------------------------|-----------------------------|-------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|---------------------------------|----------------------------------|
| AESTHETICS | | | | | | | | | | |
| Impacts | | | | | | | | | | |
| <ul style="list-style-type: none"> • Alteration of visual setting or degradation and/or obstruction of existing views • Conflict with adjoining development relative to height, mass and scale • Introduction of new sources of light and glare • Impacts on scenic corridors | | | | | | | | | | |
| Mitigation Measures | | | | | | | | | | |
| <ul style="list-style-type: none"> • Conduct site-specific environmental review of sports field lighting projects. • Implement identified general plan community design policies to mitigate impacts on neighborhood character and community design. • Retain or replace, to the extent feasible, site features having aesthetic significance. • Retain or replace vegetation and trees that screen residential development, while retaining important view corridors. • Retain or replace vegetation and trees on proposed hiking/biking trail. • Implement identified measures to preserve view corridors, site buildings to minimize obstruction of sensitive viewpoints, and preserve identified views to the extent feasible during evaluation of site-specific proposals. • Require developers to restore natural contours and vegetation at project sites and preserve various natural features of positive scenic value. • Screen parking areas; use hooded lights where needed for nighttime lighting; encourage use of regular windows instead of glass walls or massive reflective windows in research and development and office projects. • Shield street lighting and direct it downward, restrict use of high level outdoor lighting (especially on hillside ridges), and incorporate screening landscaping along roads and near residences to reduce spill light from vehicles and buildings. • Conduct design review of projects containing extensive reflective glass or metal on building surfaces. | | | | | | | | | | |

AESTHETICS (cont.)

PS= Potentially significant impact S = Significant mitigable impact U = Significant and unavoidable impact

X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkley ^a | City of Ceres ^a | City of Elkhorn ^a | City of Herkules ^a | City of Madison ^a | City of San Richmonde ^a | City of Stanislaus ^a | County of Contra Costa ^a |
|--|-----------------------------|------------------------------|----------------------------|------------------------------|-------------------------------|------------------------------|------------------------------------|---------------------------------|-------------------------------------|
| Mitigation Measures (cont.) | | | | | | | | | |
| • Implement identified general plan policies to protect resources of particular scenic value. | | | | | | | | | X |
| • Continue implementation of Measure C to centralize and contain urban development and preserve open space and protect areas of high scenic value within areas to be urbanized. | | | | | | | | | X |
| • Identify scenic ridgelines, discourage hillside and ridgeline development, and, to the extent development is allowed, minimize the visual impact of such development. | | | | | | | | | X |
| • Implement measures to exclude development from some scenic shoreline areas and promulgate and enforce guidelines for development that maintains visual quality along scenic waterways. | | | | | | | | | X |
| • Conduct a visual analysis of proposed scenic routes to identify views of significant visual and cultural value. | | | | | | | | | X |
| AGRICULTURAL RESOURCES | | | | | | | | | |
| Impacts | | | | | | | | | |
| • Conversion of agricultural land and open space to urban use | | | | | | | | | U |
| Mitigation Measures | | | | | | | | | |
| • Implement identified measures to promote continued agricultural production, discourage conversion of agricultural land, and provide mechanisms for insuring that urban development occurs in areas designated by the general plan for urban development. | | | | | | | | | X |
| AIR QUALITY | | | | | | | | | |
| Impacts | | | | | | | | | |
| • Conflict with or obstruction of the implementation of an applicable air quality attainment plan. | | U | | U | U | U | U | U | |
| • Inconsistency with region's congestion management program | | | | | | PS | | | |
| • Result in an increase in vehicle miles traveled (VMT) at a rate that exceeds the rate of population increase. | | | | | | | | U | |
| • Generation of short term air pollutant emissions from construction activities and/or equipment | PS | S | PS | S | PS | S | S | | |

PS= Potentially significant impact

S = Significant mitigable impact

U = Significant and unavoidable impact

X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | Contra Costa County ^{h,i,j} |
|---|-----------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|--------------------------------------|
| AIR QUALITY (cont.) | | | | | | | |
| Impacts (cont.) | | | | | | | |
| • Increased operational emissions that contribute to an existing or projected air quality violation | | U | U | U | U | U | U |
| • Increases in air emissions and degradation of air quality | | | U | U | U | | U |
| • Exposure of sensitive land uses to toxic air contaminants and fine particulate matter | | | | U | | | |
| • Inconsistency with air district significance criteria for odors and toxic air contaminants | S | | | | | | |
| • Exposure of substantial numbers of people to new odor sources and exposure of new residents to existing odor sources | | | | PS | | | |
| • Cumulative increase in criteria pollutant emissions, degradation of regional air quality, and/or conflict with air quality plan | | U | U | U | U | U | |
| Mitigation Measures | | | | | | | |
| • Promote use of public transportation and encourage use of alternative modes of travel (to single-passenger vehicles) including implementing improvements to bicycle and pedestrian routes and cooperation between all modes of transportation. | | | | | X | | X |
| • Continue implementation of normal City permit and review procedures. | | X | | | | | |
| • Implement identified general plan policies addressing public transit, pedestrian and bicycle use and circulation, and air quality. | X | | | | | | |
| • Implement identified general plan policies and programs. | | X | | | | | X |
| • Implement dust abatement program for construction and demolition activities. | | X | | | | | |
| • Require BAAQMD best management practices for all construction projects. | | | X | | | X | X |
| • Implement measures to reduce emissions from construction equipment and vehicles. | | | X | | | | |
| • Prepare a general plan air quality element that includes: the City's air quality goals, measures to mitigate impacts from mobile and stationary sources, and BAAQMD recommendations incorporated into general plan policies; coordinate with BAAQMD in planning future growth and implementing regional transportation plans and trip reduction measures. | | | X | | | | |

PS = Potentially significant impact

S = Significant mitigable impact

U = Significant and unavoidable impact

X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

DS-P

S = Significant mitigable impact

|| = Significant and unavoidable impact

X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkeley ^b | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | City of Sausalito ^{h,i} | Contra Costa County ^j |
|---|-----------------------------|-------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|----------------------------------|----------------------------------|
| BIOLOGICAL RESOURCES (cont.) | | | | | | | | | |
| Mitigation Measures | | | | | | | | | |
| • Locate projects along riparian corridors outside specified buffer zones and implement measures to protect sensitive riparian areas. | | | | | X | X | | | |
| • Require project-specific surveys as specified to determine on-site resources and appropriate site-specific mitigation measures. | | | | | X | X | | | X |
| • Plant native species for revegetation and landscaping purposes. | | | | | X | | | | |
| • Implement specified general plan policies and programs to protect biological resources and habitats. | | | X | X | | | | | |
| • If needed, provide, in consultation with the U.S. Army Corps of Engineers, flood control area wide enough to establish native vegetation and provide wildlife habitat. | | | | | X | | | | |
| • Require appropriate facility design and mitigation measures to prevent degradation of sensitive areas from polluted runoff. | | | | | X | | | | |
| • Locate new development in existing developed or graded areas where practicable. Work with resource agencies to determine adequate buffer to protect tidal habitat in designing bay access trail links; limit and if possible avoid public access and paths within the buffer area; encourage bicyclists to stay on bike paths; require developers to provide signage and fencing and to enforce leash laws near sensitive habitats. | | | | | X | | | | |
| • Provide open space and habitat linkages within and between properties; limit public access to wildlife habitat; and locate any trails to avoid disturbing wildlife nesting/denning areas. | | | | | X | | | | |
| • Implement identified measures to mitigate effects of development on significant ecological Resources areas. | | | | | | | | | X |
| CULTURAL RESOURCES | | | | | | | | | |
| Impacts | | | | | | | | | |
| • Disturbance of historical resource(s) | | | PS | S | | U | | U | U |
| • Disturbance of archaeological/buried cultural resource(s) | | | PS | S | | S | | U | U |
| • Potential disturbance of cultural resources and human remains | | | | | | PS | | | |
| • Disturbance of paleontological resource(s) | | | | | | PS | PS | | |
| • Cumulative impacts on cultural and paleontological resources | | | | | S ^k | U | | | |

PS= Potentially significant impact S = Significant mitigable impact U = Significant and unavoidable impact X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkeley ^b | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | City of San Rafael ^{h,i} | Contra Costa County ^j |
|---|-----------------------------|-------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|-----------------------------------|----------------------------------|
| CULTURAL RESOURCES (cont.) | | | | | | | | | |
| Mitigation Measures | | | | | | | | | |
| <ul style="list-style-type: none"> Conduct project-specific review and implement identified mitigation consistent with general plan cultural resource policies and applicable ordinances. Establish standard conditions of approval and criteria for determining which projects are likely to have archaeological resources and warrant additional site-specific evaluation as part of project development. Include in the general plan update the specified studies to be undertaken for areas that have not been surveyed and/or are sensitive for cultural resources and procedures to be followed in the event that cultural resources, paleontological resources, or human remains are encountered during development activities. Implement CEQA Guidelines Section 15064.5 provisions for the accidental discovery of historic or archeological resources. Implement measures to evaluate and protect historic, archaeological, and paleontological resources including previously unknown cultural resources. Implement specified general plan policies concerning historical and/or archaeological resources. | | | | | | | | | |
| GEOLOGY AND SOILS | | | | | | | | | |
| Impacts | | | | | | | | | |
| <ul style="list-style-type: none"> Exposure of more people or structures to hazards from strong seismic ground shaking, ground failure, ground rupture, liquefaction, and/or differential settlement Exposure to hazards associated with expansive soils Soil compaction and/or increased potential for soil erosion Exposure to landslide and/or mudslide hazards | | | | | | | | | |
| Mitigation Measures | | | | | | | | | |
| <ul style="list-style-type: none"> Implement general plan policies and programs to mitigate potential geologic and seismic hazards. Maintain and improve an earthquake disaster preparedness plan | | | | | | | | | |

PS = Potentially significant impact

S = Significant mitigable impact

U = Significant and unavoidable impact

X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of El Cerrito ^c | City of Hercules ^b | City of Pinole | City of Richmond ^d | City of San Pablo ^e | County, City of San Francisco ^f |
|---|-----------------------------|---------------------------------|-------------------------------|----------------|-------------------------------|--------------------------------|--|
| GEOLOGY AND SOILS (cont.) | | | | | | | |
| Mitigation Measures (cont.) | | | | | | | |
| • Design and construct critical facilities to resist effects of maximum credible earthquake; strengthen existing critical facilities and specified residential buildings to meet this standard. | X | | | | | | |
| • Design and construct critical facilities consistent with State of California requirements and the recommendations. Evaluate the feasibility of alternative sites for critical facilities. | | | X | | | | X |
| • Require site specific geotechnical evaluation for new development. | X | | | X | | | X |
| • Design buried utility infrastructure in vicinity of debris landfill to accommodate expected ground surface displacement. | X | | | | | | |
| • Design all cut-and-fill slopes, engineered fills, roads, structural foundations and underground utilities to accommodate estimated settlement without failure. | | | | | | | X |
| • Implement measures to minimize erosion and provide appropriate drainage. | | | | X | | | X |
| • Include slope repair contingency plans for existing landslide areas. | | | | | | | X |
| GREENHOUSE GAS EMISSIONS & CLIMATE CHANGE | | | | | | | |
| Impacts | | | | | | | |
| • Construction and operational generation of GHGs. | | | | | U | | |
| Mitigation Measures | | | | | | | |
| • Implement the BAAQMD best management practices for greenhouse gas emissions | | | | | X | | |
| • Implement general plan policies to reduce GHG emissions | | | | | X | | |
| • Require large developments and retrofits to exceed Title 24 standards as specified. | | | | | X | | |
| HAZARDS AND HAZARDOUS MATERIALS | | | | | | | |
| Impacts | | | | | | | |
| • Accidental release of or exposure to hazardous materials | | S | S | | | | U |
| • Increased number of residents exposed to possible disasters/hazardous substances | S | | | | | | U |
| • Cumulative impacts associated with waste cleanup and disposal capacity from generation of hazardous waste by new industries | | | | U | | | |
| • Increased risks associated with increased transportation of hazards substances. | | | | | | | U |

PS= Potentially significant impact

S = Significant mitigable impact

U = Significant and unavoidable impact

X = Mitigation measure identified in Environmental Impact Report

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkeley ^a | City of El Cerrito ^a | City of Hercules ^a | City of Pinole ^a | City of Richmond ^a | City of San Pablo ^a | City of San Rafael ^a | Contra Costa County ^a |
|--|----------------------------------|--|--|-------------------------------|-----------------------------|-------------------------------|--------------------------------|---------------------------------|----------------------------------|
| HAZARDS AND HAZARDOUS MATERIALS (cont.) | | | | | | | | | |
| Mitigation Measures | | | | | | | | | |
| <ul style="list-style-type: none"> Review and revise emergency preparedness plan, conduct preparedness drills, and initiate emergency preparedness program for residents and employees. Implement identified general plan hazards policies addressing hazardous soils, hazardous waste management, and hazardous materials usage and storage. Implement measures requiring strict regulation of hazardous waste storage and require industries to have up to date safety and design features in storage areas. Implement identified policies to encourage waste minimization. Implement identified measures requiring site assessment, notification, remediation, and follow-up investigation, prior to development of or near a hazardous material site. Prohibit residential development in identified cancer risk areas. Prohibit urban and suburban development in areas subject to safety hazards from oil and gas wells. Prepare a risk management and prevention plan for acutely hazardous chemicals handling at wastewater treatment plant if required by and to the specifications of the county health services department. Implement identified measures addressing access to pipelines and safety procedures for construction on parcels that include or are bordered by a pipeline, and consider notification requirements for sponsors of residential developments near pipelines. Require that the transport of hazardous materials provides greater separation from the general public and that the Office of Emergency Services be notified immediately in the event of a release. | | | | | | | | | |
| HYDROLOGY AND WATER QUALITY | | | | | | | | | |
| Impacts | | | | | | | | | |
| <ul style="list-style-type: none"> Degradation of surface water quality from construction activities, post-construction activities and uses, and/or pollutants in urban runoff Cumulative increase in pollutants in urban runoff Cumulative degradation of water quality from construction activities and increased urban runoff | | | | | S | S | PS | | U |
| PS = Potentially significant impact | S = Significant mitigable impact | U = Significant and unavoidable impact | X = Mitigation measure identified in Environmental Impact Report | | | | | | |

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Benicia | City of Hercules | City of Pinole | City of Richmond | City of San Pablo | County, Contra Costa |
|---|-----------------------------|-----------------|------------------|----------------|------------------|-------------------|----------------------|
| HYDROLOGY AND WATER QUALITY (cont.) | | | | | | | |
| Impacts (cont.) | | | | | | | |
| • Contamination of well water from neighboring septic tanks or agricultural chemicals | | | | | | | U |
| • Degradation of water quality from industrial spills | | | | | | | U |
| • Diminished water quality from increased water diversions from the Delta, sea water intrusion, and sea level rise | | | | | | | U |
| • Increased flooding and erosion hazards associated with creek restoration. | PS | | | S | S | | |
| • Increased exposure of people and property to flooding | | | | PS | S | | U |
| • Increased flooding risk due to increased runoff from impermeable surfaces | | | | PS | S | | |
| • Cumulative flood conditions from increases in impermeable surfaces | | | | | U | | |
| Mitigation Measures | | | | | | | |
| • Require review and approval by public works department staff or qualified consultant of hydraulic design and maintenance program of applicable creek restoration projects. | | X | | X | | | |
| • Implement specified general plan policies that address storm drain monitoring and maintenance, development design and review, sea level rise, and runoff water quality. | | | X | | | | |
| • Ensure adequate new drainage and pollution prevention and control infrastructure. | | | X | | | | |
| • Calculate runoff from proposed development to ensure no flooding will result. | | X | | | | | |
| • Develop a master water quality control plan to address existing contaminated water resources, manage stormwater runoff, and prevent further pollution. | | X | | X | | | |
| • Develop best management practices for developers to follow. | | X | | | | | |
| • Implement identified measures and land use controls for land bordering Pinole Creek to minimize potential conflicts between flood, resource protection and recreational goals. | | X | | | | | |
| • Work with BCDC to implement strategies to adapt to Bay-related impacts of climate change and develop a vulnerability analysis for the City's shoreline. | | | | X | | X | |
| • Implement Municipal Code flood protection standards for development within a FEMA-designated special flood hazard area and coordinate with FEMA and other agencies in the evaluation and mitigation of future flooding hazards resulting from sea level rise. | | | | | X | | |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | City of San Rafael ^{h,i,j} | Contra Costa County ^j |
|---|-----------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|-------------------------------------|----------------------------------|
| HYDROLOGY AND WATER QUALITY (cont.) | | | | | | | | |
| Mitigation Measures (cont.) | | | | | | | | |
| <ul style="list-style-type: none"> Pursue funding for adequate protection from sea level rise and continued subsidence and construction in areas threatened by level rise and/or settlement. Implement identified measures requiring protection of groundwater from contamination and limiting the number of new wells that are drilled. Identify point sources of pollution and prohibit underground discharge of toxic liquid waste. Support water quality standards and participate in review of regional, state and federal programs that affect water quality and water supply safety. Direct development away from areas at risk of flooding and outside the 100-year flood plain; require all land uses proposed within special flood hazard areas to conform to the requirements of the County Flood Plain Management ordinance. Oppose efforts to construct any water diversion system that reduces Delta water flows unless conclusively demonstrated the diversions will not adversely impact water quality and fisheries. | | | | | | | | |
| LAND USE & PLANNING | | | | | | | | |
| Impacts | | | | | | | | |
| <ul style="list-style-type: none"> Land use incompatibilities Land use impacts from creation of satellite parking facilities Substantial changes in land use density, scale, pattern, and/or character Conflicts with existing zoning Constrained growth in unincorporated areas and intensified growth in urban areas | | | | | | | | |
| Mitigation Measures | | | | | | | | |
| <ul style="list-style-type: none"> Implement specified general plan land use and community design policies. Conduct project-specific environmental review. Implement mixed use development provisions and applicable general plan policies. | | | | | | | | |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | Contra Costa County ^{h,i} |
|---|-----------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|------------------------------------|
| LAND USE & PLANNING (cont.) | | | | | | | |
| Mitigation Measures (cont.) | | | | | | | |
| • Revise the land use element to include policies that enhance the compatibility of new development with surrounding areas; provide adequate buffers between potentially incompatible uses; protect sensitive areas from new development; and require new development to demonstrate prior to approval that potential conflicts can be mitigated. | | | X | | | | |
| • Create a memorandum of understanding with local governments regarding consistency of proposed annexations with the urban limit line and growth management standards. | | | | | | | X |
| • Implement identified measure regarding changes to the Zoning Ordinance. | | | | | | | X |
| • Conduct annual land supply review and 5-year infrastructures constraints review and coordinate with local governments on growth within city spheres of influence. | | | | | | | X |
| NOISE | | | | | | | |
| Impacts | | | | | | | |
| • Exposure to short-term construction noise and/or ground borne vibration | | | PS | S | PS | U | U |
| • Exposure to or generation of excessive ambient noise levels | | | | S | S | U | U |
| • Increased noise levels particularly from vehicular traffic and/or cumulative noise impacts from increased traffic | | | | S | U | U | |
| • Exposure to or generation of cumulative noise levels that are excessive. | | | PS | | U | | |
| Mitigation Measures | | | | | | | |
| • Implement general plan programs and policies that reduce noise impacts. | | X | X | | | | X |
| • Implement/require measures to reduce construction noise. | | X | X | | | | X |
| • Conduct project-level environmental review and implement identified mitigation. | | | X | | X | | |
| • Conduct and analyze data from general and specific noise sources and develop regulatory process to address them. | | | | | | | X |
| • Adopt a noise ordinance. | | | X | | | | X |
| • Incorporate general plan policies requiring site-specific noise studies for noise-sensitive projects that may be affected by railroad noise and requiring incorporation of noise attenuation measures into the project design. | | | | | X | | |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkeley ^b | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | City of San Rafael ^{h,j} | County of Contra Costa ⁱ |
|---|-----------------------------|-------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|-----------------------------------|-------------------------------------|
| NOISE (cont.) | | | | | | | | | |
| Mitigation Measures (cont.) | | | | | | | | | |
| Incorporate general plan policies not to permit new noise-sensitive develop in areas subject to existing or planned transportation noise sources unless project design reduces exterior and interior noise levels as specified. | | | | X | | | | | |
| POPULATION AND HOUSING | | | | | | | | | |
| Impacts | | | | | | | | | |
| Substantial induced growth or concentration of population | | | PS | | | | | | |
| Mitigation Measures | | | | | | | | | |
| Implement specified general plan land use policies. | | | X | | | | | | |
| PUBLIC SERVICES | | | | | | | | | |
| Impacts | | | | | | | | | |
| Increased demand for police/law enforcement protection services | PS | PS | S | | | | | U | |
| Increased demand for fire protection services | | PS | S | | | | | U | |
| Increased demand for fire protection service and potential interference with emergency response services | | | PS | | | | | | |
| Increased demand for schools | S | PS | U | | | | | U | |
| Potential impacts from construction of new fire station | | PS | | | | | | | |
| Increased demand for child care facilities | | | | | | | | U | |
| Increased demand for libraries and other public facilities | | | | | | | | U | |
| Mitigation Measures | | | | | | | | | |
| Implement identified general plan policies addressing provision of fire and police protection services. | | | X | X | | | | | |
| Review new development for potential increases in fire hazards and potential adverse impacts on fire services. | | X | | | | | | | |
| Conduct project-specific review to assess impacts of fire station construction. | X | | | | | | | | |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkeley ^b | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | City of San Rafael ^{h,j} | Contra Costa County ^j |
|---|-----------------------------|-------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|-----------------------------------|----------------------------------|
| PUBLIC SERVICES (cont.) | | | | | | | | | |
| Mitigation Measures (cont.) | | | | | | | | | |
| • Require new development to pay fair share of costs of new fire protection facilities and services. | | | | | | | | | X |
| • Implement identified measures to establish standards for provision of police protection services. | | | | | | | | | X |
| • Conduct annual review of fire department staffing levels and new development to determine whether additional staffing or impact fee is warranted. | | X | | | | | | | |
| • Work with school district to evaluate impact of new development on district facilities. | X | | X | | | | | | |
| • Require major residential developments to prepare analysis of project impact on schools | X | | | | | | | | |
| • Implement identified measure to provide for school impact fee or other financing option. | | | X | | | | | | |
| • Implement identified measures to encourage the development of child care facilities. | | | | | | | | X | |
| RECREATION | | | | | | | | | |
| Impacts | | | | | | | | | |
| • Increased demand for new or expanded parks and/or recreational facilities | | | | PS | U | | | | U |
| Mitigation Measures | | | | | | | | | |
| • Implement general plan policies and programs to improve, expand, acquire, and/or develop park and recreational facilities | | | X | X | | | | | X |
| • Implement identified measures to ensure that new development funds its share of costs associated with providing park facilities. | | | | X | | | | | |
| TRAFFIC AND TRANSPORTATION | | | | | | | | | |
| Impacts | | | | | | | | | |
| • Unacceptable levels of service due to increased traffic volumes | | | S | | | | | | U |
| • Increased traffic and unacceptable levels of service at area intersections | S | PS | | S, U | S | | | | |
| • Cumulative traffic impacts on roadway segments and/or intersections | | | | U | S | S | U | | |
| • Cumulative transportation impacts and cumulative impacts on bus service operations | | | | | | S ^k | | | |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkeley ^b | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | Contra Costa County ^{h,i,j} |
|--|-----------------------------|-------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|--------------------------------------|
| TRAFFIC AND TRANSPORTATION (cont.) | | | | | | | | |
| Impacts (cont.) | | | | | | | | |
| • Conflict of cumulative projects with the West County Action Plan's multimodal transportation service objectives | | | | | | | U | |
| • Impacts and cumulative impacts on emergency response times due to increased traffic and congestion | | | | | | | U | |
| • Increased in freeway traffic volumes during peak commute periods | | | | | | | U | |
| • Possible diversion of freeway traffic to city streets | S | | | | | | | |
| • Increased traffic congestion and demands on public transit | | | | | | | PS | |
| • Generation of parking demand in excess of supply | | | | | | | PS | |
| • Greater conflicts between cyclists and pedestrians from growth in motorized and bicycle traffic. | | | | | | | | U |
| • Growth induced caused by planned airport expansion | | | | | | | | U |
| Mitigation Measures | | | | | | | | |
| • Implement general plan and/or local or regional transportation plan programs, policies, and measures to mitigate traffic and circulation impacts. | | | | | | X | | |
| • Revise general plan policies to: clarify that transit corridors would not be modified unless such modifications will not cause adverse impacts related to street capacity or the benefits outweigh potential level of service impacts; require that related CEQA findings be supported by analysis demonstrating the project area's transportation level of service will not significantly deteriorate; require the City to set traffic volume guidelines for all streets. | | | | | X | | | |
| • Implement identified general plan growth management and circulation and transportation policies. | | | | | | X | | |
| • Monitor specified intersections, complete roadway projects, and implement highway improvements to discourage traffic from diverting onto local streets. | | | | | | X | | |
| • Monitor critical intersections for congestion and potential improvements. | X | | | | | | | |
| • Implement operational and other measures to improve levels of service and reduce congestion at intersections. | X | | | | | X | | |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of Berkele ^b y | City of El Cerrito ^c | City of Hercules ^d | City of Pinole ^e | City of Richmond ^f | City of San Pablo ^g | Contra Costa County ^{h,i} |
|--|-----------------------------|--------------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|------------------------------------|
| TRAFFIC AND TRANSPORTATION (cont.) | | | | | | | | |
| Mitigation Measures (cont.) | | | | | | | | |
| • Through the Congestion Management Agency coordinate street and highway improvements with other jurisdictions and Caltrans. | X | | | | | | | |
| • Implement measures to encourage the use of alternative modes of travel and reduce vehicle trips. | X | | | | | | | |
| • Pursue adoption of a transportation impact fee | X | | | | | | | |
| • Monitor potentially affected roadways, prepare an action plan to improve levels of service as specified, and prepare a deficiency plan for specified routes when deficient conditions occur. | X | | | | | | | |
| • Evaluate potential impacts on transit service or parking before approving new development or zoning amendment that would allow car free development | X | | | | | | | |
| • Minimize diversions of freeway traffic to local streets and implement measures to discourage such diversions and/or to encourage traffic to return to the freeway. | X | | | | X | | | |
| • Work transportation advisory committee and transportation authority to revise action plan levels of service standards and multimodal traffic service objectives as specified. | | | | | X | | | |
| • Work with transportation advisory committee and AC Transit to construct additional bus turnouts on specified roadways. | | | | | X | | | |
| • Conduct project-specific environmental review and implement mitigation. | | | | | | X | | |
| • Implement identified measures to construct bikeways and incorporate the needs of bicyclists in major roadway construction projects and other improvements. | | | | | | | X | |
| • Limit growth inducement potential at the planned East County Airport by providing appropriate amount of buffer land around the airport. | | | | | | | X | |
| UTILITIES | | | | | | | | |
| Impacts | | | | | | | | |
| • Increased stormwater flows | | | | PS | PS | S | | |
| • Increased water demand exceeding currently planned supplies. | | | | PS | S | | | U |

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TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | Albany ^a | Berkeley ^b | City of EI | City of EI Hercules ^d | City of Richmond, ^e Palo Alto ^f | City of San Francisco ^g | Contra Costa County ^{h,i} |
|----------------------------|---|------------------------------------|--|--|--|---------------------------------------|--|
| UTILITIES (cont.) | | | | | | | |
| Impacts (cont.) | | | | | | | |
| | <ul style="list-style-type: none"> Need for new or expanded wastewater collection and/or treatment facilities and/or cumulative impact on wastewater treatment capacity Impacts associated with landfill capacity and siting solid waste facilities Cumulative impact on landfill capacity | | | | U | U | U |
| Mitigation Measures | | | | | U | | U |
| | <ul style="list-style-type: none"> Encourage the implementation of water conservation measures. Implement identified general plan policies to maintain and monitor storm drain needs. Adopt recycled water ordinance upon notification by EBMUD that recycled water is available to serve new development in the City. Condition new development on assurances that adequate water quantity and quality is available and encourage water agencies to establish service boundaries to meet future water needs. Condition new development on the assurances of adequate sewer capacity and sewage treatment facilities in compliance with applicable waste water discharge requirements. Implement general plan policies to encourage water conservation and reduce demand from current and future development. Implement identified measures requiring new development to pay its share of costs associated with providing water and wastewater service, encouraging dual plumbing systems in large developments for future use of reclaimed water, requiring low flow toilets and plumbing fixtures, and to initiate a wastewater treatment study. Cooperate with EBMUD water system planning efforts and implement a capital improvement program for selected wastewater treatment alternatives. Implement policies and measures to mitigate effects of landfill siting. Implement measures to encourage and facilitate recycling and resource recovery. | | X | X | X | X | |
| ENERGY | | | | | | | |
| Impacts | | | | | | | |
| | <ul style="list-style-type: none"> Significant increase in energy consumption | S = Potentially significant impact | U = Significant and unavoidable impact | X = Mitigation measure identified in Environmental Impact Report | | | |

TABLE N-1 (Continued)
POTENTIALLY SIGNIFICANT (PS), SIGNIFICANT MITIGABLE (S), AND SIGNIFICANT UNAVOIDABLE (U) IMPACTS OF GROWTH IDENTIFIED IN GENERAL AND SPECIFIC PLAN ENVIRONMENTAL IMPACT REPORTS IN PROJECT AREA

| Impact / Mitigation | City of Albany ^a | City of El Cerrito ^b | City of Hercules ^c | City of Pinole ^d | City of Richmond ^e | City of San Pablo ^f | City of San Rafael ^g | City of San Ramon ^h | Contra Costa County ⁱ |
|---|-----------------------------|---------------------------------|-------------------------------|-----------------------------|-------------------------------|--------------------------------|---------------------------------|--------------------------------|----------------------------------|
| • Increased demand for heating and cooling systems and potential for localized warming from increased lot coverage | | PS | | | | | | | |
| • Increased demand for automobile fuel | | PS | | | | | | | |
| Mitigation Measures | | | | | | | | | |
| <ul style="list-style-type: none"> • Implement identified general plan policies concerning energy conservation and alternative modes of transportation. • Require demonstration projects of cost-effective conservation techniques and conservation site planning, building design and landscaping. | | | | | | | | | |

^a City of Albany, *Albany General Plan Update and Revision Program Draft Environmental Impact Report and Final Environmental Impact Report*: Response to Comments, State Clearinghouse # 89022809, Technical Appendix A of Albany General Plan and Final EIR, September 1992.

^b City of Berkeley, City of Berkeley Draft General Plan/Final Environmental Impact Report, SCH # 2000102107, June 2001.

^c City of El Cerrito, City of El Cerrito General Plan Update, State Clearinghouse #99022058, April 16, 1999.

^d City of Hercules, *City of Hercules General Plan Land Use and Circulation Elements Update and Redevelopment Plan Amendments Environmental Impact Report*, Volume 1: EIR Text, prepared for the City of Hercules, prepared by Environmental Science Associates, June 9, 1995.

^e City of Pinole, City of Pinole General Plan Update Draft Environmental Impact Report (July 2010) and *Final Environmental Impact Report*, prepared for City of Pinole, prepared by PMC, September 2011.

^f City of Richmond, *Richmond General Plan Update Final Environmental Impact Report* (November 2010) and Volume 4: *Final Environmental Impact Report* (February 2011), SCH No. 200808269, Environmental Impact Report certified by the City Council April 18, 2011.

^g City of San Pablo, *San Pablo General Plan 2030, Volume 3: Draft Environmental Impact Report* (November 2010) and Volume 4: *Final Environmental Impact Report* (February 2011), SCH No. 200808269, Environmental Impact Report certified by the City Council April 18, 2011.

^h County Contra Costa County, *Findings Related to Certification of the Environmental Impact Report for the General Plan and Adoption of the General Plan* (Contra Costa County, 1991), and Notice of Determination, Negative Declaration prepared for Reconsolidation of the Contra Costa County General Plan, Contra Costa County, 2005.

ⁱ Population shown includes cities and unincorporated areas.

^j Identified as a cumulatively considerable impact that is considered significant and unavoidable.

^k Identified as a cumulatively considerable or potentially considerable impact that is reduced to less than cumulatively considerable with mitigation.

^l Identified as a cumulatively considerable or potentially considerable impact that is reduced to less than cumulatively considerable with mitigation.

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References – Appendix N

- City of Albany, 1992. *Albany General Plan Update and Revision Program Draft Environmental Impact Report and Final Environmental Impact Report: Response to Comments*, State Clearinghouse # 89022809, Technical Appendix A of *Albany General Plan and Final EIR*, September 1992.
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- City of Richmond, 2011. *Richmond General Plan Update Final Environmental Impact Report*, prepared for City of Richmond Development Services Department, prepared by Atkins, August 2011.
- City of San Pablo, 2011. *San Pablo General Plan 2030, Volume 3: Draft Environmental Impact Report* (November 2010) and *Volume 4: Final Environmental Impact Report* (February 2011), SCH No. 2008082069, Environmental Impact Report certified by the City Council April 18, 2011.
- Contra Costa County, 1991, *Findings Related to Certification of Environmental Impact Report for General Plan and Adoption of General Plan*, January 29, 1991.
- Contra Costa County, 2005, Notice of Determination, Negative Declaration prepared for Reconsolidation of the Contra Costa County General Plan, County File: GP#04-0007, January 19, 2005.